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One report and one enclosure containing:

- 9 magnetic map sheets,
- 9 enhanced magnetic map sheets,
- 9 resistivity map sheets,
- 9 electromagnetic map sheets

A Dighem II airborne electromagnetic / resistivity / magnetic survey of 4.415 line-kilometer was flown in august and september of 1981 for Orkla Industrier AS in the Løkken area of Norway.

The geological environment in the survey area was condictive and magnetically active. The EM anomalies occurred primarily due to conductive bedrock features and to culture. Numerous conductors of short strike length appear to be the best exploration targets. A knownledge of area geology will be essential for ground follow-up in the view of the abundance of EM anomalies with long strice length.

DIGHEM<sup>II</sup> SURVEY

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LØKKEN AREA, NORWAY

FOR

ORKLA INDUSTRIER A/S

BY

DIGHEM LIMITED

TORONTO, CANADA APRIL 16, 1982 S. KILTY
GEOPHYSICIST

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VICE-PRESIDENT

### SUMMARY

A Dighem<sup>II</sup> airborne electromagnetic/resistivity/
magnetic survey of 4,415 line-kilometers was flown in August
and September of 1981 for ORKLA Industries A/S in the Lokken
area of Norway.

The geologic environment in the survey area was conductive and magnetically active. The EM anomalies occurred primarily due to conductive bedrock features and to culture. Numerous conductors of short strike length appear to be the best exploration targets. A knowledge of area geology will be essential for ground follow-up in view of the abundance of EM anomalies with long strike length.

# 10°00' 10°00' 10°00' 10°00' Rennebu 10°00'

SCALE 1:750,000

FIGURE 1 THE SURVEY AREA

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# INTRODUCTION

A DIGHEMII survey of 4,415 line-km was flown with a 200 m line-spacing for ORKLA Industries A/S, from August 18 to September 12, 1981 in the Lokken area, Norway (Figure 1).

The Lama LN-OTB turbine helicopter flew with an average airspeed of 101 km/h and EM bird height of 35 m. Ancillary equipment consisted of a Sonotek PMH-5010 magnetometer with its bird at an average height of 50 m, a Sperry radio altimeter, Geocam sequence camera, Barringer 8-channel hot pen analog recorder, and a Sonotek SDS-1200 digital data acquisition system with a Digidata 1140 9-track 800-bpi magnetic tape recorder. The analog equipment recorded four channels of EM data at approximately 900 Hz, two ambient EM noise channels (for the coaxial and coplanar receivers), and one channel each of magnetics and radio altitude. The digital equipment recorded the EM data with a sensitivity of .20 ppm/bit and the magnetic field to one gamma/bit.

Appendix A provides details on the data channels, their respective noise levels, and the data reduction procedure. The quoted noise levels are generally valid for wind speeds up to  $35~\mathrm{km/h}$ . Higher winds may cause the system to be grounded because excessive bird swinging

produces difficulties in flying the helicopter. The swinging results from the  $5\ m^2$  of area which is presented by the bird to broadside gusts. The DIGHEM system nevertheless can be flown under wind conditions that seriously degrade other AEM systems.

# ELECTROMAGNETICS

classes, discrete and broad. The discrete class consists of sharp, well defined anomalies from discrete conductors such as sulfide lenses and steeply dipping sheets of graphite and sulfides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulfide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, and geothermal zones. A vertical conductive slab with a width of 100 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the electromagnetic map are interpreted according to this model. The following section entitled Discrete conductor analysis describes this model in detail,

including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

The conductive earth (half space) model is suitable for broad conductors. Resistivity contour maps result from the use of this model. A later section entitled Resistivity mapping describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulfide bodies.

# Discrete conductor analysis

The EM anomalies appearing on the electromagnetic map are interpreted by computer to give the conductance (i.e., conductivity-thickness product) in mhos of a vertical sheet model. DIGHEM anomalies are divided into six grades of conductance, as shown in Table I. The conductance in mhos is the reciprocal of resistance in ohms.

Table I. EM Anomaly Grades

Anomaly Grade	Mho Range
6	> 100
5	50 - 99
4	20 - 49
3	10 - 19
2	5 - 9
1	< 5

The mho value is a geological parameter because it is a characteristic of the conductor alone; it generally is independent of frequency, and of flying height or depth of burial apart from the averaging over a greater portion of the conductor as height increases. 1 Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger mho values.

Conductive overburden generally produces broad EM responses which are not plotted on the EM maps. However, patchy conductive overburden in otherwise resistive areas can yield discrete-like anomalies with a conductance grade (cf. Table I) of 1, or even of 2 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities can be below 1 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such surface conductors to be recognized, and these are indicated by the letter S on the map. The remaining anomalies in such areas could be bedrock

<sup>1</sup>This statement is an approximation. DIGHEM, with its short coil separation, tends to yield larger and more accurate mho values than airborne systems having a larger coil separation.

conductors. The higher grades indicate increasingly higher conductances. Examples: DIGHEM's New Insco copper discovery (Noranda, Quebec, Canada) yielded a grade 4 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Sturgeon Lake, Ontario, Canada) and Whistle (nickel, Sudbury, Ontario, Canada) gave grade 5; and DIGHEM's Montcalm nickel-copper discovery (Timmins, Ontario, Canada) yielded a grade 6 anomaly. Graphite and sulfides can span all grades but, in any particular survey area, field work may show that the different grades indicate different types of conductors.

Strong conductors (i.e., grades 5 and 6) are characteristic of massive sulfides or graphite. Moderate conductors (grades 3 and 4) typically reflect sulfides of a less massive character or graphite, while weak bedrock conductors (grades 1 and 2) can signify poorly connected graphite or heavily disseminated sulfides. Grade 1 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche Mining Corporation near Bathurst, New Brunswick,

Canada, yielded a well defined grade 1 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction.

Faults, fractures and shear zones may produce anomalies which typically have low conductances (e.g., grades 1 and 2). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

On the electromagnetic map, the actual mho value and a letter are plotted beside the EM grade symbol. The letter is the anomaly identifier. The horizontal rows of dots, beside each anomaly symbol, indicate the anomaly amplitude on the flight record. The vertical column of dots gives the estimated depth. In areas where anomalies are crowded, the identifiers, dots and mho values may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the inphase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The mho value and depth estimate will illustrate which of these possibilities fits the recorded data best.

two anomalies, having similar mho values but dramatically different depth estimates, occur close together on the same conductor. Such examples illustrate the reliability of the conductance measurement while showing that the depth estimate can be unreliable. There are a number of factors which can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be

deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock on the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes which may define the geological structure over portions of the survey area. The absence of conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

DIGHEM electromagnetic maps are designed to provide a correct impression of conductor quality by means of the conductance grade symbols. The symbols can stand alone with

geology when planning a follow-up program. The actual mho values are plotted for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike direction, conductance, depth, thickness (see below), and dip. The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

An EM anomaly list attached to each survey report provides a tabulation of anomalies in ppm, and in mhos and estimated depth for the vertical sheet model. anomaly list also shows the conductance in mhos and the depth for a thin horizontal sheet (whole plane) model, but only the vertical sheet parameters appear on the EM map. The horizontal sheet model is suitable for a flatly dipping thin bedrock conductor such as a sulfide sheet having a thickness less than 15 m. The list also shows the resistivity and depth for a conductive earth (half space) model, which is suitable for thicker slabs such as thick conductive In the EM anomaly list, a depth value of zero overburden. for the conductive earth model, in an area of thick cover, warns that the anomaly may be caused by conductive overburden.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute local anomaly amplitudes. This contrasts with the use of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth. Not shown in the EM anomaly list are the true amplitudes which are used to compute the horizontal sheet and conductive earth parameters.

# X-type electromagnetic responses

DIGHEMII maps contain x-type EM responses in addition to EM anomalies. An x-type response is below the noise threshold of 3 ppm, and reflects one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of a flight line, or aerodynamic noise. Those responses that have the appearance of valid bedrock anomalies on the flight profiles are mentioned in the report. The others should not be followed up unless their locations are of considerable geological interest.

# The thickness parameter

DIGHEMII can provide an indication of the thickness of a steeply dipping conductor. The ratio of the anomaly amplitude of channel 24/channel 22 generally increases as the apparent thickness increases, i.e., the thickness in the horizontal plane along the flight line. This thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line. This report refers to a conductor as thin when the thickness is likely to be less than 3 m, and  $\underline{\text{thick}}$  when in excess of In base metal exploration applications, thick conductors can be high priority targets because most massive sulfide ore bodies are thick, whereas non-economic bedrock conductors are usually thin. An estimate of thickness cannot be obtained when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

# Resistivity mapping

Areas of widespread conductivity are commonly encountered during surveys. In such areas, anomalies can be generated by decreases of only 5 m in survey altitude as

well as by increases in conductivity. The typical flight record in conductive areas is characterized by inphase and quadrature channels which are continuously active; local peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the interpretation of the airborne data. The advantage of the resistivity parameter is that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conduc-This helps the interpreter to differentiate tivity changes. between conductive trends in the bedrock and those patterns typical of conductive overburden. Discrete conductors will generally appear as narrow lows on the contour map and broad conductors will appear as wide lows.

Channel 40 (see Appendix) and the resistivity contour map present the apparent resistivity using the so-called pseudo-layer (or buried) half space model defined in Fraser (1978)<sup>2</sup>. This model consists of a resistive layer overlying a conductive half space. Channel 41 gives the apparent depth below surface of the conductive material.

<sup>&</sup>lt;sup>2</sup>Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v 43, p. 144-172.

The apparent depth is simply the apparent thickness of the overlying resistive layer. The apparent depth (or thickness) parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half space exists. apparent depth parameter must be interpreted cautiously because it will contain any errors which may exist in the measured altitude of the EM bird (e.g., as caused by a dense The inputs to the resistivity algorithm are tree cover). the inphase and quadrature components of the coplanar coil-The outputs are the apparent resistivity of the conductive half space (the source) and the sensor-source The flying height is not an input variable, distance. and the output resistivity and sensor-source distance are The apparent depth, independent of the flying height. discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter. The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. The DIGHEMII system has been flown for the purpose of permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel 41 can be of significant help in distinguishing between overburden and bedrock conductors.

# Interpretation in conductive environments

Environments having background resistivities below 30 ohm-m cause all airborne EM systems to yield very large responses from the conductive ground. This usually prohibits the recognition of bedrock conductors. The processing of DIGHEMII data, however, produces six channels which contribute significantly to the recognition of bedrock conductors. These are the inphase and quadrature difference channels (#33 and 34), the resistivity and depth channels (#40 and 41), the conductivity contrast channel (#42), and the product of the conductivity contrast and depth contrast channels (#44).

The EM difference channels (33 and 34) eliminate up to 99% of the response of conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. An edge effect arises when the conductivity of the ground suddenly changes, and this is a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic The recognition of a bedrock conductor in a highly noise. conductive environment therefore is based on the anomalous responses of the two difference channels (33 and 34) and the resistivity channel (40). The most favourable situation is where anomalies coincide on all three channels.

Channel 41, which is the apparent depth to the conductive material, also helps determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When this channel rides above the zero level on the electrostatic chart paper (i.e., it is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e.,

conductive overburden. If channel 41 is below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor.

The conductivity contrast channel (#42) highlights local resistivity lows. This channel, and the depth contrast (#43), both yield positive anomalies from conductors at depth. Channel 44 is the multiple 42\*43 and it is highly sensitive to conductors at depth. The interpretation of channels 42 and 44 has to be done carefully, however, because they may also respond in a similar fashion to a local thickening in the conductive cover as, for example, over a buried river channel. Channels 42 and 43 are derived from channels 40 and 41 using digital filter techniques.

Channels 35, 36 and 42 are the anomaly recognition functions. They are used to trigger the conductance channel 37 which identifies discrete conductors. In highly conducting environments, channel 36 is deactivated because it is subject to corruption by highly conductive earth signals. Some of the automatically selected anomalies (channel 37) are discarded by the human interpreter. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. The interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by

the data, such as those arising from geologic or aerodynamic noise.

The resistivity map often yields more useful information on conductivity distributions than the EM map. In comparing the EM and resistivity maps, keep in mind the following:

- (a) The resistivity map portrays the absolute value of the earth's resistivity.
- (b) The EM map portrays anomalies in the earth's resistivity. An anomaly by definition is a change from the norm and so the EM map displays anomalies, (i) over narrow, conductive bodies and (ii) over the boundary zone between two wide formations of differing conductivity.

The resistivity map might be likened to a total field map and the EM map to a horizontal gradient in the direction of flight<sup>3</sup>. Because gradient maps are usually more sensitive than total field maps, the EM map therefore is to be

<sup>&</sup>lt;sup>3</sup>The gradient analogy is only valid with regard to the identification of anomalous locations. The calculation of conductance is based on EM amplitudes relative to a local base level, rather than to an absolute zero level as for the resistivity calculation.

preferred in resistive areas. However, in conductive areas, the absolute character of the resistivity map usually causes it to be more useful than the EM map.

# Reduction of geologic noise

responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned above that the EM difference channels (i.e., channel 33 for inphase and 34 for quadrature) tend to eliminate the response of conductive overburden. This marked a unique development in airborne EM technology, as DIGHEMII is the only EM system which yields channels having an exceptionally high degree of immunity to conductive overburden.

Magnetite produces a form of geological noise on the inphase channels of all EM systems. Rocks containing less than 1% magnetite can yield negative inphase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the inphase EM channels may continuously rise and fall reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing

deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the inphase difference channel 33. This feature can be a significant aid in the recognition of conductors which occur in rocks containing accessory magnetite.

# EM magnetite mapping

The information content of DIGHEM<sup>II</sup> data consists of a combination of conductive eddy current response and magnetic permeability response. The secondary field resulting from conductive eddy current flow is frequencydependent and consists of both inphase and quadrature components, which are positive in sign. On the other hand, the secondary field resulting from magnetic permeability is independent of frequency and consists of only an inphase component which is negative in sign. magnetic permeability manifests itself by decreasing the measured amount of positive inphase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative inphase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique was developed for the coplanar coil-pair of DIGHEMII. The technique yields channel 50 which displays apparent weight percent magnetite according to a homogeneous half space model. The method can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half space. It can individually resolve steeply dipping narrow magnetite-rich bands which are separated by 60 m.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as indicated by anomalies in channel 50.

The EM magnetite algorithm is basically quite simple because a linear relationship exists between volume percent magnetite and the negative inphase response in ppm. This linear relationship is true for a fixed survey altitude when

demagnetization effects are disregarded and when a fixed susceptibility-volume percent relationship is assumed. The technique in practice involves, first, correcting the actual EM response for variations in flying altitude and, second, calibrating the negative inphase ppms in terms of volume percent magnetite.

EM magnetite mapping provides another method of airborne geologic mapping. It thus joins resistivity mapping, magnetometer mapping, spectrometry, photogeology, etc., as a possible means by which geologic information can be obtained from airborne techniques. It is not nearly as useful in the general sense as the other airborne mapping techniques, but can be of value in cases where the magnetite content gives an indication of lithology.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

# MAGNETICS

The existence of a magnetic correlation with an EM anomaly is indicated directly on the EM map. An EM anomaly with magnetic correlation has a greater likelihood of being produced by sulfides than one that is non-magnetic. However, sulfide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Ontario, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Ontario).

The magnetometer data are digitally recorded in the aircraft to an accuracy of one gamma. The digital tape is processed by computer to yield a standard total field magnetic map which is usually contoured at 25 gamma intervals. The magnetic data also are treated mathematically to enhance the magnetic response of the near-surface geology, and an enhanced magnetic map is produced with a 100 gamma contour interval. The response of the enhancement operator in the frequency domain is shown in Figure 2. The 100 gamma contour interval is equivalent to a 5 gamma interval for the passband components of the airborne data. This is because these components are amplified 20 times by the operator of Figure 2.

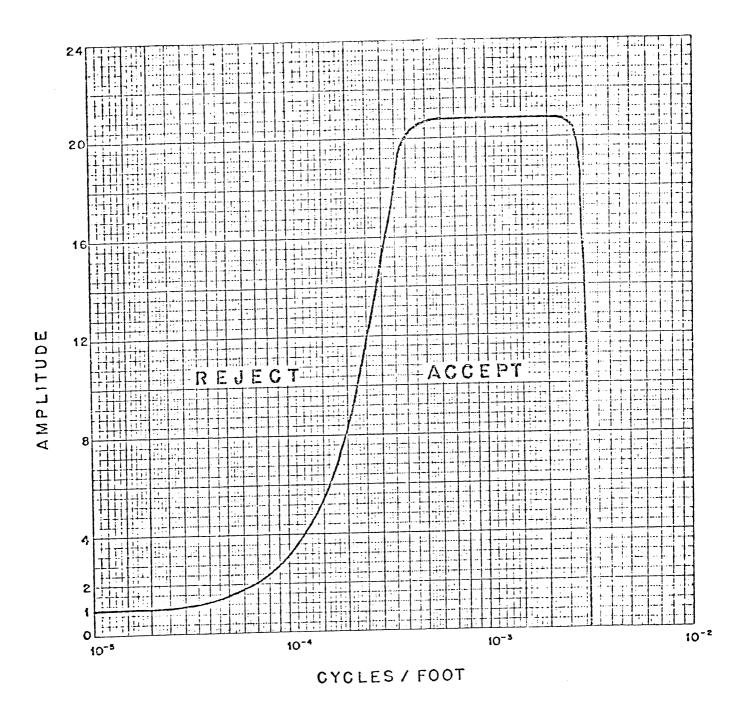


Figure 2 Frequency response of magnetic operator

The enhanced map, which bears a resemblance to a downward continuation map, is produced by digital bandpass filtering the total field data. The enhancement is equivalent to continuing the field downward to a level (above the source) which is 1/20th of the actual sensor-source distance.

Because the enhanced magnetic map bears a resemblance to a ground magnetic map, it simplifies the recognition of trends in the rock strata and the interpretation of geological structure. The contour interval of 100 gammas is suitable for defining the near-surface local geology while de-emphasizing deep-seated regional features.

# CONDUCTORS IN THE SURVEY AREA

The electromagnetic maps show the locations of conductors and their interpreted conductance (i.e., conductivity-thickness product), depth and, occasionally, dip. Their strike direction and length are also shown when anomalies can be correlated from line to line. When studying the maps for follow-up planning, consult the anomaly listings appended to this report to ensure that none of the conductors are overlooked.

The survey consisted of two flight blocks. The flight direction was north-south in the western block, and northwest-southeast in the smaller eastern block. The amounts flown in the individual blocks are shown below:

Block	Line-number	Line-km
West East	1-297 301-341	4,208 207 4,415

The EM maps indicate which anomalies are believed to be caused by culture or surficial sources. Generally, such anomalies are not commented on below as the discussions are directed to identifying bedrock features.

The larger of the two flight blocks, which occupies the western part of the survey area, contains a greenstone belt bordered on both north and south sides by older sediments.

Rocks in the eastern part of the block were mapped as younger sediments and gabbro.

The resistivity map shows an excellent correlation with geology. In general, the greenstones are resistive with

Group 3

These grade 1 to 6 anomalies and associated x-type responses reflect a series of parallel bedrock conductors which appear to dip to the south. They may belong to the same horizon as group 1. Note that the conductivity-thickness values within this group are much higher than in group 1. This group should be investigated on the ground.

Anomalies 15E-16G

These grade 2 and 4 anomalies
reflect a magnetic conductive
horizon of limited strike extent
located adjacent to a formational
horizon. This conductor appears to
dip to the south. It should be
investigated on the ground.

Responses 42xB, 49xA

These x-type responses reflect two weak conductors associated with magnetite. The magnetite has masked the responses causing suppression of their inphases.

These responses should be investigated on the ground.

# Sheet 2

Groups 1, 2

These grade 1 to 6 anomalies and associated x-type responses reflect two conductive horizons of large areal extent which have strike extensions into Sheet 1. Both groups appear to be dipping to the south. Any of the anomalies within this group could be due to a sulphide source.

Anomolies 65F, 69E, 70xA-71E, 84E-85H, 110B-111xA These grade 1 to 3 anomalies and associated x-type responses reflect an intermittently conductive horizon associated with magnetite.

These bedrock conductors should be investigated.

Anomalies 92C, 104C-107A These grade 1 and 2 anomalies reflect a weak conductive horizon

that may be due to cultural sources. This horizon should be examined on the ground to determine the source of its conductivity.

Anomalies 109A-113B, 109B-110xB, 113A-114B, 113C These grade 1 to 4 anomalies and associated x-type responses reflect an extension of group 1 to the east. Anomaly 113C is of particular interest because of its isolation. Note that this anomaly indicates that the conductor is either located between flight lines or striking parallel to flight direction.

# Sheet 3

Anomalies 119A-157B, 130xA-141xB, 144A-163A These grade 1 to 4 anomalies and associated x-type responses reflect three formational bedrock conductors of extensive strike length.

Resistivity contours indicate that they are part of a low resistivity zone of large areal extent striking parallel to the survey area boundary. The conductors are associated with weak magnetic highs.

Anomalies 120A-130xB, 133C-142xB, 140D-145B These grade 1 to grade 4 anomalies and associated x-type responses represent three probable bedrock conductors that may represent the same conductive horizon. Anomalies 133C-142xB appear to reflect a bedrock conductor through which 50 Hz signal due to powerline interference is being channeled. All three conductors have direct magnetic correlation.

Anomalies 152B, 152C-155xA, 158A-159A These grade 1 to grade 3 anomalies and associated x-type responses reflect two bedrock conductors of limited strike length. Both

conductors are located immediately adjacent to formational conductors and both are non-magnetic. They should be examined on the ground.

Group 4

These grade 1 to 3 anomalies and associated x-type responses reflect a series of parallel bedrock conductors probably related to a common formational horizon. that those anomalies labelled L? probably reflect bedrock conductors through which 50 Hz signal from an adjacent powerline is being The formational horizon channeled. represented by this group is masked by a powerline at its western This group may belong to the same horizon as anomalies 119A-156B.

Anomalies 166D-171E, 170E These grade 1 to 3 anomalies reflect two bedrock conductors located to the side of a formational horizon.

Anomaly 170E reflects a bedrock conductor comprised of magnetite and possibly associated sulphides. Conductor 166D-171E is strongest near anomaly 169H. Both of these conductors should be investigated on the ground.

# Sheet 4

## Group 5

These grade 1 to 6 anomalies and associated x-type responses reflect a conductive horizon of large areal extent whose borders are best defined by the resistivity patterns. All anomalies within this group appear to be due to bedrock sources and are probably related to conductive materials within a sedimentary horizon. Electromagnetic anomalies appear to indicate a fault striking northwest in the vicinity of lines 139 and 140. Any anomalies in this

group could be due to sulphide sources. This group continues into Sheets 2 and 6.

Anomalies 131D, 137K-138K These grade 1 and 2 anomalies are associated with negative inphase responses which has resulted in a reduction of the conductivity—thickness product. These conductors are both located to the side of a broad formational horizon and may reflect magnetite with some associated sulphides.

Anomalies 139C-1420E, 139D-140G

These grade 1 to 3 anomalies

reflect a pair of bedrock

conductors located adjacent to a

major conductive horizon. The east

end of conductor 139C-1420E abuts

against an interpreted fault zone.

Note that the coaxial/coplanar

ratio indicates that anomaly 1420E

is due to a conductor located off

the flight line. This conductor

warrants ground follow-up.

Anomalies 141C-154D, 1420C-145A, 149xB-154B, 156B-157A, 157B-158B, 160B-163xC, 165C, 169D-176F, 169E-171F, 176G-178G, 178F-180D These grade 1 to 3 anomalies and associated x-type responses reflect an intermittent conductive bedrock horizon located along the flanks of a long continuous magnetic high.

Any of these anomalies could be due to a sulphide source. This conductive horizon extends into map sheet 6.

Anomalies 1500E-157J, 153G-160M, 154K-156F, 165xF-1660, 166N-168J These grade 1 to 4 anomalies and associated x-type responses reflect bedrock conductors located immediately adjacent to a formational horizon. Conductor 154K-156F appears to be due to an iron formation with other associated sulphides. These conductors may belong to the same formational horizon as group 5. All conductors appear to have a north dip.

Anomalies 157D-161xD, 164C-165E, 173xC-176H, 173G-1740G These grade 1 to 4 anomalies
reflect four bedrock conductors
located adjacent to a formational
horizon. All conductors are
associated with strong magnetite
responses. These anomalies may
belong to the same geological
horizon.

Anomalies 161A-163A, 164A-169A, 165B-178D, 172F-175E 172D-180B, 177C-178E, 175A-175B, These grade 1 to 4 anomalies and associated x-type responses reflect a series of bedrock conductors which probably belong to the same conductive horizon. Generally, these conductors appear to be dipping to the north. This horizon extends into sheet 6. Anomalies 177C, 178E, and 176A are of particular interest because of their high conductivity-thickness product, limited strike length and isolated location.

#### Sheet 5

Group 4

These grade 1 to 4 anomalies and associated x-type responses reflect a conductive formational horizon that extends into Sheet 3. The conductive horizon correlates with a magnetic high as indicated by the enhanced magnetic contours.

Resistivity contours indicate that this horizon may have a strike extension to the north-east.

Anomalies 183E-185xB, 1880B-194C These grade 1 to 3 anomalies reflect two bedrock conductors which probably belong to the same conductive horizon. These anomalies are mainly due to magnetite, with possibly some associated sulphides.

Anomaly 193B-194B

These grade 1 and 2 anomalies
reflect a bedrock conductor located
adjacent to a formational horizon.
Note that the coaxial/coplanar

ratio indicates that anomaly 193B is due to a source located off the flight line.

Anomaly 197D-1990E

These grade 1 to 5 anomalies

reflect a strong bedrock conductor

associated with a prominent

magnetic high. These anomalies

reflect a conductor composed of

magnetite and probably associated

sulphides. This area should be

given a high priority in ground

follow-up.

Group 6

These grade 2 to 5 anomalies and associated x-type responses indicate two or more strong bedrock conductors located near an iron formation. All anomalies are strong bedrock responses and warrant ground investigation. This group should be given a high priority.

Anomaly 2160D-2240J

These grade 1 to 6 anomalies and associated x-type responses reflect a bedrock conductor of limited strike extent that appears to be

dipping to the north. The conductor appears to be magnetic in the centre and it contains a thick section on lines 2200 and 2210. It should be investigated on the ground.

Group 7

These grade 1 to 6 anomalies and associated x-type responses indicate a broad conductive horizon which is well defined by the resistivity contours. The anomalies of this grouping reflect bedrock conductors with some magnetic correlation. Generally, they appear to have a northerly dip. This group continues into Sheet 7.

Anomalies 1880C, 2060C, 2280A, 233E, 236A, 236B-238B, 238C These grade 1 to 4 anomalies all reflect probable bedrock conductors of limited strike extent scattered throughout the map sheet. Any of these anomalies could be due to a sulphide source.

#### Sheet 6

Group 5

These grade 1 to 5 anomalies and associated x-type responses represent the continuation of a large conductive horizon from map Sheet 4. Similar to Sheet 4 this group is best defined by the resistivity patterns. Conductors within this group are generally non-magnetic and are dipping to the north.

Anomalies 181C-190B, 183B-189D, 193A-213B, 194B-197E, 196xB-197F, 206B-213C

These grade 1 to 4 anomalies and associated x-type responses reflect a conductive horizon of a large strike length. The horizon is weakly magnetic and appears to be dipping to the north. Any of these responses could be due to a sulphide source. This horizon continues into Sheet 4.

Anomalies 180A-185xD, 181B-182B, 1860A-189B, 184B-192C,

182F-183E

These grade 1 to 4 anomalies and associated x-type responses reflect five bedrock conductors located adjacent to a formational horizon. These anomalies may be attributal to the same source of conductivity as the formational horizon.

Anomalies 190D-191E

These grade 2 and 3 anomalies reflect a non-magnetic bedrock conductor of short strike extent.

Anomaly 191E indicates that the conductor has either folded around to the west or else has terminated between the two flight lines. This conductor should be investigated on the ground.

Groups 8,9

These grade 1 to 3 anomalies and associated x-type responses reflect a series of short strike length anomalies located adjacent to a formational horizon. Any of these

anomalies could be due to a sulphide source. Anomaly 215F, which correlates with a known mineral showing, is of particular interest.

Group 10

These grade 1 to 4 anomalies and associated x-type responses reflect a formational horizon of large areal extent which has strike extensions into Sheet 8.

Conductivity within this group may be due to the same source as group 5.

Anomalies 232A-233A, 232B, 234A-235A, 238A-239B These grade 1 to 3 anomalies
reflect a series of short strike
length bedrock conductors striking
parallel to a magnetic high. Any
of these anomalies could be due to
a sulphide source.

Anomalies 185A,198A, 197I-198D, 212D, 2250A, These grade 1 to 2 anomalies all reflect bedrock responses due to

231A

very short conductors. These anomalies should be investigated on the ground.

#### Sheet 7

Group 7

These grade 1 to 4 anomalies and associated x-type responses indicate a conductive formational horizon that extends into Sheet 5. This horizon appears to dip to the north.

Anomalies 243C-259C, 266B-268B, 270B-272C These grade 1 to 4 anomalies
reflect an intermittently
conductive formational horizon.
Magnetic contours indicate that
these anomalies are associated with
a long continuous magnetic high.
These conductors appear to be
dipping to the north.

Anomaly 247C-248C

These grade 4 anomalies reflect a weak (low amplitude) bedrock conductor with associated

magnetite. These anomalies appear to be due to a thin conductor possibly dipping to the north.

Anomalies 261xA-262A, 264A-270A These grade 1 to 5 anomalies and associated x-type responses reflect a conductive horizon located along the flanks of a magnetic high.

Anomaly 269A is of particular interest because of its magnetic correlation and because it appears to be due to a thick bedrock conductor.

Anomalies 276xA-277A, 277xC-279xA, 279B-282A These grade 1 to 4 anomalies and associated x-type responses indicate 3 isolated bedrock conductors. Anomaly 279B is the strongest response and is associated with a broad magnetic high. These conductors may be dipping to the south. They should be investigated on the ground.

Sheet 8

Group 10

The grade 1 to 5 anomalies of this grouping reflect a large conductive horizon which has strike extensions both to the east and west of this map sheet. Any anomalies within this zone could be due to a sulphide source. Resistivity contour patterns indicate that this horizon may consist of two separate bands of conductivity.

Group 11

These grade 1 to 3 anomalies and associated x-type responses reflect a series of bedrock conductors which appear to belong to the same conductive horizon which is best defined by the resistivity patterns. This horizon is located adjacent to a long formational magnetic feature striking parallel to it.

Anomalies 256D-258C, 260C

These grade  ${\bf 1}$  and  ${\bf 2}$  anomalies

reflect a weakly magnetic,
discontinuous bedrock conductor
located adjacent to a large
conductive horizon. These
anomalies should be investigated on
the ground.

Anomalies 275D-2770xA, 279B-282D, 279xD-282xA, 286D-287A, 291B-2930A, 292xB-294D, 293B-296B These grade 1 to 2 anomalies and associated x-type responses reflect a non-magnetic discontinuous conductive horizon. They are all similar in character and may reflect a conductive source similar to group 10.

#### Sheet 9

This sheet constitutes a small, separate area to the east of the flight block presented on sheets 1 to 8. The ground resistivity within this block varies from about 3 ohm-m to in excess of 1,000 ohm-m. The resistivity map is dominated by a group of northeast trending conductive units that lie along the southeast edge of the area and appear to extend beyond the survey boundaries in both the northeast and southwest directions.

The total magnetic field map indicates corresponding northeast structural trends to be present in the area. The banded nature of these features is revealed by the enhanced magnetic map. Three magnetic bands along the southeast side of the area coincide directly with the conductive zone indicated by the resistivity map. Less prominent banding is seen in the rest of the sheet. Note that other smaller conductive zones correlate with the linear magnetic anomalies.

Anomaly 301A-328B

These grade 1 to 4 anomalies

reflect a bedrock conductor which

correlates with a linear 10 to 30

gamma magnetic anomaly over most of

its length. There is indication of

a southeasterly dip at several

locations. The conductor, which

appears to be thick at 305A-308A

and at 311A-314B, may extend

further west. Anomaly 332C may

constitute its northeastern

extension.

Group 12

These grade 1 to 3 anomalies and associated x-type responses reflect a set of parallel bedrock

conductors trending in a northeast direction. The conductors correlate with magnetic anomalies of 25 to 60 gammas.

Anomaly 306C-308C

A non-magnetic bedrock conductor is indicated by these grade 2 and 3 anomalies. It may extend to 310D.

Anomaly 312C-317D

These grade 1 anomalies reflect a thin non-magnetic bedrock conductor which parallels the group 12 conductors.

Anomalies 311xC-319D, 321D-337C, 329xB-335xA, 336xA-337B These grade 1 to 4 anomalies and x-type responses reflect a series of magnetic bedrock conductors which appear to be part of a single conductive feature.

Anomaly 319A-320A

These grade 2 and 3 anomalies
reflect a slightly magnetic bedrock
conductor of a short strike
length. The conductor, which
occurs about 300 m west of

301A-328B, appears to be an attractive exploration target.

Anomaly 320D-323E

A magnetic bedrock conductor is indicated by these grade 2 and 3 anomalies. Anomaly 322E indicates a bedrock source of a thickness greater than 10 m.

Anomalies 314A-317A, 319xA-323A, 323xA-324A, 325B-355A, 327A-332xA

These grade 1 and 2 anomalies and x-type responses appear to reflect a pair of discontinuous conductors. The northern end of 325B-335A correlates with a 10 to 15 gamma linear magnetic anomaly and indicates a dip to the southeast.

Anomalies 324E-329xD, 327D-331xB, 328E-329xE These grade 1 and 2 anomalies
reflect a set of parallel
non-magnetic bedrock conductors
which occur along the same
northeasterly trend as the other
linear features within the area.

Anomaly 337A-340xD

This short linear grade 2 and 3 weakly magnetic bedrock conductor appears to dip to the southeast. It strikes slightly north of the deneral northeast trend of the area.

Anomaly 340xC-341A

This grade 1 anomaly reflects a non-magnetic bedrock conductor which may extend beyond the survey boundary. It may be related to conductor 337A-340xD.

Respectfully submitted, DIGHEM LIMITED

S. Kilty Geophysicist

Z. Dvorak Vice-President

Thirty-six map sheets accompany this report.

Electromagnetics Resistivity Enhanced magnetics Magnetics

9 map sheets

9 map sheets

9 map sheets

9 map sheets

#### APPENDIXA

### THE FLIGHT RECORD AND PATH RECOVERY

Both analog and digital flight records are produced. The analog profiles are recorded on green chart paper in the aircraft during the survey. The digital profiles are generated later by computer and plotted on electrostatic chart paper at 1:15,000 or at map scale, whichever is larger. The digital profiles, which may be displayed, are as follows:

Channel Number	<u>Parameter</u>	Scale units/mm
20	magnetics	10 gamma
	bird height	3 m
	vertical coaxial coil-pair inphase (freq #1)	1 ppm
23	vertical coaxial coil-pair quadrature (freq #1)	1 ppm
24	horizontal coplanar coil-pair inphase (freq #2)	1 ppm
25	horizontal coplanar coil-pair quadrature (freq #2)	1 ppm
	VLF-EM total field	1 %
	VLF-EM vertical quadrature	1 %
28	ambient noise monitor (coaxial receiver)	1 ppm
	ambient noise monitor (coplanar receiver)	1 ppm
33	difference function inphase from channels 22 and 24	1 ppm
34	difference function quadrature from channels 23 and 25	1 ppm
35	first anomaly recognition function	1 ppm
36	second anomaly recognition function	1 ppm
	conductance	1 mho
	log resistivity (at freq #2)	.03 decade
41	apparent depth or thickness (at freq #2)	3 m
42	conductivity contrast (at freq #2)	arbitrary
	depth contrast (at freq #2)	arbitrary
	product 42*43 (at freq #2)	arbitrary
	log resistivity (at freq #1)	.03 decade
46	apparent depth or thickness (at freg #1)	3 m
47	conductivity contrast (at freq #1)	arbitrary
	depth contrast (at freq #1)	arbitrary
	product 47*48 (at freq #1)	arbitrary
50	apparent weight percent magnetite	0.25%

The log resistivity scale of 0.03 decade/mm means that the resistivity changes by an order of magnitude in 33 mm. The resistivities at 0, 33, 67 and 100 mm up from the bottom of the chart are respectively 1, 10, 100 and 1000 ohm-m.

The fiducial marks on the flight records represent points on the ground which were recovered from camera film. Continuous photographic coverage allowed accurate photo-path recovery locations for the fiducials, which were then plotted on the geophysical maps to provide the track of the aircraft.

The fiducial locations on both the flight records and flight path maps were examined by a computer for unusual helicopter speed changes. Such changes may denote an error in flight path recovery. The resulting flight path locations therefore reflect a more stringent checking than is provided by standard flight path recovery techniques.

The following brief description of DIGHEMII illustrates the information content of the various profiles\*.

<sup>\*</sup>For a detailed description, see D.C. Fraser, Geophysics, v.44, p.1367-1394.

## Single-frequency surveying

The DIGHEMII system has two transmitter coils which are mounted at right angles to each other. Both coils transmit at approximately the same frequency. (This frequency is given in the Introduction.) Thus, the system provides two completely independent surveys at one pass. In addition, the digital profiles (generated by computer) include an inphase channel and a quadrature channel which essentially are free of the response of conductive overburden. Also, the EM channels may indicate whether the conductor is thin (e.g., less than 3 m), or has a substantial width (e.g., greater than 10 m). Further, the EM channels include channels of resistivity, apparent depth and conductance. A minimum of 14 EM channels are provided. The DIGHEMII system gives information in one pass which cannot be obtained by any other airborne or ground EM technique.

Figure Al shows a  ${\rm DIGHEM^{II}}$  flight profile over a conductive ore body in Australia. It will serve to identify the majority of the available channels.

Channels 20 and 21 are respectively the magnetics and the EM bird height. Channels 22 and 23 are the inphase and quadrature of the coaxial coil-pair. This coil-pair is



Fig. A1 DIGHEM $^{\overline{\parallel}}$  digital profile.

equivalent to the standard coil-pair of all inphasequadrature airborne EM systems. Channels 24 and 25 are the inphase and quadrature of the additional coplanar coil-pair.

Channels 33 and 34 are inphase and quadrature difference functions of the coaxial and coplanar channels. The difference channels tend to be free from the response of conductive overburden. Channel 37 is the conductance. The conductance channel essentially is an automatic anomaly picker calibrated in conductance units of mhos; it is triggered by the anomaly recognition functions shown as channels 35, 36, and 42.

Channel 40 is the resistivity, which is derived from the coplanar channels 24 and 25. The resistivity channel 40 yields data which can be contoured, and so the DIGHEMII system yields a resistivity contour map in addition to an electromagnetic map, a magnetic contour map, and an enhanced magnetic contour map. The enhanced magnetic contour map is similar to the filtered magnetic map discussed by Fraser.\*

<sup>\*</sup>Cdn. Inst. Mng., Bull., April 1974.

Channel 41 is the depth channel. A depth estimate which is negative will occur when conductive overburden exists. A negative depth estimate implies that the conductive material occurs above the daylight surface. This false estimate shows that the EM system has responded to the conductive surface material and had also sensed the underlying resistive rock. In Fig. Al, the positive depth estimate of about 100 m is close to the true depth for this bedrock conductor.

Channel 42 is the conductivity contrast which highlights resistivity lows. Channel 43 is the depth contrast,
which usually is not plotted. Both channels 42 and 43 tend
to yield positive responses over bedrock conductors at
depth. Channel 44 is the multiple of channels 42\*43.

Consequently, channel 44 tends to yield large positive
responses over bedrock conductors at depth. The interpretation of channels 42 and 44 has to be done with care,
however, because they may also respond in a similar fashion
to a local thickening in conductive cover, e.g., over a
buried river channel.

Channel 50 provides an estimate of the percent by weight of magnetite. This computation is made whenever

the coplanar inphase channel 24 is negative. The negative response shows that magnetic permeability exists.

## Dual-frequency surveying

For surveys flown primarily for resistivity mapping, as opposed to EM surveying, the two transmitter coils may be energized at two well-separated frequencies (e.g., 900 and 3600 Hz). Apparent resistivity maps can be made independently for each frequency. The interpretation procedure involves comparing the apparent resistivity and apparent depth parameters at the two frequencies.

The use of two different coil-pair orientations (i.e., coaxial and coplanar) for dual-frequency resistivity mapping is an unorthodox procedure. However, as long as the current flow patterns are primarily horizontal, the different coil orientations do not influence the results. Wire fences and other cultural features will produce local deviations, because they usually respond preferentially to one or the other of the coil-pairs.

The difference channels 33 and 34, and the anomaly recognition channel 35, are not produced for dual frequence surveys. This is because the divergent frequencies of the two coil-pairs render them meaningless.

# APPENDIX B

EM Anomaly List

	KABB BB			ANAR IL		V ERT			ZONTAL BET	DONOS EAR	CTIVE TH
LINE 6 ANDMALY		04U) 244	FEAL PFM	CAU2 MAS	•	00N5 4H3S			DEPTH M		
1 A 1 E 1 C 1 E 1 T	27 10 13 2	15 7 3 3	53 27 57 4	37 14 20 10		39	0 . 3 . 3 . 1 9 .	5 10 1	54 59 63 62 51	20 8 2 2 95 1 59	30 39 49 12 3
14 20 20 21 21 21	29 29 12 9 3	21 27 20 3 7 5	40 25 22 23 14 11	3 4 4 9 3 3 1 2 3	•	17 6 6 27 7	6 . 0 . 16 . 25 .	2 4 2	49 47 76 93	57 34 49 10 37 51	27 20 16 55 60 66
3 A 3 C 3 C	2 5 12 12	2 7 11 10	3 18 23 39	5 27 17 23		5 6 12 17	17 . 5 . 19 . 15 .	2 2	34 40 79 52	188 - 43 45 12	27 3 44 42
44 48 40 45 46	1 1 1 2 33	2 7 5 3 2 5	4 4 3 7 109	3 5 5 5 9	•	2 2	1 . 12 . 31 .	1 1 2	152 103 103 122 33	148 111 70 47	8 9 5 2 6 0 8 6 2 0
5 A 5 E 5 C 5 C	1 19 23 8	3 9 12 13	2 45 83 25	4 13 23 24	•	34 47 9	0 .		136 96 46 43	16 1	42 67 33 15
6 A 6 E 6 E 6 E	5 1 14 5 6	4 1 13 4 1	5 20 15 4	3 3 9 13 7	•	15	12 . 31 . 0 . 0 .	1 2 2	55 120 97 45 67	209 86 50 33 69	15 70 59 14 26

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE DECAUSE THE STRONGER PART .

CF THE CONDUCTOR MAY BE DEEPER OR TO DNE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

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LIME & ANDMALY	FEAL	C 4U J M 4°		C A L C		SE NE AR OS		· ·	MHC S	DEPTH N		
74 78 70 70	13 3 1 3	15 5 1 5	28 5 4 2	27 3 5 15	•		4 5 27 0	•	1 3 2 2	54 129 86 59	5 <b>1</b> 26 35 49	28 93 54 23
5 A C 3 C	3 10 14 1	11 11 12 10	1 23 13 2	12 29 11 16	•	1 9 13 1	0 3 0	•	1 4 1 1	45 67 101 64	840 11 82 1035	0 4 4 5 5 0
9 E 9 C	5 3 8	9 3 3	4 125	12 93	•	3 2 0	11		1 6	52 32	6 51 4	9 1 3
104 108 108 108	7 5 5 1 3 5	14 49 6 7	3 126 16	2 2 6 2 3 1 0	•	24 25	3 0 10 11	•	1 4 1 1	48 41 120 103	363 10 106 178	1 24 67 45
114 115 110 110 115 11F	7 13 14 2 5 2	11 19 24 5 7	11 22 22 4 8	23 25 41 2 11	•	8 <b>6</b> 4	0 0 0 0 17 14	•	1 2 1 1 1	35 68 36 129 67 146	£30 59 265 112 150 158	0 30 0 73 22 84
124 126 12C 12C 12F 12F 12G	2 27 19 4 1 6 3	3 2 2 1 6 2 4 3 2	5 44 26 5 2 4 3	3 55 25 1 2 14 5	•	15 21 1 4	0 3 5	•	4 2 2 1 1 1	175 46 70 194 172 61 112	16 31 52 1035 1035 224 83	140 19 33 0 0 14 64
134 136 13C	15 10 7	1 5 7 2 0	24 19 5	25 16 21	•	13	3 0 0	•	1 1 1	55 69 39	32 37 277	19 42 0

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE SECAUSE THE STRONGER PART .

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LINE & ANOMALY			FEAL			CENE			COND SOHM	DEPTH M		
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144 148 140 140	4 5 3 4	13 21 12	5 4 7 2	5 12 21 15	•	5 2 3 2	17 5 0 0	•	1 1 1 1	48 67 80 59	673 721 278 654	0 9 9
154 150 150 150 156 156	2 1 5 1 41 15 3	1 2 2 1 5 8 1 1 2 3 1 5 8	2 1 11 13 70 18 15	3 2 <b>7</b> 1 1 2 5 2 3 1 4	•	2 + B 7 + 5 5	0 11 1 0 0 3	•	1 1 1 5 4 1 1	51 90 86 75 53	588 302 1035 9 11 103 73	0 35 0 62 62 32 22
1 5 Å 1 5 C 1 5 C 1 5 E 1 6 E 1 6 G 1 6 H 1 6 J	1 2 3 6 3 9 11 6 21 1 3	7 988855957	1 2 22 114 69 41 9 25	10 120 125 54 75 3 45 3	•	1 2 1 17 21 5 9 7	1 4 0 3 5 4 12 1 0	•	1 1 2 3 3 2 1 1 1	91 39 60 40 65 41 126 48 122 58	1035 818 35 15 21 34 110 91 1035 312	0 30 20 42 16 72 14 0
17A 17E 17C 17D 17E 17F	15 23 15 8 26 30	20 19 10 7 22 33	36 40 27 26 29 41	35 28 18 13 55 4	•	10 17 18 14 12 11	1 5 15 5 4	•	2 1 3 3 1 2	46 32 90 66 49 47	42 93 21 17 104 42	16 39 63 42 13 17
13A 13B 13C	3 5 46	9 5 5 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1	3 13 56	13 11 23	•	2 10 50	8 1 9 3	•	1 1 3	75 95	65 16	3 5 6 3

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

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LINE S YLAMGUA	REAL PPM	CAU) Maq	PPM	CAUD	•	00 NO 80 HP	ЭЕРТН# М		C 3 N D M H S S	DEPTH M	RESIS CHM-M	DEPTH M
155	52	3 5	£ 4	5.5	•	22	0	•	2	49	3 <b>1</b>	22
194 195 190 190 195	2 5 13 2 16 5	7 3 4 2 2 4 1 2	5 7 11 7 12 7	15 7 4 4 24 15	•	4 3 0 0 0 0 0 0	0 28 5 17 9		1 1 2 3 1	54 93 154 116 68 61	146 99 39 18 188 194	20 46 112 84 24 17
204 208 200 200 208 206 206	3 1 2 27 12 17	14 3 5 6 1 10 6	5 4 3 6 4 4 6	16 2 5 9 5 16	•	2 4 2 3 <b>7</b> 2 5 2 3 2	54 25 5	•	1 1 1 3 2 9 3	56 94 36 117 71 72 102	231 1035 316 23 1	13 0 31 85 64 56 45
21A 21E 21C 21D 21E	5 10 2 40 4	9 9 2 3 0 5	12 10 0 40 8	23 9 0 41 10	•	4 10 7 17 6	2 13 61 3 27	•	1 1 1	65 110 149 59	97 90 1035 95 212	23 61 0 22 43
22 <b>A</b> 22E 22C 22C 22E	11 3 1 25 8	20 21 7 16 12	21 14 0 31		•	6 2 1 22 5	1 4 0 1 0	•	1 1 1 2 1	57 53 146 77 41	54	21 20 0 39
23A 238 23C 23D	3 2 17 7	10 3 19 9	3 5 18 9	9 9 17 11		2 3 10 6	8 18 15 7	•	1 1 1	62 84 87 71	173	11 33 33 31
244 245	10 10	8 9	14 25	1 3 2 3	•	9 11	2 2 1 3		1 2	64 58	163 28	23 39

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

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255 250 250 255 255 256 256	2 4 6 6 3 2 6	13 6 13 17 2 7 22	5 4 2 1 3 2	26 5 17 15 9 12 30	•	2 4 2 2 7 1 4	19 0 4 34	•	1 1 1 1 2 1	32 61 22 50 100 94	211 278 647 692 51 207 69	0 11 0 0 62 38 23
265 265 265 265 265 265 256 256	5 2 0 2 1 2 5 4	13 13 27 5 17	9 6 2 2 0 5 4	25 3 5 25 2 19	•	3 7 1 9 2 2 8	0 5	•	1 1 1 1 1 1	45 72 51 118 115 52 149	205 187 807 76 1035 341 1035	5 24 0 73 0 4 0
27A 27i 27C 27C 27C 27E 27F 27G	59 25 1 19 3 3 5	24 23 10 19 5 9	93 38 2 24 1 0	55 23 7 20 1 3	•	34 17 1 12 3 2 6	4 17 0 8 23 5	•	3 1 2 1 1	58 71 68 93 125 92 31	18 16 304 46 1035 830 89	35 49 15 57 0 1 36
23A 238 23C 23C 23E	E 7 23 2 7 3	64 29 5 17 5	95 27 0 6 2	7 2 3 5 1 1 3 5	•	26 9 1 3	3 6 7 3 11	•	3 1 1 1	56 71 141 72 142	16 32 1035 160 129	34 32 0 27 63
294 295	29 45		63 68	8 <b>7</b> 4 4	•	9 22	3 1		2 3	39 52	2 E 2 Z	14 37

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OF OVERBURDEN EFFECTS.

	CEAX:		582L.		•	VEFT		-,	ZCNTAL SEET	CENEU EAR	CTIVE TH
LINE S ANDMALY	REAL	CAU PFM	FEAL PPM	C A D D P P M	•	4F 3S	•*HT93C • M	MHCS	D EPTH N	FESIS CHM-M	DEPTH M
290 290 298	24 1 4	27 4 9	41 1 1	4 0 0 5	•	12 2 2	1 • 25 • 8 •	2 1	79 159 93	33 95 <b>7</b> 22 <b>2</b>	48 19 38
3 0 E 3 0 C 3 0 C	14 47 3 5 1 2 11 8 6	15 37 9 13 4 9 2 15	36 81 0 11 0 23 5	45 3 5 3 + 8 5 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•	9 3 4 4 5 4 4	2 . 0 . 6 . 13 . 11 . 18 . 7	3 1 1 1 1 2	44 53 51 93 154 123 125 30	25 21 1035 1035 1035 1035 20 328 153	19 28 0 40 0 93 27 33
51A 31E 31C 31C 31E 21F	6 8 3 3 8 8	7 9 11 4 10	3 5 0 1 5	13 12 7 3 10	•	6 6 1 2 6	13 11 0 23 6	. 1 . 1	59 102 91 112 95	220 164 638 867 109	12 47 9 3 46
31A 32E 32C 32D 32E	4 23 4 2 4	7 19 5 8 4	10 19 2 2 2	13 22 4 5	•	5	13 0 15 0	. 1 . 1	81 62 179 141 120	60 73 1035 121 170	4 2 2 2 0 8 5 5 8
33A 33E 33C 33D	4 2 5 5 1 4	7 2 0 3 1 2	5 44 2 11	13 27 7 11	•	16 3 11	_	1 2 1 1	56 125	379 33 147 92	4 36 67 60
24A 24C 24C 24C 24C	2 23 2 2 2	4 2 5 2 3 7	3 3 8 5 3 2 5	7 4 9 2 9 8	•	10 12 2	2 - 4 9 - 0 -	. 1 . 2 . 2 . 1	57 153 87	£04 35 44 309 15	0 23 112 31 82

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART.

CF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	004X 00		00°L		•	VERT CI		•		ZONTAL BET	CENEU EAR	CTIVE TH
LINE & ANEMALY	REAL PPM	CAUJ Mag	REAL PPM	C4U2 M49		CDNE MH D3	DEPTH#. M .		CACC ZOHY	DEPTH N	RESIS CHM-M	DEPTH M
35A 35E 35C 35C 35C 35C	3 31 3 4 0 3	8 9 M 5 4 6	3 4 4 3 3 5	11 41 2 5 0	•	2 15 8 4 2	4 0 4 5 5 5 1 4 6 6 6 6	•	1 2 1 1	56 57 213 114 140 75	615 24 59 194 149	0 41 162 52 79 31
3 6 C 3 6 C 3 6 C 3 6 C 3 6 F	3 47 1 2 2 5	9 2 5 4 8 9	5 9 <b>7</b> 0 0 4 2	11 32 3 3 4 7	•	52 7 1 1 2 4	7 2 3 7 17	•	1 4 2 1 1	34 80 160 124 32 38	704 8 711 210 320 107	0 50 39 53 25 42
374 371	5 34	11 15	5 8 <b>7</b>	14 15	•	3 7 £	5 <b>7</b>	•	1 20	5 <b>7</b> 5 <b>8</b>	110	2 <i>5</i> 4 <i>9</i>
33A 335 330	21 15 17	43 17 16	27 25 19	51 13 17	•	6 12 12	2 12 3	•	1 2 1	5 <b>1</b> 90 90	60 51 61	20 53 42
3 9 A 2 9 E	ŝ <b>1</b> 5	15 10	15 34	2 1 2 3	•	5 17	12 4		1 2	54 80	90 39	26 45
40A 40B 40C 40D 40E 40F	2 2 1 11 2 2	5 4 5 18 7 6	7 7 1 16 4 2	11 8 1 19 3	•	3 4 2 6 2 2	19 23 20 3 0	•	1 2 1 1 1	39 110 116 73 87 111	33 49 249 38 215 581	45 72 54 31 32 25
414 418 410 410	2 1 15 5	7 9 19 6	5 5 29 10	3 12 23 4	•	3 2 9 9	11 0 0 16	•	1 1 2 2	91 63 50 131	63 87 33 35	50 21 30 94

<sup>.#</sup> ESTIMATED DEPTH MAY BE UNRELIABLE EECALSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	acix ac		00 PL :		•	V ERT O I		•		ZONTAL Bet	CCNEU EAR	
LINE & A WOMALY	F EAL PPM	CAU, MAS	PEAL PPM	CAUD	•	CENE MH J S	DEPTH#		COND S BHM	DEPTH M	FESIS CHM-M	DEPTH M
42F 42E 42C 42C	14 22 0 2	2 4 2 7 5 4	3 4 3 4 0 2	£1 £7 2 3	•	7 10 1 2	4 1 16 23	•	2 2 1 1	53 63 162 133	40 35 1035 1035	2 4 3 3 0 0
434 438 430 430 43E	15 3 1 15 2	13 13 6 23	2+ 16 0 24 2	35 17 4 50 4	•	8 6 1 5 2	10 0 0 3	•	2 2 1 2 1	46 77 68 54 171	40 51 412 49 147	16 41 10 23 107
4+A 4+E 4+C 4+C 4+E	20 8 15 5 2	15 17 20 7	42 10 52 4	35 15 52 4 3	•	16 5 11 6 2	0 10 0 32 13	•	3 1 1	57 82 31 93 133	17 95 14 778 1035	35 40 11 8 0
45 <i>k</i> 45E 45C 45C	11 10 3 2	11 15 9 5	14 53 4 1	23 35 7 1	•	2	1 9 0 4	•	1 5 1 1	48 60 123 200	63 7 158 1035	13 42 63 0
455 455 460 405 46F	2 2 0 1 3 4 2 0 7	30 7 16 2 15 10	31 3 47 0 21 2	5 2 5 2 5 0 1 5 7	•	8 1 19 10 16 4	5 9 0 71 0 15	•	1 1 5 1 2	39 69 55 157 93 120	42	10 22 36 0 58 0
47A 47E	11 10	8 2 <b>0</b>	19 12	23 21	•	11 5	3 13		1 1	44 72	59 140	11 30
4 8 A 4 8 B 4 8 C 4 8 D	113 4 5 21	72 15 20 35	196 0 11 33	106 17 25 52	•	2 3	5 0	•	5 1 1	47 53 62 44	7 143 117 53	3 2 2 4 2 3 1 4

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STPONGER PART .

DE THE CUNDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR DECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

702 SH1 LEKKEN

	CE AX		50 PL 00		•	- +		•		ZONTAL EET	SENDU EAR	CTIVE TH
LINE & ANEMALY	FEAL	C 4 U J P F M	FEAL PPM	CAU 2 M 3 S	•	SCHE	082 <b>7</b> 8% M		C D N D S D M H C S	CEPTH M	RESIS CHN-M	DEPTH M
435	4	13	1	7	•	Ž	2	•	1	3 €	1035	0
498 498 498 498 498 498 498	8 30 50 7 32 14 7	12 22 24 20 7	29 74 79 17 61 15	2 2 2 2 3 3 4	•	8 29 52 5 27 18 7	1 0 0 2 3 4 1.5	•	3 5 1 4 1	40 51 53 70 54 97 110	18 16 6 52 13 86 152	17 39 36 32 43 50 54
504 505 505 506 506 506	21 66 83 3 25 15	43 41 40 9 20 22 19	32 139 137 25 56	79 71 54 24 34 16 10	•	5 37 52 7 21 5 4	2 0 0 17 5 14	•	2 5 2 4 1 1	35 47 41 58 59 30 73	35 7 7 24 9 257 191	11 31 25 32 40 30 24
51A 518 51C 51D 51E 51F	10 68 0 4 2	2 2 5 <del>9</del> 6 2 5 2 0	9 97 0 8 2 7	12 71 6 5	•	4 22 1 12 2 3	10 5 0 25 6	•	1 4 1 1 1	46 49 99 93 134 58	227 8 108 99 341 501	5 33 50 44 55
5 2 A 5 2 B 5 2 C 5 2 B 5 2 B 5 2 F 5 2 G	13 78 1 23 0 3	19 63 13 23 7 13	14 99 4 51 1 4 2	11 83 25 41 7 15	•	8 22 1 13 1 2 2	13 0 0	•	1 2 1 2 1 1	49 50 54 72 82 59	129 25 96 38 731 266 633	14 26 28 42 0 7

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

DE THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	X A G Q 3 G		3€ 35 30		•	V BRIT		•		IONTAL EET	CENEU EAR	CTIVE TH
LINE & ANDMALY	REAL PPM	C A D A P P M	FEAL PPM	CAUS Mas	•	SENE	DEPTH# M		C A C D Z D P M	DEPTH M	RESIS CHM-M	DEPTH M
53A 53B 53C 53D	39 61 3 20	29 7 9 16	5 2 6 5 0 2 9	53 23 21	•	17 119 2 16	_	•	3 7 1 2	54 58 95 77	18 4 95 27	31 43 49 49
5 4 E 5 4 E 5 4 E	54 73 21 2	4 9 4 9 2 2 7	114 101 30 2	5.7 6.2 2.5 4	•	20 31 12 2	9 0 10 9 3	•	4 5 2 1	46 42 73 150	9 5 3 <b>7</b> 1035	3 0 2 6 4 1 0
554 552 550 550 555	54 9 1 21 3	46 41 3 26 5	114 185 0 33 0	8 6 6 3 3 5 5 S	•	22 5 1 11 2	4 0 8 6 1 4	•	5 9 1 2 1	49 39 103 64 131	5 2 9 <b>7</b> 45 958	34 23 56 32 9
5 6 A 5 6 C 5 6 D 5 6 E 5 6 G 5 6 G	6 5 7 5 0 2 2 5 3 3 3	43 60 34 11 64 5	165 166 53 33 2 3	132 72 54 23 7 2	•	2 2 3 4 E E	3 7 6 11 24 15 29	•	5 3 5 1 1 1	31 59 44 58 92 138 98	7 2 7 86 1011 1035 93	19 46 29 21 0 0
57A 578 57C 57D	14 9 21 5	17 24 19 12	20 33 6 3	31 39 11 15	•	8 5 10 4	0 7 6 5	•	2 3 3	52 57 51 68	53 15 22 75	18 35 26 29
5 5 6 C 5 5 6 C 5 6 C 5 6 C 5 6 C 5 6 C 5 6 C 5 6 C	47 56 41 22 1 23 3	42 85 43 21 11 30 3	121 103 49 47 11 33 1	79 141 50 27 10 45 0	•	23 11 14 17 3 6 1	9 2 C 8 4 5 4 4 1 2 4	•	5 3 3 4 1 1 1	41 42 37 36 70 45 125 100	5 13 16 10 57 85 785 210	28 23 17 64 35 17 4

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE SECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO UNE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	004X		SCPL S <b>c</b>	ANAE IL		V EFT E I	I CAL	•		ZONTAL Bet	U D N D C E A R	CTIVE TH
LINE S ANDMALY				C 4U 2 M 4 9		CD NE MHOS				DEPTH M		
594 596 590 595 595	3 4 5 0 9 2 7 1	12 26 12 23 4	42 77 9 45 1	20 43 21 41 3	•	44 34 5 15	4 0 0 0 0 0 0	•	3 3 4 3 1	52 44 65 54 128	16 14 13 17 1035	30 24 42 31 0
60E 60E 60E	20 126 63 50	5 8 3 2	18 249 70 78	3 5 1 2 5 4 0 9 2	•	7 55 35 14	6 1 3 5	•	1 7 5 3	47 38 64 43	158 3 7 18	9 25 46 22
614 618 610 615 61F	29 109 14 37 1	5 2 1 5 3 8	50 161 14 82	74 63 17 63	•	9 17	1 0 7 0 4	•	2 4 2 3 1	45 38 79 50 82	47 9 32 22 290	17 22 48 25 29
62A 62b 62D 62D 62F 62G 62H	1 87 39 84 1 2	11 55 65 7 54	1 134 56 142 2 0 2	1 6 7 9 7 3 1 4 1 5 1	•	1 34 9 17 1 2 9	4 0 5 3 9 6 3 2 3	•	1 5 2 3 1 1		857 7 40 12 177 82 1035	0 26 27 25 68 131
638 630 638 638 638 638 631	3 13 17 18 115 2 3	35 40 36	14 16 2	17 36 49 11 71 5	•	4 13	3 5 18 0 14 6	•	1 1 1 1 1 5 1 1	43 44 62 60 35 117 94 114	181 95 64 145 1 110 120 202	5 13 29 18 26 65 46 57
£4‡ £+5 £+0	20 2 <b>7</b> 45	2 3 2 1 3 5	37 40 58	5 7 4 1 4 4	•		0 0 1		2 2 4	30 61 54	46 33 12	1 31 35

<sup>\*</sup> ESTIMATEL CEPTH MAY BE UNRELIABLE BECAUSE THE STPONGER PART.

CF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

702 SHZ LOKKEN

	SDAX SE	IAL IL	C G P L C C			VERT DI	ke .		ZCNTAL EET	CONEL EAR	CTIVE TH
LINE E PARTMENT		CAU) Maq	FEAL PPM	CAUP Mag		CC ND MH DS	GEPTH*. M		DEPTH M	FESIS CHM-M	DEPTH M
645 645 645 646	62 62 2 2	54 54 54	157 129 2 1	73 73 10 5		32 27 1 2	0 . 0 . 5 . 1 .	1	3C 37 100 115	3 2 135 93	13 25 50 65
6 5 5 0 0 0 5 5 F	43 23 13 52 189 0	5 3 2 7 2 7 6 6 8 3	97 25 25 161 327 7	154 35 35 140 157 7	•	ε 1 ε	9 . 9 . 9 . 9 . 9 . 9 . 9 . 9	3 7	23 71 64 32 24 113	16 31 22 3 1	4 42 33 20 15 63
# E C D E F E F E F E F E F E F E F E F E F E	2 2 54 17 26 41 2 3	14 34 25 05 66	3 73 10 54 111 1 5	20 55 45 12 51 64 3	•	1 27 8 13 25 13	0 . 5 . 0 . 5 . 1 . 27 .	1 1 5 1 1 5	39 52 51 54 53 41 83 80	314 269 6 251 79 4 263 131	0 14 34 3 18 27 31 36
67E 67E 67C 67C 67E 67G 67I	4 82 161 102 181 16 2	23 79 63 76 98 13 12	0 167 212 245 328 5 2	19 111 111 150 183 9 11	•	2 5 5 3 5 1 0 1 9	5 · 1 · 0 · 0 · 0 · 15 · 0 · 5 · ·	1 5 10 5 10 1 1	47 43 49 36 24 88 57	214 5 2 6 1 180 630 180	9 29 38 23 15 37 0
3 A B C C C C C C C C C C C C C C C C C C	0 26 30 25 5 25 25 25	4 2 2 2 7 3 0 7 1 1 5	0 30 46 33 14 5 7	1 20 36 34 14 13 7	•	1 16 17 11 7 2 7	18 · 5 · 0 · 5 · 13 · 0 · 7 · 19 ·	1 2 2 2 1 1 1 2	8 & 67 61 64 9 & 61 65 144	1035 30 35 48 94 116 72 52	0 38 30 31 51 19 24

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STPONGER PART.

OF THE CONDUCTOR MAY BE DEEPER OF TO DNE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

702 SH2 LOKKEN

	4433 30	I/L IL		ANAR IL	•		TICAL .		ZENTAL	CENEU Ear	JCTIVE RTH
LINE S ANCMALY	REAL	C AUJ M AQ	F E A L PPM	QUAD PPM	•		DEPTH#.	2 3 HM	C EPTH M	FESIS CHM-M	DEPTH M
694 695 695 695 697 697 697	3 3 3 7 0 7 1 25	27 24 29 13 4 5 9	20 54 76 12 4 3 33	4 9 5 5 5 8 1 0 1 5 7 1 6 2 0	•	1 8 6	0 . 0 . 10 . 17 . 29 .	1 2 1 1 1 1	4C 58 53 54 57 101 39 78	81 16 36 32 426 324 233 84	10 37 24 25 -9 41 0 36
7 0 A 7 0 E 7 0 C 7 0 E 7 0 E 7 0 F 7 0 G 7 0 H	5 22 16 22 10 3 13	15 15 20 25 11 5 13	4 25 26 33 11 3 11	15 21 21 24 14 3	•	12 10 13 7 19 5	3 · 2 · 3 · 6 · 12 · 25 · 0 · 21 · .	1211212	43 46 51 67 87 96 94 164	2 24 34 1 51 61 47 1 77 65 22	0 17 11 31 51 44 52 128
71A 71E 71C 71D 71E 71G 71H 71I	8 57 79 23 0 39 9	19 50 44 32 1 21 6	1 163 112 40 3 26 24	23 97 43 40 0 21 17	•	2 1 2 2 2 4 3 8 2 1 2 2 4 3 8	2 · 5 · 1 · 0 · 8 · 4 · 13 · 0	1 7 1 2 1 1 3 2	40 43 16 42 132 75 76 88	739 375 33 148 36 17 31	0 30 0 15 120 34 51 55
72A 72B 72C 72D 72E 72F	29 5 20 36 23 11	29 11 19 33 5	5 4 3 4 5 6 3 3 3	44 13 35 54 8	•	15 4 14 15 52 11	2 . 6 . 3 . 5 . 8 .	3 1 1 3 2	73 63 52 53 34 109	25 89 69 20 19 41	45 24 18 30 57
73A 73E 73C 73E	4 7 4 11	11 17 19 25	5 19 12 22	6 26 38 30	•	(a) (a) (a) (b)	13. 0. 0.	1 2 1 2	41 48 35 54	4 8 5 5 1 1 2 1 4 6	0 16 2 22

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CCAXI		00 PL 3		•	VERTI DII			712 Sh E	ONTAL ET	SENBUI EAR	
LINE & PHEMALY	REAL PPM	Q 4U 2 PF 4	FEAL PPM	CAU) Mag		.0 N.D. NE 3.S.	OEPTH#.			DEPTH M	FESIS CHM-M	HT93C M
73F 73G	7 7	3 2	5 10	<del>3</del> 5	•	11 26	12 .		1 2	106 97	20 <b>1</b> 68	45 53
748 748 748 748 748 748	41 21 3 + 3 4	11 (4 (1 H) 5	75 19 11 15 1	8 0 8 5 1 8 4 2		1 8 (4 (5) 4 (6)	0 . 0 . 0 . 2 .		7- 4- 1- 4- 1- 4-	51 56 38 44 74 159	28 59 132 87 1035 122	25 22 4 10 0 100
752 752 750 751	75 21 0 11	2 9 2 5 2 6 1 4	142 44 3 4	2 9 4 0 4 6 3	•	76 12 1 6	3 1 0 0 8	•	3 2 1 1	67 49 52 75	15 29 164 246	45 21 11 24
756 750 750 756	0 5 19 20	3 2 2 4 2 3	0 11 63 17	4 23 72 13	•	1 3 8 24	0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 ·	•	1 1 3 2	74 25 52 31	530 155 13 33	10 0 32 50
774 778 778	7 10 7	2 2 4 3 4	3 3 6	2 ) 6 5 5	•	3 4 14	5	•	1 2 1	54 38 103	132 38 413	14 10 31
78A 78E 78C 78D 78F	25 115 35 0	2 2 7 2 1 2 5 4	145 70 0	4 2 E 2 5 4 4	•	10 38 31 1	9 3 14 20 20	•	1 4 7 1	49 46 62 116 127	105 9 3 1035 118	16 30 43 0 72
79A 79E 79C 79E 79E 73F	15 18 45 51 14	27 15	23 111 141 22	59 37 102 65 13	•	57 1E2420 9	4 5 3 0 13 10	•	1 1 2 9 2 1	47 54 46 36 78 102	80 105 48 2 49 205	16 18 17 25 42 44

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIF OR OVERBURDEN EFFECTS.

702 5 12 LEKNEN

	004X 00		CCPL:		•	VERT LI		•		ICNTAL EET	CENEU E#R	
LINE & ANDMALY	REAL	CAU) M49	FEAL	QUAD PFM		DE NE MH BS	DEPTH#		C A B D Z O H M	C EPTH M	FESIS EHM-M	DEPTH M
79G 79r	3 4	1 i 5	1 4	15 15	•	2 3	0 9	•	1	58 43	243 132	21 2
30 A 30 C 30 C 30 C 80 C 80 C	71 67 30 15 6	49 50 40 13 9	103 135 69 2 26	75 119 86 8 10 50	•	26 23 11 12 10	0 0 4 3 2	•	4 5 2 2 1 2	54 59 40 98 54 6	11 7 19 45 109 37	35 24 13 62 16 17
814 818 810 818 81F 81G 61H	114 4 82 25 0 5 2 4	119 66 31 43 36 4	196 4 153 58 0 30 37 5	190 15 137 73 6 20 10 31	•	21 23 11 1 38 5	4 1 2 0 9 3 4 5 0	•	4 1 3 3 1 2 1 2 3	50 55 28 32 82 58 64 33 71	11 136 14 13 1035 51 150 33	3 2 2 0 9 1 2 0 3 3 1 8 3
843 820 827 827 827 827 820	7 213 107 0 50 8 15	12 179 75 1 23 11 23	10 356 253 1 49 3	14 353 145 22 23 40	•	5 2 8 4 0 1 3 3 4 6	1 1	•	1 5 7 1 3 1 1	71 21 25 139 59 53 68	100 4 1 1035 15 220 250	30 9 15 0 28 8
63A 835 63C 63E 83G	4 16 35 9 13	11 9 15 4 5	8 Z 4		•	45 16 33	1 0 2 <del>9</del>	•	5	77 53 57 211 170	730 5 5 401 1035	4 35 40 88 0
844 840 840	3 4 3 5	4 17 65		14	•	÷ ;	17		1 1 2	93 58 32	85 60 38	4 <b>7</b> 25 9

<sup>\*\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONJUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	004X 00	IAL IL	00 PL :		•	V E F T C I	I C # L	•		ZENTAL EET	CENDU Ear	CTIVE TH
LINE & YLAMONA		CUFD MAG	FEAL PPM	CUAD PFM	•	SC 4D SC HM	DEPTH# M			C EPTH M	FESIS CHM-M	DEPTH M
84E 84G	0 4 0	3 2 0	0 5 0	1 22	•	4 3 €	5 5		1 2	193 70	1035	0 41
\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	6 7 14 12 12 0 58 2	22 15 21 23 19 5 16 3	12 13 23 23 20 8 3	40 15 42 42 37 21 4	•	3 7 7 7 7 93 4			1 2 2 1 2 1 9 1	21 52 56 46 52 33 71 92	127 53 46 57 29 1035 2	0 29 26 17 24 0 57
6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 12 199 75	7 10 127 152 23	6 5 5 4 8 5 8 3	11 3 287 374 47	•	2 2 4 9	19 14 0 0	•	1 1 4 6 3	71 58 29 24 61	202 274 9 4 18	20 11 14 13 37
874 87E 87C 87C	73 48 116 79	46 43 161 24	119 116 248 102	83 86 312 60	•		0 3 0 3	•	UN UN UN UN	45 42 22 55	6 7 5 7	30 27 9 33
263 263 366 263 263	17 14 94 115 10	13 13 100 51 5	13 29 198 170 27	13 42 172 73 14	•	ε 21 56	2 2 9 0 1 1 0	•	1 2 5 3 10	35 50 32 59 36	85 29 4 19 2	44 24 20 36 20
898 898 898 896 896	1 19 163 10 133		0 74 236 29 255	1 73 357 12 189	•	26 33	63 15 3 0	•	1 4 3 9 8	64 57 26 63 21	404 11 11 2 2	12 39 12 47 11
468	3	7	ź	13	•	2	2.3	•	1	72	169	3 0

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	4435 30		30 <b>21</b>		•	V ERT BI		•		ZONTAL BET	CONDU EAR	CTIVE TH
LINE 1 ANEMALY	REAL	G Q Q Q M q q	PEAL	QUAD PPM	•	COND MH OS	DERTH*		COND MHES	DEPTH M	RESIS CHM-M	DEPTH M
900 900 900 900 900 900 900 900 900 900	4 5 5 6 14 103	11 21 86 5 3 76	5 20 141 21 17 221	18 46 177 2 10 159	•	22 18	Ö .	•	1 1 4 3 3 8	70 46 38 112 98 24	171 32 10 1 22 2	27 17 22 106 71 13
914 910 910 916 91F	3 6 3 6 3	5 9 9 5 4 1	97 12 3 52 5141	113 21 17 102 4 72	•	4 1 4 6 38	1 1 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	3 1 1 2 5 9	41 57 52 36 163 32	12 70 139 27 10 2	22 21 24 13 132 21
92A 928 920 92D 92E 92F	11 171 2 3 3 147	13 101 3 4 1 173	23 297 5 7 7 270	24 219 5 4 4 335	•	S → C 4 E 14	7 0 5 1 3 3 4 3	•	1 3 1 1 5	64 31 106 211 127 21	70 2 125 517 78 4	26 20 57 78 80 9
93A 93E 93C 93E	75 3 91	12 93 5 95	16 154 5 171	19 180 2 177	•	15 5 19	5 1 2 1 0	•	1 4 4 7	63 33 133 25	3 6 8 1 4 3	24 18 150 14
948 948 940 945 945 946 946	6 9 3 8 7 4 9 3 3	9 13 7 16 4 27 25	14 19 4 20 12 61 87	23 23 4 21 3 59 44	•	14 14 31	20 7 33 9 27 0	•	1 2 1 2 13 6 7	54 73 91 56 149 38 35	67 40 75 45 1 5	30 41 51 33 136 23 23
954 952 95 <b>0</b>	12 5 0	21 3 2	15 3 4	23	•	. 5 . 1è	6 33 34	•	2 1 4	54 202 48	51 119 12	3 0 144 25

<sup>...</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	4435 30	IAL IL	SSPL	ANAE IL	•	V EFT				ZONTAL Eet	SENEU E <b>a</b> r	CTIVE TH
2 ENIL YLAMONA	REAL	C JL D PF M	FE4L PPM	C 4 U P M 4 S		4F 3S	DEP <b>T</b> HX M		C 3 D F 4	DEPTH	RESIS CHM-M	
95C 55E	3 15	2 12	3 3 <b>7</b>	1 3 2	•		53 10		4	49 48	13	29 31
9 5 A 9 5 B 9 5 C 9 5 B 9 5 B 9 5 G	2 3 5 2 14 17	12 5 13 4 24 13	2 3 12 13 41 41	14 14 10 4 17 5	•	2 3 10 7	2 2 7 3 2 0 2	•	1 1 1 9 2 2	45 107 54 135 34 44	573 240 83 3 22 28	2 53 20 116 10 18
97A 97E 97C	5 3 45	1 0 1 5 3	6 3 33	11 1 89	•	25	3 12 3		1 1 1	72 183 42	121 1035 75	27 0 15
9 8 8 C 9 8 8 C 9 8 8 F	1 2 21 1 7	12 5 37 1	3 4 <b>7</b> 3 5	21 3 57 1 20	•	2 10	11 17 12 49	•	1 1 3 1 1	50 62 54 135 43	150 299 20 517 131	2 2 1 5 4 0 5 5
9 9 Å 9 9 £ 9 9 <b>C</b>	5 7 2	4 4 11	7 7 0	4 1 2 3	•	8	1 0 3 0	•	5 1 1	154 43 75	6 198 403	127 0 17
100A 100E 103C 100E 100F	7 3 8 11 9	1 5 12 5 13	16 8 3 9	35 19 2 22 2	•	10	7 14 25 1 33	•	1 1 1 1	59 75 211 32 53	171 104 1035 143 291	1 8 3 6 0 0 5
102E 102 <b>C</b>	0 5	5 4	0 2	1 9	•	,	<b>4</b> 4 5		1	21é 19	1035 699	0 0
103E 103D	10 5	1 4 7	8 6	23	•	5	11		1 3	77 114	105	3 5 9 <b>1</b>

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	X A C C 3 2		00PL		•	VERT	K E I C a F	•		ZENTAL EET	CENEU E <b>a</b> r	CTIVE TH
LINE & ANCMALY	PEAL PPM	CAUD	FEAL PPM	C 4UC M 4G	•	COND MHOS	Э <b>⊆</b> РТ∺¥ М		CACO Zahm	DEPTH M	RESIS CHM-M	DEPTH M
1648 164 <b>0</b> 1640 1647	3 2 5 5	4 2 2 2	6 1 6 2	21 3 1 3	•	1 3 1 1 8	0 42 32 13	•	1 1 3 1	37 204 167 49	212 1035 17 295	0 0 152 0
1055 1050 1050	1 1 5	3 7 0	, 6 0 2	3 5 4	•	2 1 23	2.3 0 2.7	•	2 1 2	92 105 185	52 858 43	51 0 139
105E 105C 106D	2 1 3	3 3 5	5 0 0	12 2 0	•	2	2 2 3 0 0	•	1 1 1	47 112 154	244 1035 1035	5 0 0
107A 107& 107C 107D	2 5 0 1	7 5 0 2	0 6 6 6	4 2 4 7	•	3740	5 0 1 0	•	1 1 5 2	112 178 131 107	1035 1035 9 34	0 0 101 63
108A 108E 108C 108C	0 15 4 3	14 11 5	0 3 0 8	3 0 5	•	1 11 4 8	0000	•	1 1 1 2	75 158 131 84	1035 1035 1035 60	0 0 0 4 3
109A 109B 109C 109E 109F	1 1 9 1 3	2 3 13 7 3	19 7 7 3 7	21 10 2 2 2	•	6 3 7 2 14	3 2 2 3 0 0	•	2 1 4 1	87 81 161 115 157	34 92 14 81 1035	56 38 127 67 0
110A 110E	0 6	9	0	5 4	•	1 13	0 2 5		1 1	67 113	63 <b>8</b> 152	) 55
111A 111C 111C	20 4 2	19 5 9	64 4 12	47 3 15	•	17 5 3	5 4 0 1 2	•	5 1 1	56 118 77	7 1035 66	3 8 0 3 8

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OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

702 SH2 LEKKEN

	XA 33 30		53 <b>°L</b> 30		•	V E F T E I				ZENTAL Bet	C C N C U E A R	CTIVE TH
LINE & ANDMALY	REAL	GAU) Mac	REAL PPM	CAD	•	CONE MH DS	DEPTH M		CACO	E EPTH N	RESIS CHM-M	DEPTH M
1115	1	4	2	ó	•	1	0	•	1	173	1035	0
112A 1128	25 5	2 4 3	<b>7</b> <del>9</del> 2	£ <del>4</del> 2	•	17 59	0 2 <b>2</b>	•	5 2	40 172	8 43	24 125
1134 1136 1130 1136 1137 1136 1137 1131	4 1 4 5 2 10 3 5 2 2	3 2 1 6 3 5 10 11 8	3 5 19 3 5 6 12 41 7	12 0 9 1 5 7 15 14	•	29 29 20 4 6 21 3 3	9 6 0 6 0 0 0 5 5	• • • • • • • • • • • • • • • • • • • •	41 01 4 11 4 15 41 21 61 21	53 151 91 142 91 126 85 81 84	873 31 12 77 11 10 82 50 21 45	0 123 66 95 66 95 21 54 48
1145 1146 1146 1147 1146 1148 1141 1141	2 3 4 4 5 17 44 7	1 5 3 5 14 23 18	7 0 9 9 0 21 60 5 6	1 1 1 3 4 2 4 2 2 2 1	•	6 2 5 14 4 11 32 27	45 9 9 22 15 7		2 1 1 2 1 2 2 1 1	127 32 58 119 94 86 75 52	49 1035 177 36 737 49 41 178 981	83 0 12 81 2 51 42 13

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CUNBUCTER MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	004X 00		CE PL CC		•	vest EI			ZONTAL BET	CONDU EAR	CTIVE TH
LINE & ANDMALY	REAL PPM	CALO	FEAL PPM	CAU2 M 4 9	•		DEPTH#.	COND	E EPTH M	FESIS CHM-M	DEPTH M
115A 115B 115C	4 2 4	6 5 2	0 9 3	1 13 10	•	Ø. <b>(3)</b>	0 . 21 . 22 .	1 1 1	109 66 64	278 111 850	40 28 0
1154 1158 1150	<b>0</b> 0 3	5 1 2 8	0 2 1	1 1 0	•	1 1 2	) . 0 . 0 .	1 1 1	164 107 111	1035 292 £77	9 4 <u>1</u> 0
117A 117E	ć ć	5	2 2	9 ÷	•	13	7 . 24 .	1	136 116	207 1035	9 5 0
113A 113E 113C	2 1 9	1 7	1 1 2	3 4 5	•	<b>4</b> 14 W	27 . 20 . 0 .	1 1 1	78 134 183	1035 1035 1035	0 0 0
119A 119E 119C	1 3 5	5 6 3	0 3 1	0 1 2	•	1 12 ε	0 • 0 • 29 •	1 1 1	153 144 113	1035 815 1035	0 4 0
120A 120E	2 4	0 3	5	5 0	•	14 13	43 . 15 .	2 1	112 177	53 1035	74 0
121E 121C	<b>11</b> 9	2 <b>7</b> 3	3 <b>1</b> 2	6 5 2	•	5 26	3 · 20 ·	2 1	49 170	46 126	20 109
122A 122E 122C	8 3 0	9 14 5	2 0 1 0	1 7 1 1	•	10 1 1	0 . 0 . 3 .	2 1 1	77 154 227	39 298 1035	43 44 0
1234 1238 1230 1230 1231	1 1 9 5	3 5 2 4 6	1 0 15 4 2	0 4 24 5 0	•	2 1 4 8 2	19 . 0 . 0 . 0 . 2 .	1 1 1 1	193 72 54 163 143	1035 1035 142 1035 1035	0 0 16 0 0

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART.

OF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	004X) 00		00 PL #		•	VERT LI		•		ZONTAL Eet	CONEU E <b>a</b> r	CTIVE TH
EINE & YUAMBUA	REAL	C AU ) M 4 9	FEAL	CAUÇ Maq		CONE MH CS	DEPTH* M		COND	C EPTH.	RESIS CHM-M	DEPTH M
1248 1240 1248 1248	1 3 9 5	2 2 1 7 5	7 7 11 2	5 5 14 1	•	4 4 5 7	16 35 0 0	•	1 1 1 1	118 103 80 154	1035 89 67 119	0 5 6 3 9 9 6
1154 1258	4 4	<b>7</b> 5	· 7	15 3	•	4 &	9 2 0		1	56 113	156 74	13 68
1268 1268 1260 1260	5 5 4 0	2 9 3 1	1 1 2 4	4 4 0 0	•	11 4 13 8	11 25 0 83	•	1 1 2 2	35 115 156 208	269 25 <b>7</b> 36 29	21 54 112 163
127# 127E 127C 127E	6 3 4 0	6 5 3 7	5 2 2 0	15 4 1 7	•	4 3 9 1	11 32 9		1 1 1	45 115 105 59	237 152 128 1035	0 60 47 0
125E 126C 123D 123E	2 17 6 4	4 24 1 3	5 26 7 0	9 25 2 0	•	3 9 5 9 5 9	2 0 4 9 3 2	•	1 2 5 1	33 75 125 138	92 28 8 1035	39 46 98 0
129A 129B 129C	3 4 10	8 6 3	13 0 3	1 á 3 3	•	7 3 23	19 19 0	•	1 1 2	65 131 164	122 220 43	24 67 113
130A 130B	2	7 7	ó 4	10	•	2	1 0	•	1	54 162	173 523	11 31
131A 131D 131E	4 4 5	11 7 7			•	6) (1) (2)	9	•	1 2 1	39 91 99	125 50 197	3 53 33

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART.

DE THE CUNDUCTOR MAY BE DEEPER OR TO DNE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR EVERBURDEN EFFECTS.

	CLAX CD		SCPL		•	V ERT DI			PIZ SHE	CNTAL ET	CONEU EAR	CTIVE TH
LINE & ANEMALY	REAL	QUAD PPM	FEAL	C4U9 M4e		CEND MHDS	OEPTH#.			DEPTH M	RESIS CHM-M	DEPTH M
132E 132C 132D	1 5 12	4 11 10	9 11 9	11 20 2	•	3 4 16	11 0	•	2 1 4	53 46 131	55 58 11	25 10 59
1334 1335 1330 1330	7 5 15	3 7 2 7 0	18 13 21 3	3 5 2 9 2 5 1	•	5 6 7 11	4 19 15 60		1 2 1 2	41 86 82 197	55 39 34 59	10 52 43 146
1344 1346 1340 1340	7 3 13 5	10 11 26 5	2 6 1 0 2 1 3	31 19 23 0	•	7 5 8 10	4 5 12 0	•	2 2 1	78 59 35 143	55 44 70 96	41 26 45 87
155A 135E 135C 135C 135E	4 0 0 0	5 17 17 5 1	7 14 14 3 4	14 25 25 3 2	•	4 2 2 2 11	3) 3) 10	• • •	2 1 3 1	52 28 124 85 143	55 887 21 1035 98	13 0 94 0 91
136# 130ē 136C	4 7 12	5 8 4	12 16 4	20 11 1	•	5 9 2 <b>1</b>	10 25 0	•	2 1 4	74 95 152	38 63 <b>1</b> 5	41 55 117
1378 1370 1370 1378	1 8 8 12	4 9 14 10	1 14 10 5	13 20 26 3	•	1 6 4 12	0 13 7 17	•	1 1 1	103 47 56 160	390 116 119 476	41 11 18 57
138A 138E 138C 138D	6 7 3 23	1 10 9		1 19 5	•	40 7 3 27	68 5 0	•	1 1 1	66 44 75 175	1035 123 1035 1035	0 7 0 0
139A •	4	10	17	3 0	•	4	0	•	1	78 DNGER P	7C •	36

<sup>\*\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

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	004X 00		CEPL CE		•	V EPT DI				ZENTAL Est	CONEU EAR	CTIVE TH
S ENIL YLAMGMA	REAL PPM	G 4 U J M 4 G	REAL PPM	CAU) Mag	•	DONE MRGS	DE PT H來。 M	•	COND MHCS	D EPTH M	RESIS CHM-M	HTGEC M
139E 139C 129D 139E 139F 139C	3 1 12 3 7 0	10 9 25 4 3 4	17 3 4 7 0	31 9 1 6 9 11	•	4 1 11 14 6 1	0 0 0 42 32 6	•	2 1 2 1 1	44 60 180 104 118 54	45 584 44 542 1035 1035	13 0 134 23 0
1405 1400 1405 1405 1406 1406	15 23 27 34 13	7 27 27 43 13	32 115 116 5 1	19 76 76 3 3	•	23 22 22 13 4	0 .	•	2 5 4 1 1 1	58 75 29 194 204 197	29/ 8 10 401 207 517	29 55 13 71 113 64
1414 1415 1410 1410 1417	10 24 3 0 4	12 14 2 5	15 57 0 0	26 33 1	•	6 23 4 1 3	0 5 4 2 0 0	•	2 4 1 1	49 56 210 203 173	51 11 1035 1035 78	15 35 0 0 119
142A 1428	2 9	1 3	<del>9</del> 2 <i>5</i>	5 7	•	16 45	25 12	•	3 5	82 99	26 <b>7</b>	51 77
143E 143C	5 3	13	<del>9</del> 35	1 1 1 0	•	4 54	<b>0</b> 5	•	2 6	3 0 77	49 5	<b>42</b> 58
144A 144E 144C 144E 144G	4 3 3 2 6	5 4 5 6 0	11 9 1 1 4	18 9 4 1 3	•	2 2 17	0 2 13 5	•	2 3 1 1 1	63 73 96 192 147	30 17 268 1035 1035	33 46 33 0
145A 145E 145C 145C	10 10 5 3	20 5 10 12	16 17 1 3	13 3 9 23	•		12 13 10	•	2 3 1 1	74 116 35 209	31 21 1035 1035	44 84 0 0

<sup>\*\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE SECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO DNE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	65.4X 30		632L 38		•		ICAL Ke	•		ZONTAL Bet	CONEU EAR	CTIVE TH
LINE & ANDMALY	PEAL PPM	CAUS	FEAL PPM	CAU2 MAG	•	CONE SC 4M	*HT930 M		COND ZOHM	C EPTH M	FESIS CHM-M	DEP <b>T</b> H M
1452	22	16	3	7	•	13	0	•	1	119	207	29
145A 145E	15 4 9	8 5 25	22 14 10	14 5 3	•	19 12 4	0 4 0		2 3 2	53 100 125	39 24 47	20 67 85
1460 1460 1465 1465	ე ე ე	5 5 3	1 0 13	10 8 9	•	1 1 6 21	0 0 3 5 0	•	1 1 3	81 148 117 127	949 1035 22 1035	0 0 8 <b>7</b> 0
146G 146h 146I	7 2 2	2 10 10	1 0 7	5 1 1	•	5 5	5 5	•	11	65 177	2 1035	6 9 0
1474 1475 1475 1475 1475 1476	2 3 19 9 0	7 5 11 9 2 5	9 12 1 3 3	19 19 19 19 2	•	2 4 10 4 2 3	0 5 6 0	•	1 1 4 4 1 2	41 67 170 168 137 28	314 64 13 14 1006 34	0 30 137 135 18
147r 143A 143E 143C	3 3 11	5 4 2 5 1 5	11 3 2 2	15 3 5 9	•	£ 4 1 5	17 0 0	•	1 1 1	99 66 172 175	1035 156 1035 1035	17 0 0
149A 149B 149C 149D	4 5 2 1	6 8 7 19	11 13 1 5	13 21 15 8	•	6 5 1 1	2 4 1 5 6 0	•	1 2 1 2	51 53 44 118	1 94 55 351 33	17 29 3 75
150A 150E 150C 150D 150E 150F	2 2 0 0 13 10	4 0 3 3 19	5 7 2 2 3 3	3 4 3 9 0 1	•	5 14 7 7 7	15 33 51 43 0	•	1 2 1 1 1	102 81 139 89 176 161	34 36 1035 374 87 645	54 49 0 31 122 19

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	4433 30		55 PL 66		•	V EF T L I		•		ZCNTAL EET	CONCU EAR	CTIVE TH
LINE & ANDMALY	REAL	C A L J M A A	FEAL PFM	CAUD Mag	•	CEND	‡Η <b>Τ</b> ΡΞΕ <b>Μ</b>	•	COND MHDS	DEPTH M	RESIS CHM-M	DEPTH M
151A 151B 151C 151C 151E 151F	5 2 4 0 1 2 5 0	21 32 3 26	4 47 6 5 1	27 59 4 55 9	•	2 10 3 4 9	7 8 26 25 0 12 33	•	1 1 2 2 1 1	21 49 118 131 131 216 92	68 <b>7</b> 54 44 48 1035 1035	0 19 82 91 0
1516 151H 151I 151J 151K 151N	0 0 2 17 14 15	4 4 2 7 20 7	1 6 2 5 1 3	12 12 9 15 15 4	•	5 7 20 10 30		•	1 1 3 7	1 2 2 1 9 0 7 1 4 5 1 5 7	1035 1035 1035 26 4	0 0 3 <b>7</b> 24 0
1524 1525 1520 1520 1525 1527	5 4 2 5 5 2 4	2 6 8 1 6 3	9 9 5 3 0 4	2 5 7 17	•	32 7 2 24 3 18	14	•	2 2 1 2 1 1	104 75 81 194 67 18	52 54 164 65 1035 1035	65 41 33 142 0
153A 153B 153C 153D 153F 153G 153H	5 1 20 16 3	12 7 3 15 1 14	8 3 2 2 4 8 3	31 23 3 7 5 1 4	•	3 4 2 12 205 6 18	0 0	•	1 1 1 7 5 2	54 51 78 177 108 129 210	282 100 359 401 4 9	10 14 19 54 85 99 160
154A 154E 154C 154C 154C 154C 154C 154C 154C	5 4 1 1 0 2 2 3 17	3 0 5 1 5 1 5 2 2	9 2 3 5 4 2 1 0 2	1 4 2 4 3 2 1 2 30 2 3	•	7 17 4 3 4 3 3 5	3 19	• • • • • • • • • • • • • • • • • • • •	2 1 3 3 1 1 1	90 93 176 183 205 193 172 168 140	58 91 1035 18 22 1035 1035 1035	50 45 0 148 163 0 0 0

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	IAL IL	83 PL 30		•	V ERT				ZENTAL EET	CONDU E <b>a</b> r	CTIVE
LINE & ANDMALY	REAL PPM	CAU) Mag	FEAL	M 3 d	•	CD NE	DEPTH* M		C AC D Z D H M	TEPTH N	RESIS CHM-M	DEPTH M
155A 155C 155C 155C 155E 155F 155G 155H	3 13 14 1 1 0 4	3 13 12 1 2 4 3 15	14 20 15 9 9 7 24	2 5 1 3 1 9 5 7 7 5 3	•	4 12 11 11 5 4 7	0 14 4 25 13 0	•	1 1 1 1 1 2	49 47 48 59 24 128 90 0	133 143 57 65 1035 1035 20	9 14 23 0 104 0
15 65 15 60 15 60 15 65 15 6H 15 6K 15 6K	14 12 27 6 0 4 0 7	13 16 16 10 2 0 2	3 0 3 4 5 5 2 4 4	3 3 7 1 9 5 4 9 9	•	5 11 3 13 17 12	0 2 4 5 2 <del>6</del> 5	•	2 2 1 1 1 4 3 2	37 97 90 56 113 73 84 168	26 32 45 363 136 579 1	10 62 54 12 61 9 79 115
157A 157C 157C 157C 157E 157F 157H 157J 157J 157K	5 3 3 7 16 0 0 0 4 14	9 5 3 6.5 5 6 3 3 4 <b>9</b> 2	13 7 11 13 25 0 3 10 10	3 4 4 6 2 5 5 5 6 9 9 4 2 6 2 5 5 6 6 9 2 4 6 9 2 6 6 6 9 2 6 6 6 9 2 6 6 6 6 6 6 6	•	4 7 6 12 7 1 1 5 5 4 4	0 0 0 0 0	•	1 2 5 1 1 1 2 1 1	40 46 35 47 71 111 85 100 204 92 167	228 55 7 332 138 922 598 48 1035 1035	0 10 60 0 25 1 11 63 0
1584 1586 1586 1586 1586 1586 1584 1584	2 3 5 9 24 15 3 2	4 7 2 1 6 3 1 3 1 1 7 4	5 15 9 2 7 7 7 7	4 10 10 5 7	•	4 12 13 2 5 8 8 2 3 1		•	3 1 1 1 1 1 1 1 1 1 1 1	144 71 56 74 103 74 69 65 29	20 89 66 78 105 71 149 1035 752	110 30 18 30 49 31 22 0

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CUNDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	26 4 X 30		CC PL		•	V 3P T 2 I		•		ZENTAL EET	CONDU Ear	CTIVE TH
LINE & ANEMALY	R E A L PPM	CAU3 MA9	FEAL PPM	C 4US M 44	•	CC NE	DEPTH≭ M		C J N D S G H M	DEPTH M	FESIS CHM-M	DEPTH M
153K 155M	0 17	4 2 2	0 3	0 2 0	•	71 53	3	•	1	197 60	1035 249	o o
15595959555555555555555555555555555555	2 3 10 1 0 1 5 0 11 5 12 20 1	23931695416004	10 22 3 5 2 2 3 11 2 14 15 0 10 10	98035855352330	•	7 6 6 1 1 1 2 1 7 5 5 2 1 2 3 3	000000000000000000000000000000000000000		2 1 1 1 1 1 2 1 1 1 1	38 53 55 95 123 200 211 139 204 80 145 174	47 44 111 782 304 1035 964 2 1035 697 169 1035 115	5 2 2 2 1 9 5 5 8 0 4 7 1 2 5 0 0 2 5 0 9 7
160A 160B 160C 160C 160C 160C 160C 160C 160C 160C	3 4 1 2 2 3 3 1 3 0 0 1 9 1 3 5 3 4 2	10 15 12 75 15 15 25 15 21 77	30 63 20 17 20 29 16 17 55 1	3 3 3 1 1 2 2 4 9 9 7 6 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		8	17 8 2	•	3 2 1 1 1 1 1 3 1 1 1 2 1 1 1 1 1	41 36 48 77 150 37 218 131 232 47 207 145 158 201 162 120	21 51 153 424 1035 490 1035 1035 1035 1035 1035 115	16 43 9 21 0 0 0 124 0 15 0 102 0 0
161A 161E 161C 161C	11 5 13	5 4 13 2	13 5 17 3	13 1 29 2	•	13	6 0 1 49	•	2 3 2 1	51 120 49 124	56 21 54 210	23 85 15 61

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

CF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	204 <b>X</b> 20		SSPL SS		•	V ERT E I	ICAL KE	•		ZENTAL BET	ODNOU Ear	CTIVE TH
LINE & ANDMALY	REAL PPM	C 4 U J	FEAL PPM	CAU MAG	•	SENE MH 3S	DEPTH≭ M		COND SOHM	C EPTH M	FESIS CHM-M	HT93C M
161E 161F	3 0	3	0 15	2 5 2 3	•	1 10	3 <b>1</b> 5		1 1	51 220	1035 1035	0 0
161G	O	11	. 15	42	•	2	1	•	7	141	4	119
1616	Э	11	13	3 9	•	4	1 4	•	1	53	1035	0
1611	Э	4	15	24	•	3	_	•	11	148 208	2 1035	131 0
161J	2	5 2	3	34	•	4 4	0 0	•	1 1	20 E 59	70	2.5
161K	0	2	14	2.2 2.2	•	4	1	•	19	120	1	110
1618	1	<u>2</u> 2	- 14 14	19	•	8		•	1	217	1035	0
161N 161D	5	9	5	3	•	5	0		2	1 7 9	59	149
151F	7	20	11	3	•	4	0	•	2	67	54	28
1616	5	17	11	3		4	0	•	1	72	1035	0
162A	2	2	0	4	•	4	9	•	3	111	24	76
1622	7	15	4	3	•	4	3	•	2	102	52	6.0
1620	5	11	19	13		7	0	•	5	113	5	8 9
1 é 2 D	31	3 5	3.5	5.5	•	10	11	•	1	51	65	21
1628	4	5	0	Э	•	É		•	1	156	1035	0
1625	1	3	0	3	•	1	0	•	1	216	1035	0
162G	3	5	1	5	•	3 3	21 10	•	1 1	151 128	1035 77	0 8 <b>1</b>
162H	3	3	7	15	•	ۇ د		•	1	193	1035	0
162I	<del>4</del> 3	1 3	4	7 3	•	7	•	•	3	124	25	8 <b>7</b>
162 <b>J</b> 162K	ے 4	5	3 2	5	•	4	D	•	1	96	1 4 C	3.5
162M	0	٥	4	3	•	6	58	•	3	187	21	151
162N	15	24	39	54	•	7	0		1	54	95	18
1620	49	21	12	<b>1</b> 3	•	28	0	•	13	113	1	100
162P	ì	3	5	õ	•	3	3.3	•	2	156	43	124
163A	7	12	9	11	•	5	0	•	1	5 <b>7</b>	137	12
163E	17	1	7	0	•	107	Ö		5	132	6	105
1630	14	15	5	10	•	7	4	•	1	59	245	11
163D	0	2	2	2	•	1	27	•	1	214	107	157
163E	4	4	1	5	•	3	27	•	1	92	1035	0
163F	٥	0	12	4	•	25	_	•	14	150	1	137
163G	3	1	5	1	•	28		•	1	216	645	74
163H	3	10	5	12	•	5	3	•	1	57	245	8
1631	13	5	4	13	•	21	0	•	1 3	115	1035 21	0 54
163J	13	10	4	7	•	16	0	•	5	91	∠ 1	24

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE RECAUSE THE STRONGER PART .

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	4433 30	I/L IL		ANAR IL	•		TOAL .		IZCNTAL HEET	OE NE L E A F	JCTI VE RTH
B BALL YLAMCKA	REAL PPM	CAUS	PEAL PPM	CAUD Mag		COND MH DS	DEPTH#.		DEPTH M	RESIS CHM-M	DEPTH
, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		.,.	•		•		•				
1644	1	13	5	5	•	1	0.	. 1	202	1035	0
164E	5	3	3	5	•	4	0 -	. 1	172	130	111
1 ĕ <b>4 C</b>	5	ó	10	31	•	4	3 •		61	92	23
164D	25	27	23	3.5	•	10	12.		52	73	28
164E	3	4	3	17	•	1	g .		53	1035	0
164F	6	5	1 4	3	•	13	9 <b>.</b> 34 <b>.</b>		175	1035	0
1646	3	1	<u> </u>	5	•	5 18		1	199 210	1035 1035	<b>0</b> 0
164H	2 <del>9</del>	2 4	5 5	0 5	•	13	59 . 14 .	_	210	186	2 9
154I 164J	3	10	1	5	•	1	0.	_	5 <b>6</b> 5 <b>9</b>	279	16
164K	4	3	0	2 O	•	£	0.	_	147	1035	0
1648	20	14	1 5	13	•	ić	0.		125	1035	Ö
1 t 4 N	14	1 4	16	13		11	0.			1	31
					•		•				
165A	2	2	12	õ	•	14	13.	7	108	5	8.5
1655	44	13	5	10	•	3.3	0.	5	97	7	70
165C	8	17	2.0	3.2	•	5	3 .		5 E	<del>5</del> 8	24
1650	13	17	20	3.2	•	7	2 .	1	4 <b>6</b>	95	11
165E	7	. 0	8	5	•	41	35 •		207	46	160
165F	3	7	5	11	•	2	11.		7 E	237	26
1656	2	1	5	3	•	10	31 .		190	1035	0
165H	10 5	11 14	10 4	0 23	•	10 9	0.		119 120	3 1035	100 0
165I 165J	11	14	4	23	•	5	0.	1	132	1035	0
165 <b>G</b>	3	14	9	23	•	1	0.	9	70	3	4 9
165M	3	15	3	11	•	4	0.	1	122	1035	Ö
203.	-				•		•				
166A	3	3	3	5	•	5	o .	2	101	43	5 8
1668	7	7	13	14	•	8	23 .	1	53	139	16
165C	2	3	1	0	•	5	69 .	1	93	314	37
165D	3	5	2	0	•	4	24 •	1	202	1035	0
165E	0	ŝ	0	4	•	1	0 .	1	116	1035	0
				_	•		•				_
167A	7	5	2	2	•	10	0 •	1	138	1035	0
167E	3	4	1	1	•	15 9	5 • 8 •	1 2	178 54	1035 4 <b>7</b>	0
167C	19	21 5	30	44	•	2	15.	1	187	1035	23 0
167D 167E	2	5 1	1 5	3 1	•	15	40.	4	157	1035	130
167F	2	4	3	4	•	3	0.	1	70	431	0
1011	-	7	ر	7	•	_	•	•	, ,		J

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	604 <b>)</b> 66		50 PL 30		•	V E F T	ICAL .		ZONTAL EET	CENEU Ear	CTIVE
LINE & ANGMALY	R EAL PPM	C 4U D M 4 S	FEAL PPM	QUAD PFM		SENE MHDS	DEPTH*. M .		DEPTH M	RESIS CHM-M	DEPTH M
1 £ 7 G	ð	ó	1	1	•	1	0 .	1	217	1035	0
163A 163B 163C 163B 163B 163B 163B	5 3 13 5 0 5 3	11 3 22 5 5	Ó Ó Ó 4 M 4 IO .	3 3 2 5 4 5 <b>1</b> 7	•	57884964	0 . 0 . 13 . 22 . 19 . 11 .	2 1 1 1 1 1 1 3	163 50 76 82 78 60 50	36 487 158 1035 1035 909 269 28	119 0 32 0 0 0 2 91
169h 1690 1690 1695 1696 1696 169M 169N	2 0 2 2 2 7 3 3 3 3 14 3 8 0	1 2 12 17 45 8 0 34 13 6 7	4 3 4 7 3 4 5 5 3 2 14 3	9 057 9 1 4 4 9 4 1 1	•	1 7 2 5 0 6 5 2 4	1 · · · · · · · · · · · · · · · · · · ·	3 1 1 1 7 1 1 1 2	142 844 53 56 118 625 137 125 139	4 419 111 57 538 5 85 474 634 21 59	120 27 16 25 5 96 32 0 35 88
1704 1702 1700 1700 1700 1706	.5 3 9 2 0 1	5 3 14 7 3 7	2 3 11	2 1 2 1 4 5	•	8 7 5 1 5 2	0 . 53 . 12 . 14 . 58 .	2 2 1 1 1	151 222 60 148	59 59 148 1035 1035	100 171 20 0 0
171A 171E 171C 171C 171E 171E 171F	7 2 6 5 1 0 8	3 6 4 11 6 3 7	1 8 8 3 2 3 1	3 10 11 3 3 2 3	•	11 3 9 3 2 2 7	0 . 20 . 12 . 5 . 7 . 0 .	1 1 1 1 2 1	127 37 75 66 104 144 130	1035 227 83 325 1035 40 1035	0 35 32 13 0 99

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	00 A X I		00 PL =			VERT		•		ZONTAL BET	U D M D D R A E	
LINE &	R E A L PPM	CU4D PFM	REAL PPM	SEW CAND		SD NE MH DS	DEPTH# M		COND AHES	C EPTH N	RESIS CHM-M	DEPTH M
172A 172E 172C 172C 172E 172J 172K	3 1 3 2 0 3 6	2 4 3 7 5 14 1	0 5 6 2 0 5 5	0 5 10 7 2 1 2	•	7 2 7 2 1 2 74	8 7 0 0 0	•	1 1 1 1 1 2	162 112 76 67 198 105 125	1035 108 117 690 1035 517	0 59 29 0 0 0
173A 173B 173C 173C 173E 173F 173G 173H 173I 173T	7 21 45 35 10 45 3	1 2 2 0 1 3 3 1 7 7 1 3 7 2 1	021150200255	2 7 3 0 20 20 5 15 12 8 3		4 11 10 2 2 3 1 1 5	0 60 2	•	1 1 1 1 1 1 1 1 1 1 1 1 1	166 177 198 222 38 32 44 35 51 116 104	1035 1035 1035 1035 536 290 1035 940 1035 1035	0 0 0 0 0 0 0 0 9 1
174 <i>F</i> 174 <i>E</i> 174 <i>C</i>	4 2 3	6 5 3	4 1 0	11 5 4	•	3 2 9	19 14 5		1 1 1	74 109 134	191 1002 1035	28 6 0
175A 175B 175C 175E	6 11 4 0	4 16 10 5	17	0 3 2 1 3 2	•	17 6 2 1	6	•	3 1 1 1	137 41 78 230	28 94 1035 1035	148 9 0 0
176A 176E 176C 176C 176D 176E	0 0 20 1 1	0 1 4 7 7	3 26 2 0	3 6 35 10 0 5	•	12	۵ ٥	•	2 2 2 1 1 2	190 40 73 212	36 43 55 320 1035 46	133 144 7 17 0 77

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	CC 4X CC		002L4 001		. v:	ERTI LIK			HERIZ SHB	CNTAL ET	CONDU EAR	TH
LINE & ANDMALY	REAL PPM	CAD Mac	F EAL PFM	CAUQ	. CC		DEPTH#.		C 2 N D S	DEPTH M	RESIS CHM-M	DEPTH M
177A 177E 177C 177D 177E	10 13 3 7 0	15 13 2 21 9	1 12 4 2 0	5 20 1 5 14	•	5 12 1	0 • 3 • 1 5 • 0 • 1 3 •	•	1 1 1 1	196 62 175 168 44	1035 80 1035 1035 992	0 23 0 0
178A 1788 178C 178K 178N 178N	5 7 2 1 1 3 9	3 10 5 6 4 6	1 2 1 0 1 0 1 0 2	3 10 4 2 2 1 13	•	8723655	2 9	•	2 2 1 1 1 2 1	192 72 98 159 68 210 74	50 54 1035 1035 2 107 1035	143 24 0 0 53 153
179A 179E 179C 179D 179G 179h 179I	2 3 5 11 2 11 1	7 7 4 10 5 6	0 1 1 6 6 4 1	0 4 2 13 1 1		4 3 E 7 6 23 1	0 0 0 0	•	1 1 1 1 3 1	72 103 115 51 145 170 193	1035 1035 1011 117 26 130 408	0 0 3 106 109 72
180A 180B 180C 180C 180F 180F 180F 180F	5 10 5 4 0 5 15	7 3 3 2 5 1 2	3 1 0 0 0 0 1	2 1 0 1		3 9 13 6 5 5 11 1	17 50	•	2 1 1 1 1 1 2	59 92 113 92 201 119 90 115	29 95 179 635 1035 645 43	19 45 55 6 0 44 8
161A 181E 161C	5	5	+ 6 7 3 1 1	3	•	11 6 20	0	•	3 1 1	133 141 153	21 1035 1035	9 <b>7</b> 0 0

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	1 <b>4</b> 4 3 3		COPLA CEI			VERTI DIK			ZCNTAL SET	C D NE U E A R	
LINE & ANOMALY	REAL PPM	QUAD PFM	REAL	C 4U D M 4 q		00.00 00.00	OEPTH#.	0.000 2.25	[EPTH N	FESIS CHM-M	DEPTH M
115A 115E 115C 115E 115E 115F 116C 115H	3 6 10 1 15 13 27	4 5 11 5 11 14 7 15	3 5 10 1 39 17	1 0 0 0 13 10 5 25		6 11 12 2 21 11 1 20	14 • 0 • 0 • 2 • 17 • 15 • 2 • •	1 3 3 1 4 2 1 2	109 156 143 193 84 36 103 55	1035 26 17 517 11 38 102 31	0 118 103 60 61 53 54 35
115A 116E 116C 116C 116E 116F 116G	1 2 8 14 14 43 3	5 4 13 15 30 34 15	0 17 22 5 61 19	0 1 19 26 20 45 20	•	14 6 9 4 2 5 2 5	3 . 0 . 10 . 6 . 2 .	1 1 2 1 1 2 1	162 113 67 62 69 50	1035 1035 53 66 163 32 75	0 0 3 2 2 4 2 8 2 2 2 3
1174 1176 1170 1170 1176 1176 1176 1178 1171	2 4 9 5 3 4 9 7 2 5 5 7 5 5 7 5 5 7 5 7 5 7 5 7 5 7 5	7 21 15 6 4 24 11 33 67		1 1 2 31 3 60 41 30 110	•	3 1 4 7 3 4 9 6 1 4 4	14 20 11 3	. 2 . 1 . 3	159 149 158 69 128 59 57 80 37 104	1035 36 1035 43 44 8 53 58 16 209	0 105 0 36 90 42 23 44 17
113A 113E 113C 113E 113E 113F 113G 113H	21 20 12 21 21 02 25 7	7 5 17 17 27 5	2 35 35 51 7 7 11 13	4 0 12 1 22 14 15 92 16	•	12 20 31 23 1 8 23 7	0 0 0 41 4 0 8 0	. 1 . 1 . 3 . 2 . 3	157 70 120 80 91 83 38	1035 964 16 57 25 34 45 6 58	0 0 44 79 53 60 48 23 58

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	054XI 051		SGPLA SCI			VERTI			ZONTAL BET	UBMBB RAE	
LINE & ANDMALY	REAL PFM	CAU) Mag	FEAL PPM	CAUS		COND Cohn	DEPTH#.	COND MHCS	DEPTH ₩	RESIS CHM-M	HT93C M
119A 119E 119C 119E 119E 119F 119C 119H	14 21 3 1 5 4 94 15 7	5 13 4 5 5 5 21 73 10	10 16 0 5 5 9 109 226 3	4 8 1 7 0 15 54 15 11	•	30 15 3 2 3 3 4 4 4	0 0 0 0 18 15 0 0	1 4 1 1 2 1 3 7	124 99 120 93 92 70 50 28	9 65 16 1035 1035 60 60 2 2	0 64 0 9 51 33 33 17
120E 120C 120C 120E 120F 120G 120H 120J 120J 120K	12 1 2 4 1 13 0 31 9	10 9 5 7 0 24 3 21 11 6	5 4 3 3 67 19 35 27 14	4 1 3 2 9 9 9 1 1	•	11 1 3 4 5 11 3 16 8	0 · 0 · 13 · 2 · 6 · 0 · 0 · 0 · 0 · 0 · 10 · 0 · 10 · 0 ·	2 1 1 1 1 3 2 2 1	50 39 40	50 1035 178 376 1035 19 45 30 57 183	93 0 11 0 0 13 13 12 8
121A 121B 121C 121D 121E 121F 121G 121H	3 17 20 9 8 7 9 25 29	1 16 11 4 5 3 20 29	0 3 0 17 16 11 12 58 53	1 19 3 1 21 24 30 167 167	•	<u>-</u>	53 0 0 12 13 15 0	1 3 3 3 1 1 2 2 2	5 164 111 77 55	1035 1035 1035 17 17 71 49 30	0 0 81 52 21 34 15
122A 122E 122C 122E 122E 122F 122C 122C	1 7 3 3 15 5 61 6	3 3 4 0	10 18 7 37 163 186	5 <b>7</b> 125	•	2 5 7 4 5 7 2 5 3 1 1 0	0 13 15 2 9		174 107	1035 1035 8 140 35 14 3	0 82 3 10 37 25 19

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	00 4X 30		30 P <b>L</b> 00		•	VERT		•		ZENTAL EET	SENDS FAE	OCTIVE TH
LINE & YLAMBNA	RIAL PPM	C AU D M R R	FEAL	CAUQ MAG	•	ODND AH OS	≭H TG∃C M		C 4 6 0 Z 3 h M	E EPTH M	PESIS DHM-M	DEPTH M
122I 122 <b>J</b> 122K	71 24 95	8 2 2 6 8 0	150 - 64 368	177 82 303	•	16 11 29	<b>7</b> 0 0	•	4 3 6	37 26 21	10 13 4	21 5 11
123A 123E 123C 123E 123E 123F 123G 123H 123J 123K	0 19 19 0 3 7 6 10 41	3 7 7 6 5 1 2 10 11 22	2 2 0 0 17 30 3 39 136	4 5 11 1 2 5 17 13 23 49	•	8 23 16 1 1 59 26 4 29	0 0 0 1 0 4 7 0 0	•	1 1 1 1 5 4 1 3 4	169 163 175 204 167 119 63 43 28	1035 96 1035 1035 1035 1035 121 18	0 107 0 0 0 93 42 5 6
124A 1240 1240 1240 1240 1246 1246	5 4 4 3 2 3 2 3 2 3 2 5	5 0 3 47 3 19 33	2 11 6 77 32 102 90	4 0 0 89 21 56 105	•	8 635 21 13 46 30 12	0 45 51 0 7 0	•	1 4 1 3 5 6 4	143 125 72 42 31 23 17	1035 12 55 19 4 4	0 99 34 20 16 10
1240A 1240B 1240C 1240D 1240E	4 5 0 130 45	2 0 2 9 3 5 1	1 0 0 295 198	3 0 0 230 212	•	8 14 6 33 17	12 57 33 0	•	1 3 3 7 3	139 31 47 19 18	128 20 15 3 11	79 55 26 9 1
1258 1250 1250 1258 1258 1256 1254	19 4 4 1 35 67 59	18 2 2 5 23 43 52	0 8 3 1 46 165 184	3 3 0 51 113 149	•	8 20 9 2 15 31 23		•	1 2 1 2 3 5 4	146 119 90 74 53 14 24	1035 55 1035 36 22 4	0 7 8 0 4 1 2 8 2 8

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	<b>K</b> ABB <b>B</b> B		00 P <b>L</b>		•	V E F T E I		•	HERI SH	ZONTAL BET	CONDU EAR	CTIVE
LINE & ANDMALY	P EAL OPM	CAU, Maq	REAL PPM	QUAD PFM	•	CEND	w DES1.⊣*		COND	D EFTH M	RESIS CHM-M	DEPTH
1265 1260 1260 1265 1265 1263 1263 1268	15 3 4 1 179 0 94 11	2 2 7 0 5 1 C 7 0 2 7 3 5 2	2 2 7 11 328 328 243 44	6 0 4 24 200 9 81 9	•	11 5 32 3 45 6 98 5	000	•	1 1 2 1 9 4 14 1	99 167 109 57 32 48 27 17	1035 1035 33 92 2 10 1 63 868	0 74 15 22 30 18 0
1274 1278 1270 1270 1278 1276 1276 1274 1271 1273	646520948334912	1 11 5 29 10 40 3	2 7 4 5 4 2 2 1 2 1 2 0 1 5 0 1 2 9	0 3 7 5 1 1 1 6 4 3 2 5	•	78 3 5 10 9 10 6 25 10 133	4 0 2 0 5 23 10 0 71 0		1 1 3 7 3 3 3 3 3 3 3 3 3	1 62 991 564 994 994 998 31	858 1035 25 3 13 17 24 14 18 1	4 0 153 40 25 64 65 22 72 13
1284 1285 1280 1280 1286 1287 1286 1281 1281 1283	10 11 32 109 45 70 2 29 198	12 30 30 32 23 47 12 30 104	0 12 0 327 158 74 165 3 66 342	3 16 10 71 66 23 132 15 60 173 16	•	7 4 12 143 47 43 24 1 15 57	0 0 0 0 5 17 0 0 2	•	1 6 1 4 7 1 1 5 4 1 6 1 2 1	161 140 188 30 43 58 32 58 42 25 133	1035 6 1035 1 6 10 449 5 1	0 115 0 26 33 42 15 6 27 16
129A 129E 129C 129D 129E	2 7 7 15 0	1 5 1 5 3	6 5 14 39 3	1 4 4 17 13	•	20 10 75 36 2	3	•	5 2 13 5 2	151 113 42 55 141	6 32 1 4 28	135 72 28 39 104

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	X A C C	IAL IL	00 PL		•	VERT SI	ICAL . KE .		IZENTAL HEET	CENEL EAF	CTIVE CTH
LINE S ANOMALY	FEAL	C AU J M A G	FEAL	G AUG M 99	•	CENE MH OS	DEP¶H#. M .			FESIS CHM-M	DEP <b>T</b> H M
129F 129G	24 77	13 21	41 180	23 31	•	27 77	3 <b>.</b> 9 <b>.</b>	4 1 7		13	28 13
130A 130E 110D 130E 130F 130G 130H 130J 130K 130M	19 21 5 5 10 20 109 149	57246133905	7 5 12 29 143 9 11 57 311 311	5 2 0 2 5 3 2 2 2 4 7 1 6 3 1 6 3	•	440438413549 14071349	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1	156 67 41 39 99 126 38	1035 39 2 10 1 16 144 45 10 2	0 111 53 20 26 63 42 20 29 27
1314 1315 1310 1310 1317 1317 1317 1318 1318 1318	3 6 10 0 13 10 3 20 174 57	3 3 3 3 7 4 3 5 5 9 2 6 3 3 3	2 1 0 2 2 3 3 6 7 1 3 9 1 3 9	0 2 0 2 5 3 12 27 15 107 59 63		60621 96992150 41	18 · 2 · 0 · 0 · 15 · 0 · 0 · 0 · 0 · 0 · 0	1 1 1 1 1 3 3	132 167 161 170 80 45 83 55 71 41	964 1035 1035 1035 2 1 25 11 59 8 3	17 0 0 0 65 35 55 35 29 19
132A 132E 132C 132C 132C 1320C 1320C 1320E	1 15 15 5 22 21 19 17	1 7 8 7 29 22 4 5	5 0 2 1 18 36 40	5 1 0 1 24 24 9 20		5 25 20 5 6 10 52 34	35 · · · · · · · · · · · · · · · · · · ·	1 1 1 1 2 1 2 5 1 2	195 133 145 157 79 67	92 1035 1035 517 1035 1	59 0 0 12 0 69 59 33

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	X4 3 3 3 3		CCPL:		•	V FRT E I		•		ZONTAL Bet	ODNIU EAR	CTIVE TH
LINE & ANCMALY	R BAL PPM	CAUA MAS	FEAL PPM	QUED PPM	•	08 4D MF 08	DEPTH# M		C D N D S D H M	DEPTH N	FESIS CHM-M	DEPTH M
1320H 1320I 1320J 1320K 1320M	2 29 0 45 41	3 11 5 25 25	0 44 16 125 125	0 20 23 73 79	•	2 40 3 31 30	15 0 14 0 0	•	1 4 2 8 4	141 71 69 33 27	107 12 32 2 9	86 48 39 21 11
1230 1236 1236 1236 1236 123h 1331	3 5 0 3 4 2 3 6 4	5 0 7 15 13 23	7 15 82 32 77 137	2 0 3 2 3 1 4 € 2	•	19 49 157 17 65 54	6 4 2 0 7 7 3	•	3 29 29 3 10	174 82 44 78 72 35	1 & 1 1 22 2 1	138 75 38 53 58 24
134A 134C 134C 134E 134E 134F 134G 134H 134J	3 5 3 9 2 0 0 2 3 1 3 3 2 2 2 3 2 2 2 2 3 2 3 2 2 2 3 2 2 2 2 3 2	4 2 4 5 1 2 5 2 6 3	150 94 1552 619 3133 333	7 7 3 13 27 42 3 153 129 2	•	12 17 9 21 3 1 19 73 63 6	5 1 11 30 1 0 25 0 45	• • • • • • • • • • • • • • • • • • • •	3 5 3 4 1 11 11 15	117 59 92 89 40 33 54 20 23 38	23 6 26 10 71 117 1 1 1035	83 48 60 67 11 3 43 11
135A 135E 135C 135E 135E 135F 135G 135H	3 80 0 14 13 7 24 44	2 27 16 13 14 23 13 29	5 149 30 30 19 21 53 116	1 59 2 27 22 32 34 47 15	•	12 9 4 30 38 1	0 0 5 6 6 <b>1</b> 5 0 0	•	4 15 19 3 2 2 14 14	131 34 50 70 57 65 36 29 45	13 1 14 25 28 1 1	97 24 40 49 31 37 26 19
1368 1360 1368 1368	5 5 6 2 4	9 + 15 7	50 120	3 11 21 3	•	308 10 <b>7</b>	0 0 0 15	•	1 21 13 1	1 2 0 4 8 5 2 6 3	142 1 1 129	57 40 40 19

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	654X 36		00 PL		•	V ERT		•		ZONTAL Eet	CONDU Epr	CTIVE TH
LINE & ANDMALY	REAL PPM	C 4U D N 49	F E A L PPM	C A U Q M 9 S	•	ONGS SCHM	DEPTHX.		C O N D R H D S	DEFTH M	FESIS CHM-M	DEPTH M
136F 136G 136F 136I	23 9 361 29	23 13 121 41	39 0 345 56	3 2 2 2 2 2 3 5 2	•	13 3 30 12	6 0 9	•	2 2 10 3	48 59 26 50	33 39 1 18	20 23 17 28
187A 187B 187B 187E 187E 187G 187H 187I 187J	17 22 0 27 33 18 13 4 66	7 10 2 8 4 6 13 2 2 7 2	13 0 61 79 30 13 37 124	9 4 1 20 16 27 5 27 5 5 4	•	24 17 4 59 164 62 6 51 6		•	5 1 1 15 9 4 2 4 14 1	114 153 225 68 63 76 56 45 34 185	9 1035 1035 1 2 11 36 10 1	83 0 57 43 525 28 20
133A 133E 133E 133E 133H 133H 133J 133K	18 10 2 0 24 8 0 67 7	14 2 5 3 2 6 4 3 7	0 15 91 27 7 183 19	11 7 14 14 10 11 65 54 13	•	8 4 1 9 315 38 48 3 1	0 0 9	•	1 1 41 40 7 2 5 1	119 138 90 35 60 75 105 38 37 41	1035 1035 1035 1 1 4 54 7 140 535	0 0 31 55 53 66 23 2
139A 139C 139D 139E 139F 139G	9 3 4 1 26 28 32	20 11 2 4 7 15 24	10 10 2 0 64 72 78	5 21 4 1 20 45 5	•	5 8 2 57 26 20	0 3 4 4 0 0 0 0	•	10 1 1 2 7 4	113 46 212 169 46 42 43	3 901 858 48 3 9	94 0 54 124 33 24 25
1405 1405 1405	11 4 0	9 10 0	12 0 2	20 13 4	•	ê 1 2	0 2 51	•	11 1 1	86 89 2 <b>17</b>	2 1035 130	69 0 156

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X			ANAR IL	•		ICAL KE	•		ZENTAL EET	ODNO. EAF	CTIVE TH
LINE & ANGMALY	REAL PPM	QUAD PEM	FEAL PPM	CAUD MAS	•	SE NE SC Hr	DEPTH:	* • •	C J N D M H C S	D EPTH M	PESIS CHM-M	DEP <b>T</b> H M
140F 140G 140H 140I 140J 140K 140M	10 6 9 13 12 20 9	12 6 4 3 0 16 29	4 4 10 10 4 4 10 10 4 4 10 10 10 10 10 10 10 10 10 10 10 10 10	31 96 150 54 94	•	14 10 55 25 30 8	5 3 7 19 7 0	•	4 2 13 5 5 4 1	71 106 66 71 74 59 34	9 46 1 8 7 13 65	50 70 54 51 55 39
141A 141C 141C 141E 141F 141F 141C 141H 141I	20 0 3 4 28 12 1	9 50 6 3 11 7	3 5 4 1 3 1 5 5 1 0 3	. 3 44 14 12 4 11 4	•	2 1 6 24 64 19	00005040	•	1 1 1 2 3 7 2	172 45 57 64 84 58 110 68	78 105 627 30 22 3 30 308	118 10 0 34 53 41 79 13
1420A 1420C 1420D 1420E 1420F 1420G 1420H 1420H 1420J 1420J 1420K	3 1 1 1 1 3 0 19 5 5	5 9 1 3 12 11 5 4	5 10 12 7 7 47 4 0 35 3	10 5 17 4 4 19 22 22 13 11 20	•	9 16 9 6 30 1 35 6 3	41 5 7 0 0 6 21	•	2 1 1 3 3 3 1 1 4 3	116 168 42 140 81 75 44 56 75 106 48	74 944 503 17 19 23 224 85 9	70 10 0 109 51 50 0 19 53 73
143A 143E 143C 143C 143E 143F 143G 143H 143H	0 5 10 8 14 13 19 34	2 5 0 3 5 7 2 1 4 6	5316005444 255444 26005444	5 2 2 2 2 2 5 5 5 1 7	•	3 6 2 6 1 6 1 9 9 5 8 3 8	21 4 0 18 0 5 0	•	1 2 7 3 4 2 2 14	201 126 56 69 33 50 53 65	119 56 4 20 12 26 26 26	143 85 37 46 14 25 27 28 47

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	SSAX SS		00°L		•	V ERT DI		•	4831 . Sn	ZCNTAL EET	C C N C U S A S	CTIVE TH
LINE & ANCMALY	REAL	C 4 U # D P 9 9	REAL PPM	CAUD	•	SENE MESS	) 35PT서#. 기		C D N D	DEPTH M	RESIS CHM-M	DEPTH M
144£ 144C 144E 144E 144F 144G 144H 144H 144K 144M	14 0 1 5 12 5 0 17 16 54 76	820272171448 2448	17 42 19 19 11 15 48 13	15 5 1 6 17 14 9 70 107 49 63	•	17 6 16 34 13 7 9 51 44	14 63 57 10 23 02 10	•	21765223177	96 178 99 51 74 70 34 44 41	25 1035 5 8 25 27 19 54 3	65 0 75 79 41 47 43 17 14 33 28
144N 144D 144P	0 0	1 0 6	1 2 2	4 1 1	•	1 7 1	103 0	•	1 1 1	140 204 194	1035 1035 944	0 0 3 5
145A 145B 145C 145D 145E 145E 145F 145G	1 11 3 10 10 282 216 85	.2 7 3 3 9 132 96 46	11 15 18 19 28 353 323 95	5 10 14 5 19 297 169 56	•	11 17 11 55 14 49 65	0 2 4 0 0 3 0	• • • • • • • • • • • • • • • • • • • •	1 2 3 3 4 7 11 5	92 98 30 116 55 28 34 41	210 63 17 15 13 3 1	29 57 53 83 41 13 25 26
146G 145H 146I 146J 146K	20 15 54 83 11	1 8 2 1 3 4 1 4	32 2 <b>7</b> 109 162 28	9 1 8 6 4 8 3 2 2	•	150 20 41 51 10	0 4 21	•	6 3 5 7 5	37 66 47 42 61	5 18 8 3 6	67 42 30 29 44
147A 147E 147C 147D 147E 147E 147F	11 10 3 2 28 47 1	12 5 0 2 5 22 9	10 5 23 93	11 13 2 2 2 3 5 2 4	•	10 128	10 0 35 4 1	•	1 4 5 4 4 7 2	90 64 77 95 66 45 41	70 11 8 14 8 3	48 41 52 68 46 32 7

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE SECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR GVERBURDEN EFFECTS.

	35 A X 36		00 PL -		•	V ERT LI		•		ZENTAL Bet	C D N D U E A R	
LINE & ANOMALY	REAL	k do CAD	FEAL	CAU2 MRS	•	CDND MH DS	DEPTH#		C D C D Z B F M	DEPTH M	FESIS DHM-M	DEPTH M
148A 148B 148C 148D 148E 148E	0 15 10 3 37 18	1 15 1 1 25 12	2 12 25 8 6+ 29	1 14 5 6 49 24	•	5 157 15 21 16	9 <b>7</b> 9 0 3 0	•	1 1 11 5 2 2	1 3 0 8 7 5 3 6 1 5 0 5 7	180 130 2 8 31 30	114 39 38 39 22 23
149A 1490 1490 1490 1490 1490	17 6 3 2 65 93	20 2 2 0 51 79	14 15 3 120 139	13 4 4 103 133	•	8 3 <del>6</del> 2 1 2 2 2 2 2	0	•	1 7 5 4 3	85 61 68 64 45 45	117 4 5 10 16 12	3 9 4 1 4 7 4 1 2 3 2 7
1504	1	3	0	0	•	2	4 5	•	1	2 0 <b>7</b>	1035	0
1500A 1500E 1500C 1500E	15 22 7 16 7	1 8 0 4 1 5 1 7	10 44 11 22 32	13 0 6 31 57	•	8 2000 16 9 5	0 20 15 11	•	2 29 2 2 2	90 50 39 61 50	53 1 28 54 92	52 53 59 28 19
151A 151E 151C 151C 151E 151F 151G	10 0 3 10 8 2	21 4 0 5 6 1 14	17 0 14 8 14 6	2 5 2 3 4 1 5 2 3 2 3	•	1 2000 19 10 2	13 11 0 1 2 14 0	•	1 1 24 6 1 1	41 179 80 62 62 99 43	750 1035 1 5 63 92 742	0 72 60 24 54
152A 152E 152C 152C 152E 152F 152G	3 19 13 13 20	7 0 5 3 21 24 14	11 5 29 26 13 35 6	17 0 11 5 18 33 25	•	805 56	13 13	•	1 10 5 5 1 2	90 103 64 35 70 55 59	82 7 8 176 37 675	45 86 45 63 27 23

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OF THE CONDUCTOR MAY BE DEEPER OF TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	44 35 35		00 PL		•	V ERT				ZONTAL EET	CONDU Ear	CTIVE TH
LINE &	R EAL PPM	GAUJ MAG	F EAL PFM	CAU) Mac		SENE 80 HB	⋨⋸⋑ <b>Т</b> Н∜		COND	DEPTH M	PESIS CHM-M	DEPTH M
1534 1535 1530 1535 1536 1536	5 13 23 6 3 23 23	2 3 1 6 2 1 4 2 3	13 16 36 16 10 39	4 2 1 3 6 6 1 3 5 7 2	•	2 9 194 40 12 8	0 14 0 5 19 6	•	1 13 21 2 2	50 70 55 65 126 49 50	175 154 1 1 47 31 55	9 25 45 57 83 22 21
154C 15445 15445 15446 15447 1544 1544 1548	2 2 2 2 5 9 1 8 1 5 9	7 8 8 4 9 6 6 5 4 3 5 215	14 14 14 2 3 5 0 15 9 100 13	199 199 159 159 153 153 22	•	4 4 3 64 10 11 11 4 24 5		•	1 2 1 1 1 4 3 1 2 1 4	70 67 198 217 74 36 104 103 171 51 60	245 53 107 756 1 16 115 54 295 10	17 32 141 67 61 60 55 63 87 32
1558 1550 155F 155G	10 15 28 17	1 10 35 33	14 28 48 37	1 15 63 52	•	177 20 10 5	0 7 3	•	13 4 2 1	9 C 8 4 5 7 4 2	1 12 28 55	76 60 30 16
156A 156E 156C 156E 156F 156G 156G	0 3 5 15 7 9	4 10 1 9 20 5 15	1 6 12 29 5 21 16	1 15 1 16 22 17 25	•	1 2 139 21 3 15	0	•	1 1 2 1 5 1 2	214 78 58 72 76 78 57	1035 107 1 7 156 35 82	0 36 49 52 32 46 21
1574 1576 1576 1576 1576	0 3 5 4	7 4 2 2 1	4 5 1 2 5	12 3 0 7 1	•	c	7 20 51 26 0	•	1 1 1 1 3	107 81 201 203 104	1035 168 1035 130 20	0 34 0 142 71

ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART.

OF THE CONDUCTOR MAY BE DEEPER OR TO DNE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CE4X		CCPL.		•	VERT LI		•		ZCNTAL EET	CDNDU EAR	CTIVE TH
LINE & ANOMALY	REAL	C 4U D M 9 9	FEAL PPM	CAUS	•	COND MH 3S	DEPTH*		COND	DEPTH M	RESIS CHM-M	DEPTH M
157F 157G 157H 157I 157J 157K 157M	5 0 3 2 1 0 0 3	3 1 2 2 3 2 2 5	3 2 4 8 1 4 2 3	4 0 37 7 2 1 2	•	12 2 20 1 5 2	39 18 2 0 75 62 17	•	2 4 5 1 2 1	115 151 53 120 197 223 201	65 14 7 233 54 119 298	73 120 36 61 151 165 91
1568 1560 1560 1568 1567 1566 1564 1581	3 4 23 10 3 16 4 5	3 2 5 8 2 1 1 9 3 2	7 11 53 47 52 27 0 12	3 2 2 1 2 1 3 0 1 4	•	6 14 46 24 31 12 6 11	2 5 3 0 8 0 1 2 6 2 2 7	•	1 2 3 5 5 7 1 2	115 114 53 42 54 62 95 105	110 47 3 4 20 63 41	63 77 39 27 35 38 55 71
1592 1598 1590 1590 1598	2 2 16 14 26	5 7 12 12 25	0 3 3 4 3 8 3 9	1 13 29 24 27	•	2 15 13 <b>1</b> 3	0 0 0 0 0	•	1 1 4 4 2	159 49 62 59 50	1035 701 12 13 26	0 3 9 4 5 2 3
160A 160E 160E 160E 160F 160G 160H 160T 160K 160M	1 4 7 0 22 0 12 13 30 2	10 14 4 2 7 4 4 6 3 5 7	0 2 0 2 5 0 2 0 4 5 4 7 7	17 25 3 16 0 11 28 43 5 15	•	1 1 2 1 57 6 27 23 13 4 4	30584 30584 3141 0892	•	1 1 1 1 8 1 3 4 2 1 1	38 2118 218 50 98 69 74 47 143 73 84	1028 590 1035 130 3 1035 15 12 25 174 1035 135	0 0 0 157 44 0 44 50 22 80 0
161A 161C	3· 0	2 4 1	13	5 2 4	•	3	4 54		1	44 95	265 55 <b>1</b>	5 2 5

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OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CE 4 X		SSPL		•	V E F T L I		•		DENTAL EET	CONDU EAR	CTIVE TH
LINE & ANGMALY	REAL	CUAD MAG	FEAL PPM	QU4D M46	•	CEND MHOS	DEPTH# M		C D C D Z D H M	DEPTH M	RESIS CHM-M	DEP <b>TH</b> M
161D 161E 161F 161G 161H 161T 161T	16 9 8 17 19 16	3 5 3 7 4 1 3	6 12 15 41 41 7	6 0 8 5 9 + 2 3 0	•	3 16 29 51 150 7	3	•	1665022	15 78 80 76 56 46 134	261 5 5 8 2 24 50	0 59 60 55 41 20 95
162A 162E 162C 162D 162E 162F 162G 162h	2 4 2 0 1 5 3 1 4 4 3 1	3 2 1 3 2 2 7 1 3 4 1 6	2 7 40 5 106 364 4	5 27 20 2 71 25 55	•	2 33 7 32 12 12		•	1 1 5 8 5 5 5 7 1	67 8 54 88 57 50 33 115	461 826 4 3 8 17 170	1 0 47 63 40 43 13 59
163A 163C 163F 163G 163h 163I	3 0 0 33 11 41	15 1 1 7 27 36	10 4 1 61 45 81	2 4 4 2 3 4 3 8	•	8	53 42 12 0		1 2 1 6 4 5	41 197 177 55 49 35	199 55 965 5 8 <b>7</b>	4 150 34 39 30 20
164Å 164E 164D 164D 164E 164E 164F	5 0 0 116 35 20	4 3 9 1 21 31 21	9 1 0 7 197 55 62	14 11 10 5 89 45 66	•	1 5 99 17	5	•	1 1 2 9 5 3	53 19 95 112 35 46 47	213 673 1035 45 2 6 17	12 0 0 77 25 30 25
165A 1650 1650 1650 1655 165F	1 4 0 2 0 7	6 14 3 2 3 1	0 13 1 0 0 7	0 2 3 4 2 2 5	•	1 3 1 4 2 32		•	1 1 1 1 1 4	134 52 153 153 196 132	181 91 917 1035 1035	71 14 25 0 0 102

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, DR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	00 4 X 00		00 PL 00		•	V E F T C I			EET	CENEU Ear	CTIVE
LINE &	REAL PPM	040) M 49	F EAL PPM	CAU2 Mac	•	CEND MH DS	DEPTH#.	COND MHCS	DEPTH N	RESIS EdM-M	DEPTH M
165G 165H 165I	73 22 25	14 25 19	139 56 56	47 65 65	•	103 11 14	0 . 6 . 0 .	9 4 3	3 <b>1</b> 48 32	2 11 14	20 30 12
1668 1666 1666 1666 1666 1666 1666 1666	6 2 12 43 15 60 9 10 0	3 0 19 2 9 22 12 71 17 4	7 20 26 92 36 110 53 2	10 77 27 3 24 24 47 153 31 51	•	60890000 420000 71653	23 4 17 · · · · · · · · · · · · · · · · · ·	1 1 17 5 23 7 3 1	103 97 63 59 52 48 39 38 65 203	147 69 70 1 8 1 3 16 73 1035 87	50 55 29 43 41 26 13 1 43
167E 167E 167F 167G 167H 167L 167J 167K	2 0 24 3 9 21 6	5 2 3 4 13 19	7 2 50 10 14 14 14	1 2 2 1 3 3 4 2 9 2 3 3	•		1 . 70 . 9 . 17 . 11 . 2 . 10 . 50 .	1 1 3 5 3 2 1 1	51 142 52 61 77 53 59 114	161 1035 2 8 25 44 123 101	3 7 40 47 20 23 63
168A 168E 168E 168F 168G 168H 168H 168K	2 3 7 5 5 0 1 2	1 3 16 5 4 15 10 9 6	6 3 2 2 2 2 2 1 1 3 4 4 3 3 0	9 14 13 15 13 11 41 10 6	• • • • • • • • • • • • • • • • • • • •	15 115 7 1 2	40. 19. 2. 16. 6. 0. 15. 0.	4 21 3 1 1	131 95 42 73 55 39 56 59 98 179	79 171 361 18 13 1 15 127 1035	84 46 1 48 32 31 35 20 0
169A 169E	1 5	5 1 7	0 0	0 19	•	3	9 <b>.</b> 9 <b>.</b>	1	177 30	1035 962	0 0

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CC AX CC		SEP <b>L</b> Se		•	V ER T D I		•		ZONTAL Bet	CONEU EAR	CTIVE TH
LINE & ANDMALY	REAL PPM	GAUJ Mag	REAL PPM	CAU2 Mag	•	CD.NE MH DS	CEPTH*		C J C J C J C J C J C J C J C J C J C J	DEPTH M	RESIS EHM-M	DEPTH M
1695 1695 1696 1696 1697 1697 1697	3 0 1 1 5 15 14 2	9 6 4 5 3 13 12	5 0 8 1 0 5 0 5 0	15 11 11 11 9 9	•	2 3 3 3 9 3 4 1 5 1	17 25 2 15 24 9 7	•	1 1 1 1 1 4 3	50 93 197 94 34 55 54 37	235 1035 1035 78 64 13 14 692	17 0 0 50 44 42 35 0
170A 170E 170C 170E 170E 170F 170G	2 41 6 2 14 6 7 22	5 60 24 13 10 7 13 22	3 52 16 0 32 12 37 37	1 100 25 14 23 24 40 40	•	2 9 3 1 16 5 7	22 . 5 . 17 . 0 . 15 . 1 .	•	1 2 1 1 2 1	135 48 52 57 72 68 99 52	147 46 114 610 19 70 27	76 21 23 1 49 28 69 19
1714 1710 1710 1715 1716 1716 1716 1711	1 0 13 6 0 27 3 4	1 5 20 14 3 12 4 1	0 0 17 4 0 72 4 15 23	2 4 27 22 0 26 14 5 20	•	2 1 8 3 1 46 3 3 17	62 0 1 6 0 8 0 8	•	1 1 1 1 4 2 1 2	2 2 6 93 54 2 8 1 6 9 6 0 5 9 6 9	1035 1035 128 552 1035 13 36 122 40	0 0 14 0 0 40 27 25 31
172A 172C 172E 172F 172G 172H 172I 172J 172J 172K 172M	0 2 2 2 4 5 7 1 3 2 10	25 335 452 7 18 15	4 1 39 11 83 132 9 37 37 622	2 74 43 51 269 265 27 12 34	•	5 1 7 2 6 9 2 30 10 4 6	0 <b>.</b>		1 1 1 3 2 1 2 1 1	235 226 35 33 99 28 29 64 70 43	1035 1035 76 144 15 22 254 27 65 221 69	0 0 7 0 73 11 0 41 19 22

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	SE AX		COPL CC		•	VERT DI	ICAL Ke	•		ZONTAL EET	CONTU Ear	CTIVE TH
LINE & ANDMALY	PEAL	CAU) MAG	FEAL PPM	C A U D M A A	•	CD ND	#HTFIC M		COND	DEPTH M	RESIS Chm-M	DEPTH M
172C	Э	1	1	2	•	1	14	•	1	175	1035	O
1734 1735 1730 1730	28 2 23 2	4 2 2 4 2 3 2	3 9 5 3 0	74 45 36 7	•	7 1 1 C 4	6 2 3 3 6	•	1 1 1	3 <i>6</i> 29 56 76	83 211 74 173	8 1 22 23
1735 1735 1735 1736	0 0 1 2	3 6 7 3	1 0 0	2 2 4 3	•	1 1 1 10	1 6 0 0 4 5	•	1 1 3 3	30 213 134 91	1035 1035 1035 16	0 0 0 64
1731 173J 173K 173M	7 25 9 6	4 29 24 17	48 51 25 11	D 57 49 31	•	44 11 4	8 0 7 9	•	2 2 1	79 43 64 54	15 24 54 159 24	54 18 31 15 23
173N 173C	22	23 12	4 <i>5</i> 32	43	•	13	3 13	•	2 2	49 61 89	12	23 29 63
1740A 1740E 1740C 1740C 1740E	5 1 5 3 3	2 + 15 5	14 2 13 5	14 35 -14	•	34 1 4 3	0 2 4 61	•	1 1 1 1	77 43 46 193	179 101 241 1035	23 10 1
1740F 1740G 1740H 1740I	1 39 22 33	7 15 16 48	0 110 149 149	10 23 142 154	•	1 71 18 15	0 0 0	•	1 15 5	56 38 46 30	710 1 7 5	0 2 3 3 0 1 7
1740J 1740K 1740M	10 2 3	14 7 13	15 18 5	33 28 18	•	6 4 2	17 13 5	•	2 1 1	45 67 35	49 65 358	17 32 0
1754 1758 1758 1758 1758	1 1 56 0 27	4 3 4 0 3 2	5 5 117 3 49	15 15 59 9	•	2 2 2 2 4 3	0	•	1 1 4 1 2	64 203 30 68 50	210 1035 12 137 43	19 0 11 24 21
175G 175H 175I 175J	4 5 1 3	3 3 1 2	4 11 5 5	14 3 1 1	•	4 14 25 21	Ö	•	1 7 3 2	52 55 94 136	360 4 19 36	3 35 64 99

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	00 AX 00		00 PL		•	V = R T		•		ZONTAL Bet	SENEU Ear	CTIVE TH
LINE & ANDMALY	R EAL PPM	04U) M49	REAL PPM	CAU@ MR9		CC VD MH DS	DEPTH# M		COND SOHM	C EFTH N	RESIS Chm-m	DEPTH M
175K	3	7	5	1 2	•	3	3	•	<b>4</b> -	64	173	20
176A 1768 1760	11 21 7	19 13 19	67 34 17	73 33 33 30	•	10 13 4	2 0 0		3 2 1 2	42 54 38 59	15 27 94 40	2 <b>1</b> 26 <b>7</b> 28
1765 1765 1766 1766 1766	20 2 1 3 4	1 9 2 2 7 3	29 5 3 4 4	1 1 10	•	11 5 3 0	5 5 + 9 43	•	1 1 1	208 176 68 211	517 1035 287 130	75 0 16 150
1761 1761 1763 176K	12 85 61 12	5 15 5 8 9	23 136 94 25	19 32 103 42	•	16 159 17 10	4 7	•	7 15 3 2	57 48 46 51	3 1 13 26	51 38 27 25
175N 175E 176P	12 15 1	10 24 4	2 8 3 1 2	24 44 9	•	13 7 1	17 5 15	•	3 2 1	3 E 5 O 4 4	24 40 434	62 2 <b>1</b> 0
1774 1775 1770 1770 1776 1776	54 2 4 7 77 21	84 15 4 11 23 22	216 4 22 0 140 35	230 44 17 11 35 45	•	21 1 10 3 100 10	0 25 0 10 0	•	5 1 2 2 10 4	22 26 31 54 43	6 138 36 33 2 11	8 0 49 33 31 40
1776	3	5	9	13	•	4	10	•	<b>1</b> 3	<b>7</b> 2 40	94 2	30 2 <b>7</b>
176A 1785 1785 1785 1786 1786	27 9 7 5 0	12 16 9 0 11 7	76 5 8 9 3 6 143	47 40 23 3 21 13 33	•	30 4 57 1 1 92	0 0 2 5 <b>7</b> 1 0	•	2 1 2 1 1	38 43 105 39 76 55	41 125 61 450 161	9 6 65 0 29 42
173H 173I 178J 178K	56 27 37 32	20 10 24 30	62 56 23	13 29 44	•	67 27 10	1 4 4	•	(9 (1) (8)	6 <b>1</b> 52 53	3 7 14	45 35 34
1790	41	2 0	97	4 5	•	35	0	•	9	43	2	30

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	004X 00		CEPL CE		•	VERT		•		ZENTAL EET	OE NE U E A R	CTIVE TH
LINE &	REAL PPM	56 W 6 9 Y D	FEAL PPM	C JL D M 79	•	KH 03 00 ND	DEPTH*	•	COND MHCS	DEPTH M	RESIS CHM-M	DEPTH M
179E 179F 179G 179H 179I 179J 179K	3 18 23 29 29 7	15 21 21 10 12 5	3 5 5 5 5 6 4 1 0 1 0	12 51 51 11 22 13	•	2 13 15 56 49 7 12	0 0 0 6 0 10 15	•	1 3 4 9 7 2	58 49 43 62 51 59 34	236 16 12 2 3 52 79	11 28 25 47 37 24 40
180C 180D 180E 180F 180G 180H 180J 180J	12 4 17 105 33 21 122 7	7 9 7 51 23 23 130 3	29 1 42 189 79 77 266 5	17 3 15 2 43 43 230 8 32	•	20 25 25 27 18 24 2	0 0 0 0 0 0 2 3	•	2 1 5 4 6 11 5 1	48 81 52 36 53 48 25 81 44	39 221 8 9 4 1 5 223 132	14 27 34 20 35 13 33

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<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW BIP OR OVERBURDEN EFFECTS.

	85 4 X 30		SEPL:		•	V ERT		•		ZENTAL BET	C C N C U E A R	CTIVE TH
LINE S ANDMALY	FEAL PPM	CAUS	FEAL	C 4U 2 P 4 9	•	COND MH DS	35PTH*. M .		COND RHDS	DEPTH M	RESIS CHM-M	DEPTH M
1804	ś	5	0	3	•	7	0 .	•	1	119	1035	9
1814 1810 1810 1817	1 10 11 5	6 6 11 4	1 3 9	3 4 3 2	•	1 11 9 12	0 · 6 · 2 · 0 · .	•	1 1 1 2	77 65 95 139	1035 129 67 36	0 2 <b>1</b> 5 4 9 5
1822 1820 1828 1828 1828	15 3 0 0 5 15	4 7 7 1 12 13	11 3 5 2 0 3	1 0 0 5 2 4 6	•	2 8 1 5 2 10	54 0 0	•	1 1 1 1 1	75 96 97 212 200 0	54 1027 1035 130 1035 306	34 0 0 151 0
1834 1835 1830 1835 1831	3 14 3 2 25	1 7 12 1 26	2 13 4 0 7	2 19 2 0 5	•	16 12 6 6 11	0 11 14 55 0	•	1 1 1 1 2	151 53 93 220 178	1035 82 115 1035 34	0 16 45 0 135
184A 1843 184C 184C 184E	21 5 0 0	11 5 2 5 7	15 3 0 1	15 5 1 4 6	•	19 9 5 4 1	31 77	•	2 1 1 1	73 159 229 134 82	48 1035 1035 1035 1035	3 6 0 0 0 0
185A 185E 185C	4 11 6	7 7 3 2	3 12 7	10 17 13	•	3 10 2	4 0 0	•	1 2 1	5 <b>0</b> 5 <b>1</b> 98	257 49 1035	10 24 0
1868 1860 1860 1865 1865	18 4 16 0	13 3 14 1	7 0 24 0 4	2 3 1 2 2 3 2 0	•	11	0 19 1 88 0	•	1 1 2 1	0 32 52 136 142	770 319 36 1035 1035	0 0 2 2 0 0

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OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	KACO 30		00 PL			VEFT			IZENTAL Heet	CONEU Eas	EVITOL HTS
EINE & YJAMDNA	REAL PFM	CAU2 Mag	REAL	CAUS MAS	•	SEND MHOS	DEPTH*.			FESIS CHM-M	DEP <b>T</b> H M
1 3 é 0 A	3	2	1	ī	•	Ģ	0 .	. 1	143	207	5 2
1874 1878 1870 1870 1870 1878	2 4 12 4 7 0	7 14 11 1 26 12	2 0 24 0 26	0 5 19 1 24 7	•	13 26 5 1	0 . 0 . 7 8 . 0 .	. 1 . 2 . 1	30 47 177 153	1035 638 26 1035 96 1035	0 2 0 0 9 <b>7</b> 0
1884 1885 188 <b>0</b>	11 1 1	5 5 7	15 1 0	13 1 3	•	11 1 8	0 15 44	. 2 . 1	. 218	30 1035 1035	2 4 9 0
13802 1880C 1880E 1880F	0 11 3 2	1 1 4 12	0 0 2 2 3	5 5 4 7	•	5 24 22 . 2	57 . 33 . 0 .	. 31	209	1035 1035 1 394	0 0 53 55
189A 189D 189E 189F 189G 189H 189J 189M	2 5 2 3 0 0 3 3 1 1	5 11 31 1 1 9 45	6 1 33 7 1 4 19	4 5 50 7 7 5 23	•	6 2 10 6 6 3 9	0 5 3 64 5 8 0 0	•	32 101 2 47 1 99 1 194 1 187 3 158 1 216	1035 134 37 1035 1035 858 21 1035	0 50 19 0 0 29 131
190A 190E	<b>7</b> 5	3	11 5	11. 11	•	13 7	0		2 64 3 149	34 19	33 114
1910A 1910C 1910C 1910E 1910K 1910N	5 1 4 6 2 7 0 3	8 0 14 24 5 30	4 3 4 3 9 4 3 0	7 4 22 3 3 4 41	•	4 165 2 14 7 5	0 2 9 0 0 4 6 0	•	1 26 2 143 1 44 3 45 1 114 3 25	219 37 195 18 1035 19	0 105 2 22 0 1

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

			059L4 061			PTICA DIKE			ZENTAL EET	CONDU( EAR	
LINE S ANDMALY	REAL PEM	CUFD MAG	R E A L D P M	CAUS	. CC VE		• PTHX。 M •	C 0 N D 8 D F M	DEPTH M	FESIS CHM-M	DEPTH M
192A 192C 192C 192E 192E 192I 192K 192C	3 6 19 13 0 20	5 17 25 7 2 9 0	8 0 30 31 0 13	9 24 3.6 6.5 2.6 2.6 2.2 2.2 2.2	• 3 • 1	2 7 1 5	0 . 0 . 3 . 67 . 0 .		170 40 58 45 149 122 215 215	1035 213 39 25 1035 2 1035 1035	0 0 29 18 0 105 0
1934 1935 1930	7 2 9	1 1 15	8 6 2	5 5 0	_	1 5 5	0 • 47 • 0 •	1 1	34 111 193	51 73 130	45 67 132
194A 194E 194C 194C	13 2 0 7	10 9 4 5	23 6 0 2	24 10 1 2	•	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 C O O	2 1 1 1	52 78 183 156	36 117 1035 1035	31 31 0 0
195 <b>4</b> 195 <b>0</b>	4 13	4 5	9	7 1	•	٤ 2 <b>7</b>	<b>1</b>	4	38 172	40 1035	5 <b>3</b> 0
1968 1960 1968 1967	1 5 0	0 7 1 3	5 4	) 3	•	1 0 8 3 2	0 65 33	. 2 . 4 . 2	132 215	52 14 39 137	80 93 170 146
197E 197C	10 35				•	19 39	ე 5	. 1 . 3		1035	0 58
1980E 1980D	5 0	: 4 ; 9	, 1 9 S		•	8	0 <b>1</b>	. 1		1035 1035	0
1990E 1990E	<i>5</i>			3 <u>2</u> 3 3	•	2 <b>1</b> 8	0 2 4		4 160 1 139	14 1035	125

<sup>\*\*</sup> ESTIMATED DEPTH MAY BE UNRECIABLE RECAUSE THE STRONGER PART .

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LINE, OR BECAUSE OF A SHALLOW DIP OR BVERBURDEN EFFECTS. .

	SSAXI SS		00PL:		•	VERT:		•		ZENTAL EET	CONEU EAR	
LINE & ANDMALY	REAL PPM	QUAD PPM	FEAL PPM	C 4U2 M 4 9		CEND MHOS		•	COND SOHM	DEPTH M	RESIS CHM-M	DEPTH M
2010C	9	1 4	7	5	•	٤	0	•	2	157	59	11 5
20202	23	2.5	9	5	•	13	0	•	5	135	10	104
2030A 2030C 2040C	4 3 20	4 4 13	. 2 5 3	3 1 <u>2</u> 3	•	5 2 22	0 1 3 0	•	1 1 1	143 83 194	1035 866 1035	o o o
205 <b>0C</b>	ອິ	11	10	9	•	ć	0	•	2	153	34	110
2060A 2060C	9 2	3 1	<b>4</b> 4	<del>4</del> 5	•	25 S	0 3 <i>3</i>	•	2 1	169 158	39 895	124 15
2071A	4	5	5	7	•	5	0	•	1	172	1035	<b>.</b>
2080E 2080E 2080F 2080G	ó 1 25 45	11 2 17 22	0 15 163 155	2 2 9 4 3 5 3	•	3 5 2 5 2 5 6	0 24 8 10	•	1 2 7 7	134 83 53 59	1035 43 3 3	0 4 <del>9</del> 3 <del>9</del> 4 5
2091B 2091 <b>C</b>	15 9	18 18	29 29	50 50	•	8 5	0	•	2 7	121 106	66 <b>4</b>	76 85
2100A 2100B 2100C 2100E	10 23 2 5	7 2 9 0 3	9 5 3	3 94 3 11	•	25 15 34 13	0 0 -42 1	•	1 3 1 1	59 34 114 175	1035 13 120 1035	0 15 59 0
2110A 2110C	4 1 7				•	8 2 <b>1</b>		•	1 5	109 43	1035	0 2 <i>5</i>
2120E	13	1 2	11	1 5	•	12	0	•	2		65	20

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	I XABO I BO		50 P L 4 50 I		VERT		c t :	ZONTAL EET	DUBNBD PARE	
S ENIL YLAMDNA	REAL	CUAD PFM	FEAL opm	QUAD .	. CBNE . MHOS	OEPTH#. M .	COND MHCS	CEPTH	RESIS CHM-M	DEPTH M
21200	14	10	27	25	. 14	12	2	71	34	4 0
2130A 2130E 2130F 2130G 2130H	5 0 5 4 4	5 4 1 1	4 0 15 15	1	5 . 6 . 274 . 114 . 149	9 54 25 24 17	2 1 2 11	133 222 139 106 139	43 1035 30 2 517	87 0 102 90 55
2140A 2140E 2140C 2140E	24 37 0 14	6 1 6 1 11	4 41 0 25	1 4 4 5 4 2 0	11 22 1	0 0 0 1 9	. 3 . 1 . 1	198 19 137 103	23 337 1035 36	161 0 0 71
2160A 2160E 2160C 2160D 2160E	5 5 0 3	1 0 2 0 5	2 5 0 0	3 2 3 5 1	22 129 5 7	õ	. 1 . 1 . 1	135 136 36	1035 858 1035 1035 1035	0 0 0
21704	ō	4	4	3	·	28	•	185	1035	0
21804	4	3	21	11	. 18	4	• 4	102	12	7 <b>7</b>
2190A 2190E 2190C 2190C 2190E	2 5 0 13 1	1 2	3 . 3 2 15	9 0 4	5 . 4 . 5 . 49	22 63 31	. 7	111 198	1035 740 39 3 15	0 15 153 71 72
2 200E 2 200C 2 200D	44 14 2	, 1	31	7	. 54 . 123	0	-	2 57 9 53 3 91	1 2 16	45 3 <b>7</b> 65

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNREGIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIF OR OVERBURDEN EFFECTS.

	05 4 X I		00 PL 4 00 I		•	V ERTI				ZENTAL Eet	CONDU EAR	
LINE &	FEAL PFM	CAU, Maq	REAL	CAU2 M45		CCND MHCS	DEPTH#.		C / C   C   C   C   C   C   C   C   C	DEPTH N	FESIS CHM-M	DEPTH M
2210A 2210B 2210C	c <del>4</del> 3 <b>2</b> 6	15 25 13	141 65 1	3 5 5 4 3 2	•	149 19 2	0 •		2 2 4 1	41 35 19	1 12 360	33 15 0
2 2 2 3 A 2 2 2 3 E 2 2 2 0 C	61 7 7	4 2 1 2 1 0	11 <b>7</b> 3 2	86 14 16	•	26 3 3	0 0	•	7 2 1	30 68 20	3 45 240	17 34 0
2 13 0 A 2 23 0 C 2 23 0 E 2 23 0 F 2 23 0 G 2 23 0 H	4 5 44 15 11 5	6 2 13 4 3 9	0 2 107 27 27	1 0 43 10 10	•	2 26 47 50 43 6		•	1 1 11 3 5	208 177 54 40 54 58	1035 1035 1 3 6 83	0 42 23 35 15
2240C 2240E 2240E 2240F 2240G 2240G 2240H 2240J 2240J 2240K 2240M	5 2 7 6 1 5 9 17 75 13	0 4 3 10 6 5 9 3 2 7	2 2 1 3 1 2 4 15 164 23	0 4 1 0 1 2 2 2 0 74 21	•	4 2 9 3 1 C 5 1 5 5 4 4 5 3 0	23 30 20 0 27 21 3	•	1 1 1 1 1 1 1 1 6 3	167 114 206 212 185 200 129 81 24 46	1035 1035 1035 517 298 845 297 69 4	0 0 78 75 47 62 40 10 22
2250A 2250C 2250D 2250E 2250F 2250I 2250J 2250K	692 1 166 762	7 3 13 0 0 63 81 23	2 0 1 5 173 195 39	4 0 0 0 0 140 207 49	•	5 27 1 36 52 22 18	3 3	•	1 1 1 5 4 6 6 3	95 205 194 163 141 37 25 33	230 1035 1035 10 16 5 4	36 0 0 132 107 23 12
2260E 2260D	25 49	53 9	5 .4	1	•	8 1 2 9	0 13	•	1	214 217	1035 1035	0

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	SEAX		002 <b>L</b> 00		•	V ERT DI			IZONTAL Heet	CENEU Ear	CTIVE TH
LINE & ANCMALY	REAL PPM	C 4U2 M 49	REAL OPM	G A U G M 9 9	•	CC NE MH DS	DEPTH*.		DEPTH M	RESIS CHM-M	DEPTH M
2260G 2260K 2260M 2260N	5 4 5 0 5 11 1	5 2 6 2 5 2 0	5 8 1 8 1 3 3	0 £1 £1 47	•	7 21 22 9	30 .	1 5 4 2	205 53 2 <b>7</b> 33	1035 7 11 32	0 3 5 . 9 . 7
2270E 2270E 2270E 2270E 2270F 2270I 2270J	13 35 12 7 77 49	23553994	0 1 3 2 1 181 108	3 5 2 1 1 201 84	•	51 52 102 23 5 17 24	4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 . 1 . 1 . 1 . 4	222 195 180 215 190 27 29	1035 1035 1035 756 1035 7	0 0 64 0 12 12
2280A 2280E 2280E 2280E 2280F 2280F 2280H	4 12 10 20 16 12 16	4 21 11 17 22 21 3	21 3 2 25 15 11 53	10 1 19 33 20 28	•	16 5 7 14 7 5 20	0 17 17 10	. 2 . 2	205 211 56 47 45	18 298 1035 33 30 45 40	65 95 0 23 21 15 6
2291A 2291B 2291C 2291C 2291E 2291E 2291F 2291G 2291h	0 4 15 17 17 7	3 0 0 5 3 41 6 13	2 0 22 27 30 10	1 0 0 17 63 77 0 23	•	1 21 124 24 5 5 9	91	. 3 . 2	156 210 48 38 35 53	203 1035 1035 15 22 46 181	96 0 27 15 11 13
2300A 2300E 2300C 2300D 2300E 2300F 2300G	5 1 11 13 14 0	29 5 5 18 21 21 6	20 20 20 9 9 0	79 17 23 23 21 3	•	2 14 8 5 1	0 0 1 2 0 0 0	. 4	20 52 47 2 43 2 57	96 352 44 30 53 26 1035	0 20 19 12 30

<sup>.\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	ODAXI OD		00 P <b>L</b> 4		•	VERT		•		ZONTAL EET	CENEU EAR	
LINE &	R EAL PPM	QUAD PPM	FEAL PPM	QUAD PFM	•	00 ND 20 HW		•	C NC O 2 J F M	D EPTH N	RESIS CHM-M	DEPTH M
2301A 2301B 2301C 2301D 2301F	11 23 3 11 13	3 7 15 16	47 47 5 1	4 4 3 0 1	•	1 55 2 <b>7</b> 9 9	0 0 21 6 12	•	1 1 1 1	161 95 207 206 213	1035 1035 1035 1035 1035	0 0 0 0
251A 231E 231F 231G 231H 231X 231M 231F 231C 231F	0 4 3 1 0 1 2 1 3 3 3	1 13 41 50 3 15 15 14	7 7 7 7 31 5 5 0 21 5 15 5	1 0 15 14 132 73 73 1 56 16 24	•	18 30 2 4 3 1 1 3 8 4 4 2	42 87 00 00 00 42 05 13	•	5 1 1 1 1 1 1 1 2 2 1	145 222 57 61 0 58 212 34 35 44	6 1035 154 774 76 449 1035 1035 30 47 54	120 0 12 0 0 0 0 0 3 8 16 4
2324 2328 232C 232E 232F	1 13 9 15	5 15 3 14	2 2 2 3 1 3 6 1	6 4 3 7 5 6 2 3	•	1 5 6 6	4 0 0 0 0	• • • • • • • • • • • • • • • • • • • •	1 1 1 2 2	124 22 158 31 46	1035 77 1035 30 49	0 0 0 4 15
233C 233E 233H 233I 233J 233K 233N 233N	0 0 5 0 21 2 1 15	3 3 3 2 3 5 4 2 13 11 3 3 3	5 10 18 0 52 0 0 19	5 15 67 0 94 1 7 59	•	<b>8</b>	3 9 3 6 0 0 0 0 4 0 0	• • • • • • • • • • • • • • • • • • • •	1 1 1 1 2 1 1 2	98 14 25 16 139 59 34 30	1035 1035 148 701 37 174 164 47	0 0 0 0 7 7 20 7
234 <b>A</b> 234 <b>B</b> 234 <b>C</b>	2 <b>0</b> 4 0 8		3	14	•	13 11 5	9	•	3 1 1	103 62	20 130 64	30 46 25

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONCUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW CIP OR OVERBURDEN EFFECTS.

	CCAX Ce	IAL IL	CEPL:		•	V EFT				ZONTAL EET	CDNDU EAR	
LINE &	REAL PPM	C 4 U J M 4 S	REAL PPM	C4U2 M49	•	CENE MH DS	DEPTH#.	, M	C A C	DEPTH N	RESIS EHM-M	DEPTH M
2340	7	14	1 ŏ	3.0	•	4	0	•	1	48	197	4
23 > <b>C</b> 23 5 <b>C</b> 23 5 <b>E</b> 20 5 <b>F</b>	1 3 3 9	4 5 14 11	0 15 7 10	2 15 0 12	•	1 10 7 7	0 8 2 0	•	1 2 3 1	96 76 194 58	3 6 1 4 1 2 5 7 4	33 42 156 18
23 6A 23 6E 23 6C 23 6E 23 6E 23 6F	20 13 10 4 5	1 + 7 5 4 5 3	22 4 19 15 0	23 6 17 14 1	•	14 14 15 95 8	3		2 1 2 1 1 2	70 85 62 74 196 75	44 121 36 356 1035 54	36 35 31 13 0
2378 2370 2370 2370 2376 2376 2376	0 2 3 6 3 5 9	5 3 15 6 3	14 1 7 10 11 11	2 1 1 2 6 15 14	•	έ 6	17 36 27 28 7 0 13	•	1 4 1 1 1 2 2	152 141 132 129 76 52 34	1035 11 1035 193 70 54 36	0 114 0 65 35 15 52
25 5 B 22 5 C 25 5 D 23 5 E 23 8 F 23 8 G	25 10 0 3 12 5	29 7 12 4 10	41 37 3 16 20 9	43 17 6 8 22 15	•	11 22 1 11 14 5	1 0 2 3 0 2 4 0 2 2	•	3 5 1 4 3 2	50 86 111 95 58 52	22 6 1011 14 19 59	35 68 5 72 33 44
23 9 A 23 9 B 23 9 C 23 9 D 23 9 F	0 41 14 13 2 5	10 29 20 20 0 5	1 79 79 6 4 10	13 61 61 23 2	•	. 14	<b>1</b> 3		1 3 2 1 3	51 44 34 22 202 63	840 19 31 114 25 71	0 21 3 0 164 25

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART.

DEF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT.

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	KABC BC		05 PL (		•	VERT:	ICAL .	. 40	RI SH	ZCNTAL EET	CONDU EAR	
LINE & ANDMALY	REAL	QUAD MA9	REAL PPM	C A U D M P P	•	CEND MH OS	DEPTH*.	MHO		DEPTH M	RESIS CHM-M	HT93C M
240A 240B 240C 240C 240E 240E 240G 240H 240I	4 4 16 1 0 5 17 3	3 5 14 6 2 2 13 13	1 4 5 4 9 3 1 5 5	4 1 9 5 7 10 27 37	•	6 7 35 2 4 42 16 1	5 • 2 4 • 1 • 5 • 1 6 • 0 • • 0	•	1 2 7 1 2 3 2 1	83 155 76 78 61 52 43 93	2 9 8 5 1 7 0 3 9 1 5 3 5 3 2 9	18 121 58 36 28 30 13 35
241A 241E 241C 241D 241E 241E 241F 241G 241H	5 3 17 10 3 1 10	5 6 0 1 3 3 10	4 1 22 19 7 3 4 21	12 3 0 3 8 3 9	•	20	0 . 1 2 . 2 1 . 2 3 . 2 7 . 0 . 3 0 . 1 3	•	11431115	53 113 109 76 52 91 139 114	562 126 13 25 104 70 77	0 60 84 49 11 48 93 92
242C 242C 242E	3 3 5 2 5	3 16 14	5 107 42	0 3 3 3 4	•	4 10	0 1 10 10	•	1 5 5	50 50 60	1000 10 10	30 30
243C	22	10	44	2.5	•	20	10	•	5	<b>65</b>	7	40

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	00 AXI 00		562L 30		•	VERT:			HERII Shi	ZENTAL EET	CENEU! EAR	
LINE &	R E A L PPM	QAU) Mqq	REAL	CAUD	•	OD NO MH OS	CEPTH*.		СИСЭ 8 ЭРМ	DEPTH M	RESIS CHM-M	DEPTH M
1803	3	1	0	Э	•	12	64 .		1	198	1035	0
181A 1818 181C 181F 181G 181H 181I	19 4 13 12 31 83 40 3	22 17 34 44 15 25 3	44 22 13 -21 231 239 51 4	3 3 4 5 3 8 7 3 2 2 6 5 9 3	•	13 3 5 3 146 112 9	3 . 1 . 0 . 0 . 0 . 2 . 4 2 .	•	2 1 1 3 9 23 2	54 39 47 44 43 20 36 130	23 36 100 16 2 1 22 34	29 9 12 23 30 13 15
182A 182B 182C 182E 182F 182H 182H 182I 182J 182K	2 2 1 2 3 0 1 4 2 1 3 2 2 4 0	15 6 47 36 36 7 56	52 2 18 3 25 0 47 59 107	35 12 52 73 72 2 3 23 143	•	20 1 5 1 4 1 52 48 12 3	19 10 3 1	•	3 1 1 1 1 1 10 4 3	44 29 41 9 28 127 57 46 35 158	19 415 106 376 114 1035 2 9 14 126	21 0 10 0 1 0 43 27 16 100
183A 183E 183C 183E 183F 183G 183H 183J 183K	70 4 13 1 13 19 3	53 38 21 15 94 36	177 7 3 0 54 64 15 0	155 36 36 32 45 24 17 5	•	7	0 52 1 0 6 3 13 0	•	4 1 1 4 5 1 1	28 106 39 21 41 38 51 218 79	11 339 225 745 8 7 65 1035	11 47 2 0 24 21 15 0
184A 184E 184C 184C 184E	9 3 2 0 4 2 5	11 29 11	29 17 38 7 60	14 44 62 21 59	•	_	6 0 0 0	•	3 1 2 2 3	35 35 45	16 79 52 50 18	7

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	X430 50		COPL CC		•	V ER T C I		40		ZCNTAL EET	CCNEU EAR	
LINE & YJAMONA	REAL PPM	C A U J M 9 9	FEAL	CAUD Mag	•	CENE	DEPTH*.	ከተ		DEPTH M	RESIS CHM-M	DEPTH M
185A 185E 185C 185C 185F 185G	4 19 2 95 1 43	10 42 3 50 0 40	14 13 90 151 3	25 63 161 10 94	•	4 4 18 20 2	5 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 •		1 3 3 1 5	54 42 88 28 156 36	56 138 17 17 102	21 6 61 8 112 21
1860A 1860E 1860C 1860E 1860F 1860F	3 4 5 0 4 0	2 5 3 3 2 9 1	12 13 53 3 4 4	15 15 90 9 16 5	•	7 6 18 2 2 3	19 0 0 17 6 47		1 1 4 1 1	82 57 20 150 41 104	93 66 10 1035 1035 170	33 17 3 0 0 50
1878 1870 1870 1875 1877 1876	3 8 20 40 2 0	10 19 39 34 9	24 27 39 39 0	45 50 49 33 12	•	4 5 7 16 1 2	3 . 0 . 11 . 5 . 0 .	•	1 1 1 1 1	57 52 47 48 54 204	113 136 68 67 1035 1035	19 12 19 17 0
1380A 1380E 1560C 1380C 1380E	5 2 7 23 1	3 4 4 31 1	21 14 39 46 1	10 31 7 64	•	22 4 53 9 4		•	4 1 2 2 1	87 43 76 41 107	14 133 31 35 970	63 7 46 14 13
1898 1890 1890 1898 1898	3 6 7 21 0	19 20 7 15	32 32 9 15	67 68 12 16 32	•	4 7 13 1	3 0 2 2 3	•	1 1 1 1	66 26 87 49 74	99 81 64 87 1035	29 0 47 12 0
190A 190B 190C 190D	17 25 1 7	33 15 13 14	21 13 0 26	7 5 1 0 3 0 4 3	•	5 20 1 5	0 5 0 11	•	1 2 1 1	24 79 13 47	68 31 733 67	0 49 0 17

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	CEAX!		CCPL:		•	V ERTI		ម្រក ទ	IZCNT HEET	ΔL	ODNOU EAR	
LINE & ANOMALY	REAL PFM	G AU D M q q	FEAL	CAUS Mag	•	CCND MH JS	DEPTH*.	C DNC S	DEF	HT: N	RESIS CHN-M	DEPTH M
1910 1912 191E	5 9 5	11 11 1	1 2 2 3 1	20 25 5	•	5 8 17	1 · 2 2 · 4 6 · ·	1 2 1		75 57 89	120 44 227	30 27 34
1924 1925 1920	0 0 3 <b>1</b>	2 0 3 2	0 0 56	3 2 €4	•	1 2 13	17 · 74 · 6 ·	1 1 1		130 37 43	1035 1035 70	0 0 13
193A 193E 193C 193E 193F	10 3 1 4 3	1 4 2 1 3 3	11 2 2 7 4	1 3 5 7 7	•	64295	21 . 30 . 39 . 22 .	1	L L	55 69 205 3 <b>7</b> 104	155 176 298 127 86	17 21 95 36 55
1944 1942 1940 1940 194	14 5 1 2	17 14 3 8	10 5 5 5 1	20 20 21 21 1	•	6 2 1 2	20 6 4 1	•	1 1 1 1	42 27 41 49 203	217 287 164 476 1035	5 0 5 0
19 <i>54</i> 19 <i>5</i> 8	71 7	7 6 2 3	7 <del>9</del> 1	101 30	•	15 2	2 0	•	2 1	39 22	33 393	15 0
196A 196E 196C 196C 196E	14 31 1 8	4 11	43 2 9	1 3	•	6 10 2 5 4	4 . 5 . 37 . 4 . 6 .	•	2 2 1 2	55 46 226 62 51	31 48 1035 53 68	28 18 0 27 17
1974 1978 1978 1978 1978 1977	0 0 5 4 4 5	19 60 77	0 75 65	23 107 132 4	•	1 1 11 8 7	9 63	•	1 1 2 1 1 3	122 22 41 36 29 51	737 491 30 55 911 17	30 4 18 13 0 35

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	55.4X.3 30.3		05 PL : 05 PL :		•	VERTI EII	164L •		ZCNTAL EET	CONEU EAR	
LINE &	REAL PPM	C J L D M q q	REAL PPM	QUAD Mag	•	CONE 804M	DEPTH#.	C D N D S D H M	DEPTH M	RESIS CHM-M	DEPTH M
1984 1988 1980 1980 1980	2 2 9 2 4 1	5 2 <del>9</del> 2 5 5 2	6 4 2 0 8 2	16 43 44 15	•	3 13 1 4 2	24 · 3 · 2 · 0 · 31 · ·	1 2 1 1 1	47 47 18 42 37	248 39 641 65 113	9 18 0 4 39
1994 1998	13	7	5 0	1 2 1 7	•	7	23 .	1	5 E 34	183 978	1 5 0
200A 200E 200C 200E 200F	2 19 0 2 2	5 1 3 3 4 3	6 18 5 5	7 20 3 3	•	3 11 2 3 4	42 • 22 • 27 • 0 • 10 •	1 3 1 1	32 53 195 109 34	720 134 22 173 37	0 17 159 48 28
20 <b>1</b> A	3	7	6	10	•	7	21 •	1	50	319	3
2024	10	કે	19	13	•	14	34 .		48	130	14
2034	3	3	16	13	•	18	13	2	36	35	37
204A 204ê	<b>43</b> 2	5 D 2	6 2 4	8 2 1	•	13	8 . 71 .	2		44 298	13 23
205A	25	21	31	34	•	13	6 .	. 1	50	57	18
205A 205E	4 <i>5</i> 3			77 13	•	10	9	. 1 . 1		62 505	15
207A 207E 207C	43 1 1	1 3	, 2	21		. 21 . 1		. 2 . 1	4 8	34 528 819	15 1 0

<sup>.\*</sup> ESTIMATED DEPTH MAY SE UNRELIABLE SECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	60 4X 3		00 PL 4		•	V EFT:			ZENTAL EET	CONDU EAR	CTIVE TH
LINE & ANDMALY	LAER MR99	CAUS	REAL PPM	CAUS		BND IHDS	DEPTH#.	COND MHCS	DEPTH M	PESIS CHM-M	DEPTH M
2084 2085 2080 2030 2035	0 0 4 4 7 3	4 3 43 5 21	6 0 8 0 3 5	3 11 67 7 33	•	2 1 15 10	17 • 14 • 10 • 43 • 0 •	1 1 2 1	9 9 4 4 4 3 9 9 2 9	117 969 33 160 226	50 0 19 50 0
2094 2092 2090 2090 2095	1 1 51 40 2	8 8 54 2 <b>7</b> 4	5 5 29 44 11	12 11 122 31 15	•	2 2 13 22 4	20 • 12 • 1 • 2 • 22 • •	1 1 2 2 1	38 75 31 57 57	962 164 22 51 95	0 31 10 24 20
2108 2100 2108 2108 2108	13 0 69 0 52	3 9 5 9 5 6	69 11 84 0 73	139 35 110 12 90	•	6 2 16 1 14	0 • 12 • 5 • 1 •		30 102 35 34 46	52 1035 35 553 31	4 0 12 0 21
211A 2118	107	104	174 4	203 <b>7</b>	•	19 5	2 • 33 •		3 <b>0</b> 35	10 163	14 37
212A 212E 212D	2 <i>5</i> 1 <i>9</i> 0	34 39 2	62 34 0	82 72 9	•	10 6 7	7 • 9 • 53 •	. 2	41 40 85	15 49 1035	21 15 0
213A 213E 213C 213C	2 17 14 1	4 20 22 0	5 3 <b>7</b> 18 6	7 53 35 5	•	4 9 6	34 • 0 • 5 • 5 •	2	112 29 39 78	39 28 110 98	65 4 7 34
214A 214E 214C 214D 214E	27 3 2 7 5			5 4 1 6 1 7 3 2 3 4	•	8 3 2 4 2	0 15 11 9	. 1 . 1	35 52 56 53 40	47 85 70 139 262	8 26 22 16 2

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CEAXI CE		CCPL:			V EFT C I				ZCNTAL EET	EENEU Ear	
LINE & ANOMALY	PEAL	CUAD M 49	F E A L P P M	CUAD PFM		CEND MH OS	DEPTH#.	N	2 A S	DEFTH N	RESIS CHM-M	DEPTH M
2154 2155 2150 2150 2150 2153 2155	9 2 4 7 3 10	7 4 7 13 16	20 5 5 16 8 30	20 7 18 22 21 24	•	11 4 3 6 2	0 . 17 . 12 . 7 . 0 .		1 1 1 1 1 2	43 66 58 36 45 78	70 133 153 344 159 42	4 20 19 0 7 44
2164	0	4	ĵ	ó	•	2	15	•	1	92	108	45
218A	1	કે	1	15	•	1	0	•	1	49	391	2
219A	1	12	3	15	•	1	10	•	1	50	1035	0
220A	12	41	7	43	•	2	<del>4</del> ,	•	1	38	353	2
2214	5	17	3	23	•	2	1	•	1	69	192	24
2225	15	3 9	21	55	•	4	3	•	1	41	115	9
2244	5	13	9	28		3	0	•	1	19	395	0
225A	19	2 9	33	4 3	•	7	1	•	1	39	71	9
2 2 5 0 A	2	7	9	13		• •	13	•	1	B 2	93	4 0
226A 226B	4 4	9	3 7	2 0 2 0		• 3 • 2	4 0	•	. 1 1	5.7 35	113 284	19
2274 2278	5 9					• • 4		•	1 1	55 24 RONGER P	76 417	21

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X		SOPL CC:		•	VERT DI		•		ZCNTAL EET	C D N D U E A R	CTIVE TH
E BRILL YLAMINA	REAL PPM	CAU) Mag	FEAL PPM	CAU2 M49	•	CEND	SEPTH# M		COND	DEPTH M	RESIS CHM-M	DEPTH M
228A 228E	19 17	57 19	16 31	5 3 6 0	•	4 7	0 0	•	1 2	43 29	90 49	13 0
2290A 2290E 2290C	1 45 43	4 7 0 7 0	0 102 102	5 12 <b>1</b> 113	•	2 12 12	0 0 3	•	1 3 4	113 25 24	100 18 11	63 5 7
2304 2308 2300	7 8 74	15 14 63	0 19 142	0 22 133	•	4 6 21	ა ი ი	•	1 2 3	76 32 25	3 0 5 3 5 1 3	2 2 4 7
2314 2318 2310 2310 2318 2316 2316 2316	1 1 2 5 20 12 14 42	8 6 2 17 36 3 26 27	5 5 6 14 16 13 83	7 13 5 37 27 32 32 67	•	2 2 6 2 6 8 5	7 0 63 1 3 9 10	•	1 1 1 1 2 1 3	105 14 57 30 61 50 45 31	92 705 80 152 65 37 53	58 0 26 0 26 21 17 9
232A 232E 232C 232E 232E 232F 232F 232J 232J 232M	0 0 1 4 3 3 1 1 20 4 9	10 9 10 4 3 4 0 27 9 13	0 0 2 15 24 7 6 5 26 23 14	27 21 12 37 26 18 21 13 31 7	•	8 4 7	9 10 15 34 33 3 3 4 0 17	•	1 1 1 2 3 2 2 2 1 1 2	26 28 28 50 55 46 48 48 48 65	843 892 560 40 18 28 37 38 71 73 25	0 0 0 25 38 29 19 25 14 32 16 32
232N 2320 233A 2336 2330 2330	6 204 7 9 4 3	283 7 5 19	347 27 1 16	39 6 21 18 56 39	•	20 12 1 2	30 9 7 15	•	3 1 2 2	26 36 57 43 39	22 1 83 40 31	61 17 13

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	00 AX		C C P L C		•	V ERT		•		ZONTAL EET	CENEU EAR	
LINE & ANGMALY	R EAL PF M	CAUA M 99	REAL PPM	CAU2 M99	•	CD ND MH OS	DEPTH#.		CAGO	DEPTH M	RESIS CHM-M	DEPTH M
233E 233F 233G 233H 233I 233J 233K	7 1 15 5 19 13 3	3 11 19 3 20 12 37	41 3 13 11 28 16 15	54 32 23 17 26 61 56	•	8 1 7 5 11 5	5 6 8	•	3 1 2 2 2 2 2	37 47 43 59 47 57	21 70 47 41 26 40 54	15 16 12 27 21 27 22
23 4A 23 4B 23 4D 23 4E 23 4E 23 4F 23 4F 23 4H 23 4I	2 1 5 0 4 1 50 3 13	16 3 7 16 16 9 29	3 0 17 0 5 2 110 10 40	2 2 1 3 7 3 3 3 5 1 6 3 6 7	•	1 2 4 1 2 3 12 4 7	0 11 5 6	•	1 1 1 1 1 2 3 3	41 65 48 19 27 63 29 34	220 1035 56 843 270 410 13 15 23	2 0 17 0 0 10 11 59 27
2354 2358 2350 2350 2356 2356 2356 2356	5 11 7 5 7 14 15	12 13 13 14 7 17 29 32	4 21 13 8 11 9 35 29	17 37 37 43 18 21 61	•	2 7 4 2 6 6 6	0 0 0 9 15 9 4		1 3 2 1 2 2 2 2	27 51 36 32 58 58 45 38	4 25 22 50 177 49 28 28 75	0 2 5 6 0 2 4 4 0 2 1 1 0
236A 236E 236C 236D 236E 236F	5 30 10 1 5	14 21 11 4 1	13 61 13 0 15 26	33 60 19 1 13 41	•	_	0 1 0 2 3 2 0 4	•	1 3 2 1 3 2	30 40 42 34 74 46	144 18 26 344 16 26	0 18 15 27 49 21
237A 2376 237C 237D	3 5 5 4	5 7 12- 6	4 2 8 4	5 7 1 9 1	•	,	10 6 11 26	•	1 1 1 1	56 48 55 93	196 1035 143 106	\$ 0 16 45

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	06 4 X		COPL.		•	V EPT E I		•		ZENTAL BET	CONEU Ear	
LINE S ANSMALY	R EAL PPM	CUED PEM	REAL	CAUQ MAS	•	CEND MHOS	⊅EPTH≭ M		C 3 HM	DEPTH N	RESIS CHM-M	HT93C M
2378 2378 2376 2378 2371 237J 237K	2 61 9 7 13 11 13	12 61 25 13 31 11	4 151 29 7 17 14 	11 123 65 13 49 3 42	•	1 20 4 4 4 15		•	1 5 2 2 2 2 2 2	42 21 38 69 34 56 34	749 7 32 33 45 26 46	0 7 14 39 9 29
23 3 A 23 8 B 23 6 C 23 8 E 23 8 E 23 8 F 23 8 G 23 3 H	6 3 9 3 8 7 24 10	3 5 8 2 1 9 1 8 3 1 1	5 3 27 4 11 44 45 31	10 4 12 32 12 30 60 21	•	4 4 17 1 7 9 9		•	1 1 2 1 2 2 2 2 2	73 54 54 54 54 54 54 45 45	153 263 32 81 33 49 26 25	25 3 25 12 22 14 15 19
289E 289C 289E 289E 289F 289G 289H	5 13 10 13 2 0 2	4 21 5 0 6 6 3	3 1 43 43 6 3	6 1 0 14 20 3	•	132 2000 2	4 0 7 0 16 0 26	•	1 1 1 4 1 1 2	41 52 90 111 84 43 90	8 8 7 3 1 2 1 1 6 1 2 3 7 9 1 6 1 2 8	0 40 84 28 4 61
240A 240B 240C 240D 240E 240F 240G 240H 240I	3 10 3 4 4 5 5 7 4	1 2 3 7 7 2 1 5 8 3	11 3 4 10 16 12 3 14	10 0 2 17 27 5 16 12 5		5 21 2	17 31 7 4 0 41 5 4	•	1 1 1 1 2 5 1 3 2	75 61 71 53 43 94 58 73 54	84 144 100 51 44 7 265 19	31 16 21 17 10 74 13 47
241A 2418 241C	4 3 0 0	4 23 4	19 68 2	9 5 <b>7</b> 9	•		4 0 1		1 5 1	73 41 75	72 5 107	30 25 32

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STEDNGER PART .

BE THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	CGAX		66 P <b>L</b> 66		•	V ERT I I		•		ZCNTAL EET	CONDU EAR	
LINE &	R EAL PPM	6463 M 48	FEAL	CAUS		CDND 8CHM	DEPTH*	-	C	DEPTH M	FESIS CHM-M	DEPTH M
241D	6	17	5	15	•	2	3	•	1	54	132	2 5
242A 242B 242 <b>C</b> 242E	1 9 7 7	6 5 2 10	4 26 15 21	5 2 3 5 2 4	•	2 13 43 7	11 22 37 3	•	1 4 5 4	98 71 69 56	1035 9 7 12	0 5 <b>1</b> 5 0 3 5

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<sup>.</sup> OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	00 A X 00		00PL		•		ICAL .		ZCNTAL EET	CONDU E <b>a</b> r	CTIVE TH
LINE & ANCMALY	REAL PPM	CAU2 M49	REAL PFM	QUAD PFM	•	COND MH OS	⊃EP <b>T</b> H*. M .		DEPTH M	RESIS CHM-M	DEPTH M
242A 242E	5 5	<u>2</u> 5	5 5	5 5	•	14 5	41 . 23 .	1	8 C 6 9	182 34 <b>0</b>	31 13
2434 2438 2438 2438	5 20 2 4	23 13 10 1	19 18 7	61 12 24 0	•	3 14 2 32	0 · 17 · 5 · 67 ·	1 3 1 1	19 104 71 207	85 20 107 1035	0 76 31 0
244£ 244£ 244C 244C	4 7 9 47	19 10 4 30	1 5 2 5 7 2	4 3 7 3 4 7	•	3 5 20 26	0 · 14 · 33 · 11 ·	1 1 1 5	1 & 1 7 & 1 3 & 5 5	100 1035 1035 7	0 0 0 4 3
2454	3	3	4	2	•	٤	5 .	1	141	112	84
246A 2462 246C	3 63 1	1 5 9 5	5 126 4	2 117 11	•	20 15 1	3 9 . 4 . 3 .	1 4 1	20 <b>7</b> 43 36	1035 8 308	0 27 31
247A 247E 247C 247B 247E	3 3 3 5	0 1 3 3 15	4 1 6 9 13	3 0 1 4 20	•	20 19 27 15 6	46 • 53 • 26 • 15 • 0 •	1 4 1 4 1	79 169 201 129 71	105 11 517 11 80	31 137 68 101 30
243A 243C 243D 243E 248F	1 7 3 2 14	1 3 6 3 11	7 2 5 4 18	4 2 9 12 14	•	10 22 3 2	42 • 33 • 5 • 8 • 9 •	2 1 1 1 2	139 203 126 81	28 1035 97 145 48	103 0 75 36 45
249A 249E 249C	9 3 8	1 3 5	1 2 7 1 0	2 5 5	•	124 8 15	24 . 0 . 3 .	10 3 2	139 160 112	3 18 43	120 125 74

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X433 33		CC 2F		•		ISAL . KE .		IZONTAL Heet	CONDU EAR	CTIVE TH
LINE & ANEMALY	PEAL PPM	CAU) MAS	FEAL	CAUD	•	COND	OEPTH≭. M .			RESIS CHM-M	DEPTH M
250 <b>4</b> 2508	9 1	7 7	10	12	•	1 C 2	7 .	. 2 . 1		61 116	61 51
251A 2516 251 <b>C</b>	2 2 4	3 3 6	1 0 4 7	3 3 10	•	7 3 4	34 · 10 ·	2 1 1	109	40 943 55 <b>7</b>	45 9 0
25 2 <b>4</b> 25 28	6 3	6 1 5	3 7	3 13	•	7	9 . 1 .	1		158 152	4 3 2 1
283A 253 <b>C</b>	4 3	3 5	14	7 13	•	16 3	0 . 8 .	4		9 8 <b>C</b> 3	5 <del>6</del> 0
254 <b>A</b> 2548	4 2	3 4	1 ó 5	5 5	•	19 4	12 .			11 88	6 5 3 <b>1</b>
255A 2558 255C 255D	5 6 15 3	14 14 10 9	1 1 25 3	15 15 13 10	•	2 4 20 2	3 . 9 . 16 . 5 .		2 <b>1</b> 9 98	858 1035 23 676	6 6 0 6 9 0
256A 256B 256C	0 0 11	4 7 7	4 4 18	5 5 3	•	1 2 21	0 .	1 1 2	207	96 1035 44	70 3 64
257E 257C	7 3	9 2	14	12 4	•	8 11	7 . 24 .	2		46 27	60 69
258A 253E 253C	9 0 17	11 5 9	15 0 40	23 4 21	•	7 1 26	0 .	1 1 4	58	165 1035 12	15 0 27
25 9 A	3	2	5	ó	•	7	• 5 •	1	121	91	69

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OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, BR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	00 4 X		CCPL CC		•	VERT DI			RIZONTAL Sheet		JCTIVE RTH
LINE & ANDMALY	REAL	CAU	F E A L P P M	CAU2 Mag		DD ND SC 4M	#HT93C M			RESIS CHM-M	DEPTH M
259â	43	2 9	104	<i>ŧ</i> 3	•	2 &	0	•	5 41	ε	25
260A	13	3	24	15	•	17	D	•	2 5 <b>7</b>	27	2 9
261A	14	12	2.2	23	•	11	0	•	1 63	93	2 2
262 <b>A</b> 262 <b>C</b>	3 9	5 10	8 <del>9</del>	14 11	•	4 7	2		1 100 1 43		47 0
2648 2648 264 <b>0</b>	1 4 9	2 1 2 5	6 5 2	5 11 2	•	5 3	4 0 1 2 0	•	2 146 1 85 1 123	40 220 1035	10 <b>7</b> 35 0
265A	2	7	3	7	•	2	10	•	1 62	622	0
265A 2663	4 0	3	7 2	7 3	•	(a)	3 <b>7</b> 34		1 104 1 111	89 463	58 3 <b>1</b>
267A 267B 267C 267C	4 3 0 14	2 12 3 13	13 3 0 25	2 1 2 1 3 6	•	5 0 2 1 9	3 5 0 0 1 1	•	5 129 1 76 1 113 1 58	5 509 943 136	105 9 0 20
268A 2682 268 <b>C</b>	2 1 12	3 2 13	6 2 19	2 3 3 0	•	7 2 . 7	2 0 2 9 0		1 97 1 159 1 53	329 719 141	31 33 11
269A 269E	42 15	3 5 1 5	7 <sup>2</sup> 2 31	63 36	•	1 E 11	1 2 0		3 E 1 50	10 106	4 0 1 1
270A 270E	3	1	<del>9</del> 3	<b>6</b> 2	•	14 11	3 6 7 2		128 1 218	14 192	100 163

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LINE, OR BECAUSE OF A SHALLOW DIP OR GVERBURDEN EFFECTS.

·	CE 4X CE		COPL CC	ANAR IL	•	VERT LI			ZENTAL EET	CENEU EAR	ICTIVE TH
LINE & ANDMALY	REAL PFM	C UAD PPM	PEAL PPM	CALD	•	COND MHDS	)EPTH*.		D EPTH F	RESIS CHM-M	DEPTH M
270 <b>C</b>	1 0	9	21	2 0	•	10	0.	2	58	5 <b>4</b>	20
271A 271B 271C	3 3 5 3 9	3 2 8 4 2	3 <b>7</b> 5 <b>7</b> 5	2 51 51	•	7 13 13	21 · 2 · 0 ·	1 3 2	148 53 35	94 14 23	9 6 3 3 1 2
2723 272 <b>0</b>	1 24	3 2 3	2 5 4	2 79	•	2 10	22.	1 2	2 0 2 2 4	4 0 <b>1</b> 2 4	7 9 1
2732	11	14	10	23	•	5	0.	1	46	118	3
274A	÷	÷	20	10	•	23	3 .	4	76	12	5 1
2 <b>7</b> 5£	7	9	3	9	•	ŧ	0.	1	53	374	9
2 <b>7</b> 6A	1	4	1	3	•	2	29 .	1	124	1035	0
2774	1	4	5	12	•	2	8 .	1	68	129	24
2784	1	4	6	13	•	3	19.	1	97	114	49
2 <b>7</b> 9A 2 <b>79</b> B	1 21	4 12	7 71	13 40	•	3 26	0 •	1 5	58 40	11 <b>1</b> 5	1 2 2 4
+ · · · · ‡					•		•				
2 <b>2</b> 0E	3	11	3	2 9	•	2	6 <b>.</b>	1	53	164	15
281A	9	ō	1	4	•	2	29 .	1	107	1035	Э

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<sup>.</sup> LINE, OR SECAUSE OF A SHALLOW DIP OR DVERBURDEN EFFECTS.

	0			ANAR IL		RTICAL DIKE	•		ZONTAL EET	CONDU EAR	JCTIVE RTH
LINE & ANDMALY	REAL PPM	C AU J M A Q	FEAL PPM	CAUP	. CEN!		TH∺. M .	C D N D S D H M	C EPTH M	FESIS CHM-M	DEPTH M
2 E 2 A	1	3	5	ŝ	•	3	33.	1	103	128	5 2
2884	3	9	4	,1 ó	•	2	1 .	1	25	1 99	0
29 <b>04</b> 2907	2 4	5 9	7 4	<del>9</del> 24	•	<u>2</u>	19.	2 1	10£ 35	50 221	6 5 0
2914	4	11	3	23	•	2	o .	, 1	33	175	0
293 <b>4</b> 2938 2930	10 3 0	1 4 1 5	3 5 0	4 7 5	•		3 • 27 • 30 •	1 2 1	204 157 98	1035 35 1035	0 117 0

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	00 A X		05 PL		•	, -		•		ZONTAL EET	CONDU EAR	
LINE & ANEMALY	FEAL	DAU2 M 49	REAL PPM	CAUD	•		×nT9∃C M		COND ZOHM	D EPTH N	RESIS EHM-M	DEPTH M
243E 243C 243D	2 1 4	9 3 2	3 0 2	2 0 2 4	•	1 1 7	0 4 ś	•	1 1 2	38° 63 103	5 60 2 9 1 4 5	0 8 6 <b>7</b>
245A 2458 245C	0 5 2	5 8 1	0 4 8	9 15 3	•	1 3 22	0 2 5.5	•	1 1 2	122 37 92	1035 392 28	0 9 62
246A 246E 246C 246D 246E	21 14 5 10 5	3 3 1 0 5 7	7 15 15 13 21	23 13 2 22 15	•	22 7	13 2 7	•	1 13 3 2 4	51 132 70 50 57	1 14 1 17 47 13	18 119 44 17 44
247A 247B 247C 247D 247E	13 5 12 8 7	17 6 7 6	5 2 25 15 16	23 7 20 15 15	•	4 16 10	9 4 0 5 5		1 1 2 3 2	50 32 50 <b>7</b> 5 52	200 265 28 21 47	3 0 21 48 27
248E 248C 248D 248E 248F 248G	1 0 11 4 4	5 6 11 4 4 3	9 3 25 19 19	12 0 27 14 16 2	•	1 9 10	15 2 6 24 19 52	•	2 1 2 5 4 1	74 92 58 86 81 189	57 124 30 6 9 1035	37 41 29 63 59
249A 249E 249C 249D 249E 249F 249G 249h	24 1 2 3 14 5 11	46 63 615 14 4	12 0 4 3 29 1 0	52 7 5 9 33 1 7 16		5 1 3 2 10 6 6	11 6 35	•	1 1 1 1 3 1 1	3 9 7 0 7 E 5 2 5 0 1 5 3 4 3 5 0	104 351 96 208 21 1035 1035	8 17 35 8 26 0 0

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<sup>.</sup> LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	CCAX CD		30 P <b>L</b> 60		•	V ERT E I			RIZENTAL Sheet	CENEU EAR	CTIVE TH
S BAIL YLAMONA	REAL PPM	CUAD PFM	REAL PPM	CAUS Mag	•	CEND MHDS	DEPTH*.	. MHES		FESIS CHM-M	DEPTH M
250E 250C 250D 250E 250F 250G 250H	0 6 5 3 4 21 5	5 12 13 3 10 15	0 4 6 23 2 43 2	3 13 22 2 2 22 41 1	•	1 3 2 34 2 14 18	0 . 0 . 5 . 0 . 0 2 3		1 103 59 52 52 39 48 106	107 153 103 5 58 12	54 16 14 35 7 23 52
251A 251B 251C 251D 251E 251F 251G 251H 251I	3 6 4 2 3 2 6 0 11 2	6 13 11 4 9 20 3 7	2 3 4 1 4 4 5 5 4	6 9 16 14 14 5 6 8 0	•	2 3 2 2 2 14 2 11 15	4 16 10 22 11 0 5 0		71 94 52 31 64 30 92 52 107	213 202 165 71 95 13 3 49	21 43 21 41 26 10 72 26 70
252A 252E 252C 252D	2 7 4 16	7 17 5 14	4 4 4 22	12 22 5 29	•	2 2 5 10	0 3 3	. 1	. 50 . 95	98 169 106 18	37 13 44 13
2538 2530 2530 2538 2536 2536 2534 2531	11 7 2 2 5 4 5 10 8	7 11 4 4 7 9 15 9	5 1 2 2 1 5 1 19 14	5 5 5 3 2 15 20 7	•	13 4 3 3 5 3 2 10 28	34 13 35 27 10 0	1 1	42 54 73 107 43 55 38	281 343 224 173 131 268 274 13	41 0 18 26 52 0 8 16 15
254B 254 <b>C</b> 254D	2 11 3	7 15 7	2 4 4	1 0 1 1 2	•	2 5 4	10 13 20	. 1	76	211 165 236	13 30 36

<sup>\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

<sup>.</sup> OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .
LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	DE AX		SDPL CC		•	VERT DI		•		ZENTAL EET	C C N C U E A R	CTIVE TH
LINE & ANOMALY	REAL PPM	QULD MAQ	FEAL PPM	CALQ MAG	•	CC ND SC HP	≎HTS∃C M		СИ6 <b>О</b> 20нм	D EPTH M	RESIS CHM-M	DEPTH M
254E 254F	2 <u>2</u> 2 3	1 4 1 4	5 4 5 2	3 4 3 2	•	22 29	0 0	•	<del>4</del> 5	3 <b>1</b> 25	10 7	1 1 7
255A 255B 255C 255C 255E 255F 253G 255H 255I	10 3 6 16 7 2 1	10 5 11 25 10 7 5 6 7	5 3 4 8 21 6 2 7	7 4 12 17 26 7 3 9	•	5 5 6 7 3 2 1 s	7 7 1 19 0 25	•	1 1 1 2 2 1 1	78 49 45 56 124 79 76 39	3 0 5 2 9 5 2 1 1 1 4 5 3 0 5 1 9 3 8 7 2 7 6	24 0 3 17 27 86 0 36 2
2554 2556 2560 2560 2560 2560 2560	2 5 13 5 9 4	6 11 37 12 7 5	4 10 10 13 7	7 18 39 20 15 7	•	2 3 4 3 10 6	6 6 3	•	1 1 1 2 1	55 43 38 51 39 63	1 92 1 79 1 42 1 57 34 1 1 4	10 4 5 12 9 19
257A 257E 257C 257D 257E	5 3 3 2 24	9 9 5 5 16	2 4 1 5 36	8 9 3 5 4 2	•	3 3 3 3 14	18		1 1 1 1 2	51 50 111 71 41	1035 287 863 1035 42	0 1 4 0 11
258A 258B 253C	3 3 10	5 10 13	3 2 2 0	5 7 22	•	4 5 · 7			1 1 1	55 67 39	203 388 304	5 9 0
25808 2580C 2580D	4 × 0 3 5	10 5 23	9 0 5 <b>7</b>	23 10 75	•	2 1 14	3	•	1 1 2	49 82 26	205 122 24	7 37 3
259A 259E	<del>9</del> 3	2 1 5	6 2	2 <b>7</b> 1 0	•	3	0	•	1	3 & 5 0	1 82 697	ე 0

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	X A C C		00 00 1		•	V ER T D I		•		ZENTAL EET	CENEU Ear	CTIVE TH
S PARTICLE S	REAL	CUAD PPM	REAL PPM	CAUQ M 49	•	SE NE	DEPTH≄ M		COND	DEPTH . N	RESIS CHM-M	DEPTH M
259C 259C	5 28	9 22	2 2 <b>7</b>	1 2 4 7	•	2 11	0 0	•	1 1	32 28	346 68	0 0
250A 250E 260C 260D 260E	5 0 0 10 0	9 11 10 15	2 2 16 3	7 5 17 23 12	•	3 2 7 2 8	5 0 0 0	•	1 1 1 1 2	4 6 3 4 5 5 1 5 6 7	251 1035 62 412 57	0 2 <b>7</b> 0 2 3
2614 2618 2610	1 4 11	15 8 11	0 6 5	20 9 12	•	1 2 7	12 7	•	1 1 1	2 \$ 5 0 5 3	850 317 225	0 2 7
262A 2625 262C 262D	5 2 10 32	10 7 17 22	2 1 11 54	11 4 21 60	•	3 1 5 16	0 1 0 0	•	1 1 1 2	4 é 111 4 é 35	247 1035 81 26	0 9 10
263A 263E 263C	12 1 52	25 6 39	15 1 108	3 2 3 9 1	•	5 1 22	0 3 0	•	1 1 4	45 127 37	3C 76 12	11 81 18
264A 264B 264C 264D 264E 264E 264F 264G 264H	5 1 0 5 6 7 8 6 9 6	8 7 4 5 11 8 5 6	2 2 0 10 2 14 215	9 3 0 3 17 3 6 159	•	3 1 1 4 4 6 16 31	5 0 14 19 0 26 19	•	1 1 1 1 1 1 2 5	42 128 101 67 35 68 78 24	487 1035 236 145 120 293 46	0 0 41 20 0 16 43 12
2658 265 <b>C</b> 265 <b>D</b>	2 1 3	10 14 23	2 2 10	3 7 31	•	1 1 3	0 3 0	•	1 1 1	40 32 45	467 614 107	0 15 11

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	4423 33		00PL 00		•	VERT EI		•		ECNTAL EET	0 0 M 0 0 3 4 3	CTIVE TH
LINE & ANCMALY	REAL	C AU D M q q	REAL PPM	DAUG Mag	•	CDND MH 3S	OEPTH#	•	COND MHCS	D EPTH M	RESIS CHM-M	DEPTH M
265E 265F	4 £4	1 1 5 2	5 136	3 125	•	3 21	10	•	1 4	51 36	970 10	0 19
266 266 2666 2666 2666 2666 2666 2666	2 2 4 5 1 7 13 5	5 0 2 2 5 7 11 6 5	1 10 4 7 0 2 14 8	3 5 2 5 1 4 1 0 1 2 1 7	•	1 4 12	11 57 0 1 0 6 4		1 1 1 1 1 1 2 2	47 64 25 32 41 40 50	5 6 6 93 2 7 0 1 1 6 3 1 4 2 2 1 3 1 3 7	0 25 0 0 0 0 21 6
267A 2675 267C	3 3 15	5 3 1 0	6 6 30	4 1 5 2 4	•	3 16	5 0 0	•	1 1 3	69 26 48	131 107 23	16 0 22
263A 263E 263C 263D	2 3 2 5	7 4 4 5	1 5 0 8	9 3 5 10	•	2 6	0 6 1 2	•	1 1 1	2 t 3 9 4 4 5 1	617 157 204 77	0 0 0 2 0
269A 269E	<del>4</del> 3	7 17	1 11	9 24	•	. 3	0	•	1	3 <b>6</b> 4 2	393 140	0 5
2704 2708 270C 270D 270E 270F 270G 270H	6 11 2 2 15 3 2 13	12 23 3 1 21 12 10 27	7 9 0 4 8 3 3 23	26 26 7 0 15 15 2		1 16 6 3	2 0 4 7 0 2 0 4 0	•	1 1 1 2 1 1 1	45 39 59 121 36 46 67 44	129 179 438 55 59 76 230 64	9 1 8 8 1 6 12 13
271A 271E 271C	11 61 5	30 68 25	7 <b>7</b> 5 5	3 3 11 3 2 9	•	_	0 11		1 2 1	32 29 29	144 27 684	0 7 0

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<sup>.</sup> LINE, ER BECAUSE OF A SHALLOW DIP OR GVERBURDEN EFFECTS. .

	XACO CO	IAL IL	CEPL CC		•		ICAL KE	•		ZCNTAL EET	CONEU EAR	CTIVE TH
LINE & ANEMALY	REAL PPM	CAUD M 99	FEAL PPM	CAU2 MRR	•	CE ND MH DS	DEPTH*.		COND 23HM	DEPTH M	FESIS CHM-M	DEPTH M
271E 271E 271F 271G 271H	1 16 10 5 13	4 1 9 2 0 6 9	3 28 20 11 11	2 3 3 3 3 9 3	•	9 5	3 0 · · · · · · · · · · · · · · · · · ·	•	1 2 1 2	71 28 41 63 65	391 39 119 45 73	13 0 7 27 24
2724 2726 2720 2720 2726 2726 2726 2726	0 5 15 0 2 5 2 25	2 10 10 7 13 12 5	5 0 14 0 8 4 0 26	3 13 20 9 50 20 1	•	10	26 0 0 9 0 1		3 1 1 1 1 1	162 76 53 71 20 58 111 33	16 146 59 1035 173 111 127 52	130 28 16 0 0 19 57
273A 273E 273C 273D 273E 273F 273G 273H 273I	2 5 8 6 6 0 2 12	6 11 11 10 17 3 21 12	4 2 5 4 5 0 0 10 4	7 12 22 5 15 1 29 22 13	•	2 2 4 5 3 1 1 7	27 1 0 8 0 0 0		1 1 1 1 1 1 1	93 47 47 45 53 58 11 35 52	1035 198 126 153 137 239 574 99 318	0 5 8 4 14 10 0 5
274A 274E 274C 274D 274E 274F 274G	6 14 3 13 2 0	3 19 6 23 8 6 24	2 12 4 22 2 0 12	8 3 9 7 4 0 9 1 3 4	•	4 5 3 5 2 1 5	10 . 0 . 2 . 0 . 1 .		1 1 1 1 1 1	56 35 56 37 57 87 44	197 152 144 68 223 159	11 0 11 6 11 34 12
275A 275E 275C 275C 275E	έ 3 4 2 3	3 7 5 7 11	5 4 5 2 3	11 6 13 9 12	•	4 3 3 2 4	9 . 10 . 0 . 1 .		1 1 1 1	47 48 106 38 30	220 502 113 1035 250	0 0 5 3 0 0

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

	ee 4x		03PL 00		•	V ERT D I		•		ZCNTAL EET	SCNDU EAR	CTIVE TH
LINE & ANDMALY	REAL PPM	CAUS	REAL PPM	QUAD PFM	•	COND	#HT93C		CAES ZOHM	DEPTH M	RESIS CHM-M	DEPTH M
275F 275G 275H 275I	4 2 2 13	5 9 11 25	2 0 0 13	11 11 9 48	•	3 1 1 5	1 3 0 0 0	•	1 1 1	54 54 59 25	24 <b>4</b> 30 <b>4</b> 309 98	14 6 9 0
1764 2768 2768 2768 2768 2768	11 2 2 3 2 44	15 3 7 7 7 28	11 1 0 4 0 83	2 3 5 3 11 7 5 4	•	5 1 2 7 1 16	1 0 13 0 0	•	1 1 1 1 1 3	49 42 72 32 24 25	172 904 931 196 956 17	7 0 0 0 0 0 4
277A 277E 277C 277D 277E 277E 277F 277G 277H 277I	5 2 4 5 4 4 3 B	17 11 13 2 32 9 10	7 0 2 4 3 5 3 4 5	27 11 3 15 2 62 30 13 10	•	3 1 15 2 12 14 2 2	0 0 0 2 5 0 5 8 0	•	1 1 1 1 3 1 1	29 39 38 38 109 31 67 28 53	538 903 830 332 197 17 252 956 100	0 0 0 53 9 17 0 8
2770A 2770E 2770C	37 72 99	42 85 107	69 171 171	94 175 218	•	12 17 17	0 0 0	•	3 2 3	23 19 20	18 19 13	2 0 3
278A 278E 278C 278C 278E 278E 278F 278G 278H	1 99 108 0 4 0 93 84	4 136 116 12 15 15 50 90	1 182 158 4 2 0 187 187	1 273 203 9 10 6 201 201	•	2 14 17 2 1 1 20 18	17 0 0 8 6 17 0	•	1 4 4 1 1 1 5 4	145 20 21 31 41 25 20	499 9 5 752 421 689 7	48 5 5 0 0 0 5 2
2794 2798	.2 .1	7	0 2	5 <b>7</b>	•	1	2 1 5	•	1	118 59	1035 1029	0 0

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<b>32</b>	•											
	CCAXI		002L4 001	.N. 4 R	•	VERTI SIR	ECAL .	•		ZCNTAL EET	CONDU EAR	
LIKE & ANDMALY	REAL PPM	.L (U4D PFM	FEAL PPM	CU40 PPM	. ε	D ND H OS	*HT93C M		С ЛЕ Э 2 ОН М	DEPTH M	R ESIS C HM-M	DEPTH M
27 ±0 27 9D 27 9E	1 8 3 2 7	10 3 22	48 1 65	25 3 49	•	27 2 18		•	5 1 4	38 75 28	5 5 2 5 1 0	21 10 10
250A 28 <b>0</b> 6	6 5	3 14	5 · 1	9 15	•	F1 (II	9	•	1	57 31	271 776	5 0
2800A 2800E 2800C 2800E 2800E 2800A 2800A 2800J 2800J 2800J	1 5 2 2 2 2 1 27 37 125	4 5 9 8 7 5 6 8 5 4 4 4	3 2 3 1 0 0 2 60 93 212	2 15 5 5 1 2 19 56 275		3 2 2 1 1 2 1 61 27 18	15 3 0 2 2 17 12 15 5		1 1 1 1 1 1 1 5 6	160 30 55 41 41 68 77 45 38	120 742 287 674 731 569 440 7	101 0 5 0 1 18 29 24 4
261A 281£ 281C 281D 281E 281F 261G 261H	3 1 2 60 1 0 0 95	3 5 5 2 1 2 8 5 11 6	11 0 9 139 1 0 0	17 2 22 115 4 11 13 219		6 1 3 22 1 1 2 15	2 5 0 0 0 1 0 3	•	1 1 1 5 1 1 1	73 41 22 57 34 57	82 527 98 5 277 474 82 9	17 8 6 8 11 0 21 3
282A 282B 282C 282D 282E 282F 282F 282G	1 4 1 1 3 5 5 4 3 5	4 7 21 63	6 2 26 95	136 11	•	2 6 1 5 13 7	13 10 0 15	} •	2	66 50	634 114 566 57 13 18 29	15 20 0 0 3 15 9
28 <b>3A</b> 263b	2	, <u>.</u> 2 2 2 2			•	10	•	0 .		1 59 1 21	89 334 • •	

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102 5.45												
	CCAX		00°L:			VEFT	ICA KE	<u>.</u>		ZONTAL Eet	DENEU( EAR	CTIVE TH
LINE S ANDMALY	REAL PFM	CUFD PFM	FEAL PPM	CAU MAS	•	CD 4D 3C 4M	Σ:	EPTH*.	С Л С Э 2 Э Н М	DEPTH N	RESIS CHM-M	DEPTH M
2830 2830 2830 2836 2836	3 5 15 4	10 0 22 6	2 0 2 9 8	13 0 59	•	2 4 9 5 5		5 • 6 • • 0 •	1 2 2 2	42 54 30 65	108 36 33 51	5 23 4 2 <b>7</b>
28404 28409 28400 28400 28400 28400	3 2 1 7 7	7 5 14 19 26 3	7 1 1 3 9	17 7 10 22 41 27	•	1 2 2 5		7 . 11 . 0 . 0 .	1 1 1 1 1	43 62 51 32 29 41	249 771 212 204 137 117	0 0 10 0 0 6
2854 2857 285 <b>0</b>	21 1 3	3 5 9 7	44 1 1	ε <b>1</b> 7 3	•	. 7		0 .	2 1 1		41 173 178	1 19 2
2868 2865 2860 2865 2865 2865 2866	2 2 1 3 3 3 3 2	4 11 6 42 19	1 3 0 61 9	25 4 100 23	,	2 2 1 1 10 11		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 2 2	39 34 96 34 22	851 686 844 838 31 387 37	14 0 0 1 8 0 23
287A 287E 287C 287D 267E		) 3 7 4 6 4 1 7	3 0 6 79 7 1	) 2 9 114		. 1 . 1 . 13	L S	19 10 0 0	•	63 5 5 0 2 21 1 39 2 46	502 198 26 153 55	10 29 0 2 9
288 <b>A</b>	:	3 1	1	5 17			2	Ó	•	1 49	287	1
2880A 2880E 2880C 2880C	3	<ul><li>5</li><li>1</li><li>3</li><li>3</li></ul>	3 4	2 7 3 23 4 73 1 23		. 1	1 2 C	0 3 0	•	1 95 1 36 2 29 1 30	1035 717 43 106	0 2

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LINE, OR BECAUSE OF A SHALLOW DIF OR OVERBURDEN EFFECTS.

				•	V EFT I	ISAL Ke	•					
PEAL PPM	C AU D P F M	REAL	CAUS	• "						DEPTH M	RESIS CHM-M	HTSEC M
14 10	2 2 1 3	15 15	2 3 3 3	•	5 4		<b>4</b> •		1	40 41	5 <del>6</del> 2	10 11
1 24 1 62 41	5 3 2 1 6 3 3 2	2 23 0 101 83	11 45 0 134 75	•	1 11 1 15 22		0 0 0 0 0		1 2 1 3 4	52 36 44 20 18	437 48 90 15 10	7 7 9 1 1
2 1 32 14 73	5 3 26 16,	2 1 21 22 149	5 2 40 34 53	•	2 2 11 8 34		3 · 0 · 3 · 0 ·	•	1 1 2 2 5	134 136 33 32 32	1035 1035 43 51 6	0 0 4 4 13
5 1 25 5 43 63		4 0 23 1 51 121	7 3 65 21 62 139	•	6 1 7 3 16 16		14 · 7 · 0 · 10 · 0 · 0	•	1 1 1 1 3 4	70 72 25 55 30 21	237 1035 54 62 15	13 0 0 21 10 4
8 1 4 5 3	9 0 3 3	0 0 76	17 18 3 15 74 141	•	20		4 7 6 8 4 0	•	1 2 1 2 4 2	50 46 61 40 33 26	270 54 64 45 9 20	5 13 26 12 16 5
				•	3				1	35 100	256 1035	0
51	2 5 1 50	5 0 9 9 3	3 9 9	•	1 1 6	l É	11	•	1 1 3 1	73 75 29 56	1035 1035 15 61	00924
	CC PEPM 140 14127 21243 516533 681450 151653 1653 1653 1653 1653 1653 1653 16	PPM PFN  14 22 10 13  1 24 32 1 63 47 32 2 1 36 1 73 43 5 7 25 14 73 43 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	CCIL CCIL  PEAL QUAD REAL PPM PFN PPM  14 22 15 10 13 15  1 0 2 24 32 23 1 0 101 47 32 88  2 1 26 21 14 16 22 73 43 149  5 6 4 1 7 0 2 5 32 23 1 43 31 51 63 66 121  63 63 121  64 8 9 17 1 0 0 4 8 9 17 1 0 0 5 3 2 3 76 6 3 6 6 76 8 9 17 1 0 0 0 5 3 3 3 76 6 8 9 17 1 0 0 0 5 3 2 3 76 6 8 9 17 1 0 0 0 5 3 3 3 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 8 9 17 1 0 0 0 5 3 5 8 76 6 9 8 9 17 1 0 0 0 5 3 5 8 76 6 9 8 9 17 1 0 0 0 0 5 3 5 8 9 17 1 0 0 0 0 5 3 5 8 9 17 1 0 0 0 0 5 3 5 8 9 17 1 5 1 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CCIL CCIL  PEAL CUAD FEAL SUAD PPM PFM  14 22 15 23 10 13 15 23 10 13 15 23 10 13 15 23 11 24 26 26 21 40 21 47 32 26 21 40 21 47 32 26 21 40 21 47 32 26 21 40 21 47 32 26 21 40 21 40 22 24 43 21 49 53 26 26 21 40 21 40 22 24 43 21 49 53 26 26 21 40 21 40 22 24 43 21 49 53 26 26 21 40 21 139 26 26 26 21 21 139 26 26 26 21 21 139 26 26 26 21 21 139 26 26 26 21 21 139 26 26 26 21 21 21 21 21 21 21 21 21 21 21 21 21	CCIL CCIL CCIL CCIL CCIL CCIL CCIL CCIL	CCIL CCIL CCIL CCIL CCIL CCIL CCIL CCIL	PEAL QUAD FEAL QUAD	CCIL CILL CIRE  PEAL CUAD FEAL CUAD COND DEPTH*  PPM PFM PFM PFM PFM PFM PFM PFM PFM PFM	CCANTAL CUAD FEAL CUAD CONE DEPTH*. CAMP OF M PF	CCAXIAL CULAD FEAL SULD SCENE SEPTH* COND PFM	Coll	CCIL COLL COLL COLL STARS SHEET EAR  PEAL CUAD FEAL CUAD COLL STARS MHOS N CHAPPA  PEAL CUAD FEAL CUAD STAR MHOS N CHAPPA  14 22 15 23 5 1 1 40 62  14 22 15 23 5 1 1 40 62  1

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	CCAXI CCI		00 PL 4 00 I		•	VERTI DI:		•		ZCNTAL EET	SENEU EAR	
LINE &		C 4U 3 M 99	REAL PPM	CAUC	-	DND HDS	DEPTH*。 M		COND MHCS	DEPTH M	RESIS CHM-M	DEPTH M
2930E 2930F 2930G 2930H	75 3 23 30	49 10 32 32	129 3 67 67	109 10 70 70		26 3 13 13	17 0 0	•	4 1 2 3	2 & 3 & 2 5 3 5	8 90 22 14	1 2 8 3 1 5
2944 2944 2944 2944 2944 2944 294	7 3 34 11 18 14 24	13 13 39 13 27 15 21	2 75 24 24 14 41 3	14 12 81 29 41 23 43	•	3 13 7 3 13 8	4 3 0 7 5 12	•	1 1 4 2 2 2 2 3 3	48 42 26 46 44 45 31 34	279 652 11 31 27 33 16 14	3 0 3 19 19 18 9
295A 295B 295C 295C 295E 295F 295G 295H 295I	3 4 3 3 3 15 87 3 23	12 3 3 5 2 19 53 12	4 3 3 0 67 0 144 0 34	14 3 5 6 3 13 13 24	•	4 2 3 2 17 8 6 8 15	0 15 0 12	•	1 1 1 1 2 2 2 4 1 3	1 é 82 92 78 3 é 59 27 41 33	831 245 194 325 25 43 8 8	0 30 37 24 12 27 12 11
2950A 2950E 2950C 2950D 2950E 2950F 2950G 2950H 2950I	6 3 44 23 17 29 1 53 53	13 12 40 33 20 29 4 23	24 23 19 0	16 10 74 35 33 39 36 45	•	2 1 18 8 9 1 26 27	10 3 13	•	1 1 4 2 2 2 2 1 4 4	46 28 44 41 47 42 32	654 873 10 38 29 29 127 10	0 0 11 17 15 22 8 15
295A 295E 295C 295D	3 5 2 10	5 9 5 1 2	; 2	4 7 4 17	•	(3) (2) F4 (3)	17 14		1 1 1 2	. 50 92	1035 702 1035 26	0 0 0 2 6

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	CE 4X CC		CCPL CC		•	VERT DI		•		ZCNTAL EET	CENEU Ear	
LINE & ANDMALY	REAL PPM	CAUD	FEAL PPM	CAU2 MAG		OD VD SCHM	DEP <b>T</b> H≭ M		C A C D Z D F M	DEPTH P	RESIS CHM-M	DEPTH M
29 6E 29 6F 29 6G 29 6H 29 61 29 6J	7 6 9 0 14 42	9 9 9 5 5 19	13 0 16 0 32 55	17 6 16 3 22 23	•	8 4 10 1 23 34	0 0 0 0	•	2 1 2 1 3 4	52 49 42 52 38 29	35 110 49 78 15 8	21 10 9 22 18 11
297A 297E 297C 297E 297E 297E 297G 297C	5 5 19 14 7 7 0 20	7 17 24 24 7 12 55 55	2 30 30 33 33 0 55 152	9 12 20 29 19 28 114	•	3 10 2 5 4 1 9 34	6 2 6 13 9 2 0	•	1 1 3 2 2 1 1 5	71 52 45 46 51 47 65 45 25	212 423 19 34 56 59 59	21 6 22 18 13 15 23 30 12

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	X		CC PL .		•	VERT LI		•		ZONTAL EET	UDNDO BAR	
LINE & YJAMONA	REAL	QUAD MAG	FEAL PPM	CAUS	•	CC VC MH OS	M W		C D N D M H E S	DEPTH M	RESIS EHM-M	DEPTH M
301A	23	20	19	3.5	•	10	0	•	2	35	46	5
302A	14	÷	14	21	•	10	9	•	2	53	45	19
303A 303P	2.6 2	2 5 9	31	53 13	•	ş 1	) 0	•	2 1	2 E 2 <del>č</del>	3 <b>9</b> 956	1
30+A 30+E 30+C	1 2 7 7	8 12 14	<b>Φ</b> Φ Φ	1 5 2 2 2 2	•	10 3 3	3 9 0		1 1 1	59 35 39	12 <b>1</b> 410 233	14 0 0
305A 305E 305C	59 13 17	37 20 20	71 14 14	75 31 31	•	21 5 7	0 0 0	•	4 1 1	38 58 53	12 80 64	19 20 18
30 54 30 6E 30 6C	30 3 24	15 10 25	35 7 44	34 14 59	•		0 0 0	•	4 1 3	47 75 33	12 96 21	25 33 9
3078 3070 3070	36 2 4	23 5 0	2 9 1 7	43 9 7	•	1	0	•	2 1 2	33 75 39	29 240 53	5 2 2 2
308A 3085 3080	19 4 7	9 1 2 7	19 3 16	19 13 13	•		0 2 0	•	3 1 2	59 43 41	25 44 <b>1</b> 3 <b>4</b>	33 0 10
309A 309E	27 5	1 5 1 2	26 0	24 14	•		9 0		2	57 47	36 365	2 <del>6</del> 0
310A 310E 310C	54 7 4	4 0 9 5	6 5 <b>7</b> 2	7 9 1 1 5	•	17 5 3	0 3 5	•	3 1 1	31 54 31	17 233 1035	9 7 0

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LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X430 30		SEPL SE		•	VERT BI		•		ZONTAL EET	CENEU EAR	
LINE &	REAL PPM	C 4U D M 4 G	FEAL PPM	CAUS MAG	•	CD ND MH DS	DEPTH≭. M		COND	DEPTH M	RESIS EHN-M	DEPTH M
310E	3	3	2	5	•	3	3 .	•	1	47	420	0
311A 311E 311C	43 12 7	23 15 11	65 9 9	5 <b>1</b> 2 0 2 0	•	26 6 4	D .	•	4 1 1	32 70 60	8 63 78	14 31 20
312A 312E 312C 312C	86 20 6 29	5 8 2 4 9 2 7	159 21 4 99	138 38 14 <b>71</b>	•	2 6 8 4 20	0 2 0	•	5 1 1 5	22 42 48 35	5 110 294 5	9 7 0 19
313A 313E 313C 313D 313E	70 23 25 5 24	47 25 35 7 14	97 44 44 2 27	105 58 58 7 21	•		0 0 0 4	•	4 2 2 1 2	3 0 5 0 3 6 3 9 5 1	10 36 27 243 46	13 20 10 0
314A 314B 314C 314D 314E 314F 314G 314H	5 39 8 7 13 2 5	4 20 14 16 15 12 23 23	1 56 14 22 9 0 23 21	4 50 25 27 10 14 25 25	•	6 m m 6 8 t	3 <b>1</b> 0 0	•	1 4 1 2 2 1 3	117 34 40 46 42 16 56 47	213 12 61 27 35 268 23 93	5 5 1 5 7 1 9 1 3 0 3 0 1 3
315A 315B 315C 315E 315E	3 35 17 1	6 15 21 4 10	0 43 18 0 23	3 3 4 3 0 3 2 7	•	2 27 8 2 10	0 0 0 12 3	•	1 3 2 1	96 - 43 - 45 - 63 - 49	1035 21 43 214 57	0 18 14 13 15
316A 316E 316C	4 0 9 2 3	21 13 19	83 12 43	52 27 36	•	31	0 3 0	•	5 1 2	44 47 46	107 32	27 11 17

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

<sup>•</sup> DE THE CENEUCTER MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT • LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. •

	25 A X		COPL CC		•	V ERT		•		ZCNTAL EET	CENETU EAR	CTIVE TH
LINE S ANSMALY	REAL PPM	04U3 M49	PEAL	Q A D M 3 S	•		DEPTH*		COND 8 dh M	DEPTH K	RESIS CHM-M	DEPTH M
3174 3178 3170 3170 3170	3 51 10 0 7	4 31 15 4	1 70 9 2 4	5 61 22 4 13	•	4 23 5 1 4	13 0 0 3 12	•	1 3 1 1	67 44 43 73 55	1035 15 115 339 195	0 23 5 16 12
318A 3182	15 7	11 11	21	21 17	•	12	0 <b>1</b>	•	2 1	49 5 <b>6</b>	4 <b>4</b> 95	14 24
319A 319E 319C 319D	5 27 8 13	7 15 14 14	5 30 4 13	3 23 15 20	•	5 21 4 11	0	•	1 2 1 1	73 57 63 49	156 32 194 58	25 27 16 14
320A 320B 320C 320C	20 25 5 15	19 15 10 17	19 34 5 20	29 22 3 23	•	10 22 4 5	0		2 2 1 2	47 61 64 43	44 34 313 54	15 31 13 9
321A 321E 321C 321D 321F	2 53 15 5 19	7 45 20 4 13	1 59 11 3 19	9 60 22 14 27	•	1 15 6 4 12	0	•	1 2 1 1 2	80 48 56 46 49	1035 22 127 172 38	0 24 15 3 18
322A 322E 322C 322D 322E	2 19 3 19	6 9 3 6 16	1 27 10 1 33	3 19 14 9 37	•	2 21 & 2 12	3 0 9 0 0	•	1 2 1 1 3	111 67 78 75 31	751 37 142 154 20	5 34 29 23 7
323A 323E 323C 323C 323E	2 11 14 4 22	4 5 13 5 26	1 5 11 1 62	3 5 14 9 72	•	2 18 10 3	14 5 4 1		1 2 1 1 3	195 134 77 86 36	845 68 78 140 14	43 90 35 33 16

<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

<sup>.</sup> OF THE CONDUCTOR MAY BE DEEPER OR TO DNE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

	X433 30		20 20		•	VERT EI		•		IONTAL Bet	CCNEU EAR	CTIVE TH
LINE & ANDMALY	FEAL PFM	CAU) Mag	FEAL PPM	GAUQ PAM	•		SEPTH# M		MHC2	DEPTH N	RESIS CHM-M	DEPTH M
3244 3248 3240 3240 3240 3248	1 22 9 13 3	5 15 13 13	1 31 7 16 13	2 3 0 1 4 2 4 1 7	•	1 1 é 5 9 4	0 2 9	•	1 2 1 2 2	162 46 50 57 58	1035 37 207 48 29	0 15 5 23 29
52 <i>5A</i> 32 <i>5</i> 2 32 <i>5</i> 0 32 <i>5</i> 0	1 1 9 9	3 6 <b>7</b> 9	1 3 7 2	5 3 9	•	1 1 5 6	0 4 14	•	1 1 1	113 129 42 56	1035 1035 843 1035	0 0
3268 3268 3260	7 9 8	10 3 16	15 13 3	15 12 23	•	6 11 3	70 Ó O	•	1 2 1	70 3 c 57	101 45 73	26 50 13
327A 327E 327C 327C 327E	1 2 13 5 4	7 3 8 15	0 10 12 2 3	7 12 13 25 25	•	15332	0 3 0 0	•	1 2 1 1	75 75 65 26 31	1035 55 64 257 237	0 3 5 2 6 0 0
323A 323E 323C 328D 328E	2 4 9 3 0	7 4 3 1 2	1 1 5 5 4	1 13 4 15	•	2 3 28 4 6	3 0 12 0 17	•	1 1 5 1	189 76 150 31 156	1035 1035 7 180 96	0 0 123 24 100
329A 329E 329C 329E	2 4 23 8	5 3 11 12	2 1 10 14	5 3 12 15	•	2 6 20 6	0 22 9 0	•	1 1 2 1	6 <b>1</b> 92 33 58	424 416 49 82	1 20 47 18
330A 330E 330C	3 1 2 2	7 7 4	0 11 7	6 12 11	•	2 14 3	0 0 0	•	1 3 1	7 E 9 8 5 4	180 22 104	25 6 <b>7</b> 8

<sup>\*</sup> ESTIMATED CEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

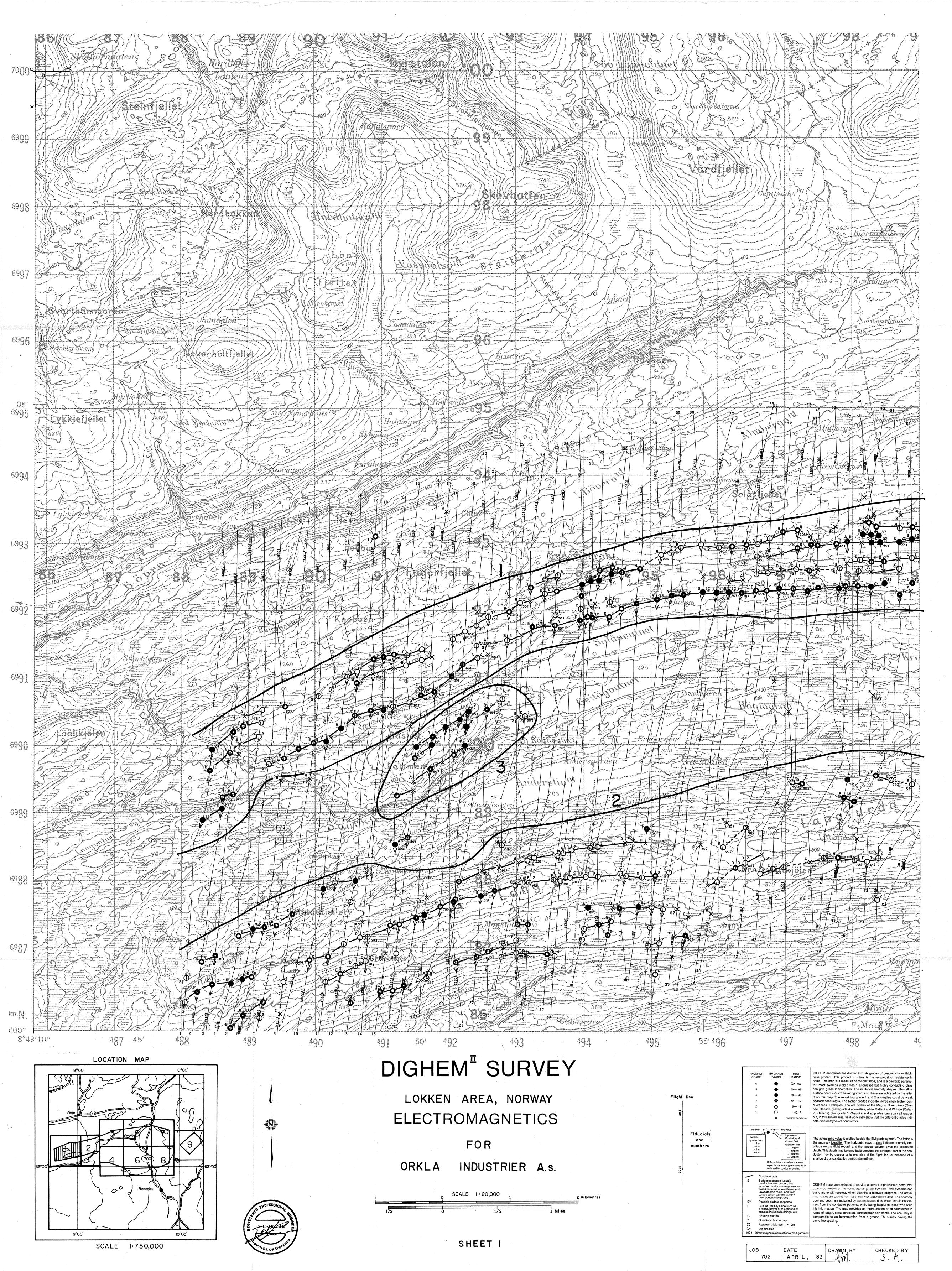
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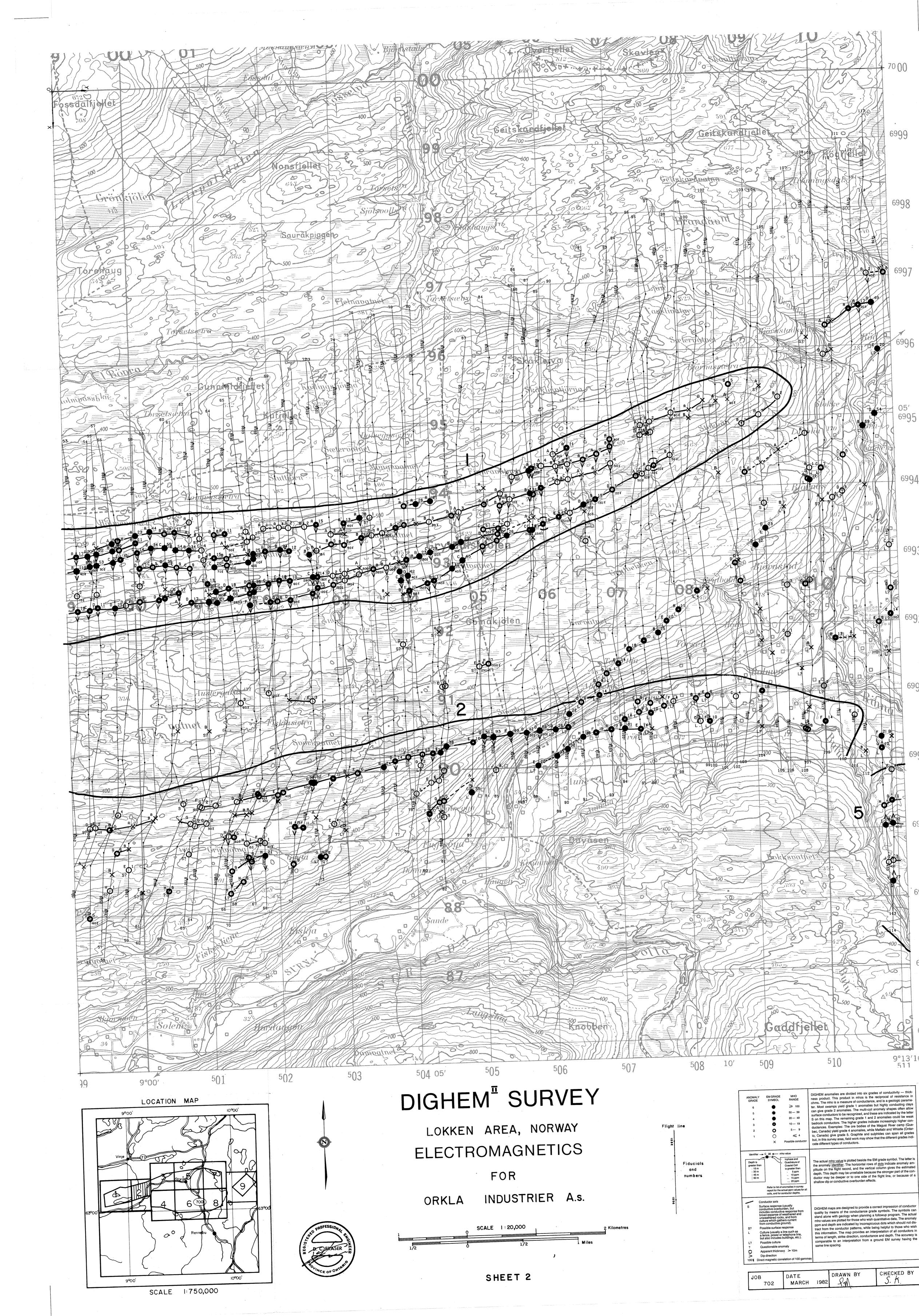
LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .

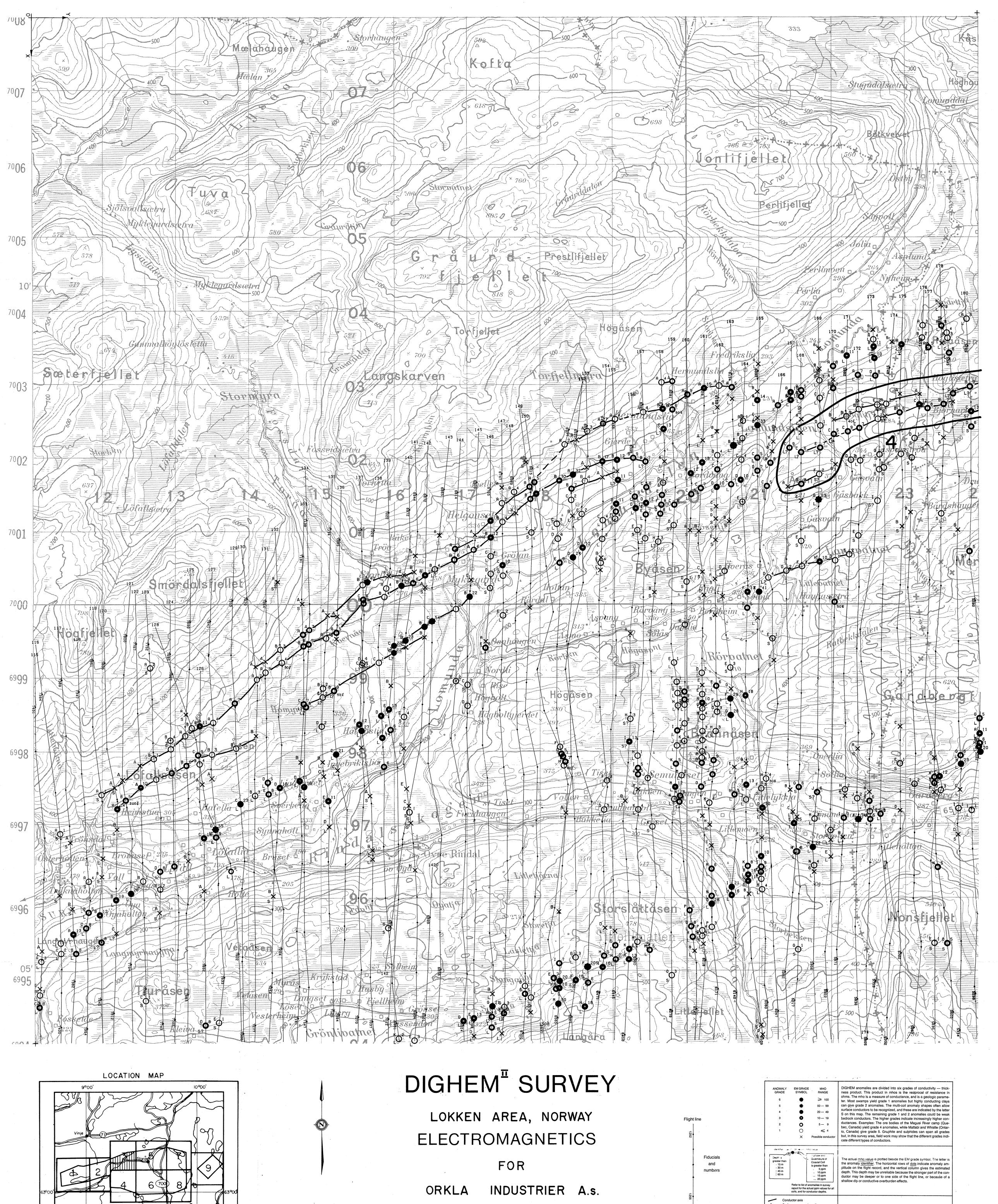
	XA30 <b>3</b> 0		SCPL SC		•		ISAL .		ZENTAL EET	SENDU Ear	ICTIVE ITH
LINE & ANDMALY	REAL PPM	C 4U J M 4 9	FEAL PPM	C 4 U D M 4 9	•	SEND	· · 本中TP3C · M	K 4 E S	DEPTH M	RESIS EHM-M	DEPTH M
3314 3315 3310	3 11 13	7 11 17	1 14 14	15 19 15	•	1 3 10	0 . 0 . 7 .	1	91 45 95	167 71 52	3 6 8 5 <b>7</b>
33 2 <b>A</b> 33 2 <b>C</b> 53 2 <b>D</b>	9 2 11	9 7 10	1 2 . 5 9	2 2 1 3 - 6	•	7 2 10	9 . 0 . 2 .	1 1 2	47 50 94	66 154 33	10 5 61
323 <b>A</b> 333 <b>E</b>	1 ŝ	13 4	13 6	2 5 5	•	9 14	• • • •	1	54 120	104 507	16 29
334E 334E 334C	7 2 12	6 4 9	7 1 11	10 10 7	•	7 1 13	5 . 0 . 12 .	1 1 2	56 61 91	29 <b>7</b> 1035 48	11 0 54
335A 335E	3 <b>7</b>	5 3	3 10	<b>7</b> 9	•	3 14	7 . 15 .	1 1	7 <i>6</i> 107	500 31	5 60
4688	5	2	કૈ	9	•	13	14.	2	118	36	81
337A 337E 337C	1 0 5	2 5 2	6 3 3	5 7 7	•	5 1 13	23 . 0 . 23 .	2 1 2	112 39 167	34 188 61	77 33 121
336A	15	10	13	17	•	14	1 .	1	68	107	23
33 <b>9</b> 4	14	10		2 0	•	16	0.	2	63	33	3 2
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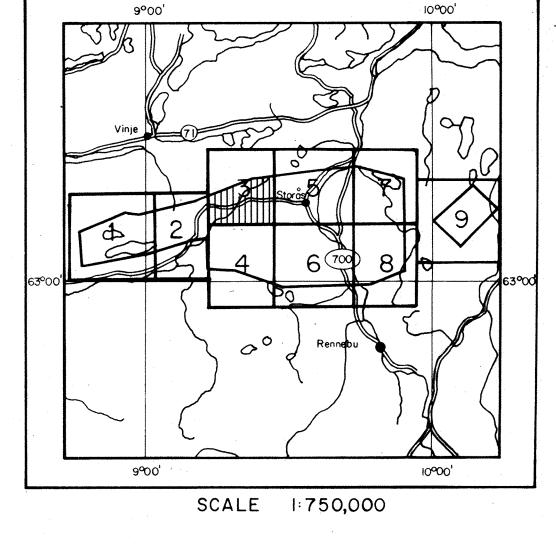
<sup>.\*</sup> ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

<sup>.</sup> OF THE CONDUCTER MAY BE DEEPER OR TO DAY SIDE OF THE FLIGHT . LINE, OR BECAUSE OF A SHALLOW DIF OR OVERBURDEN EFFECTS. .

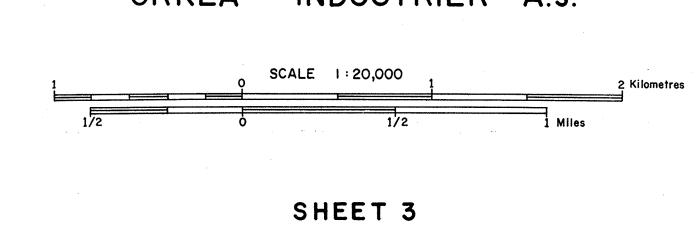




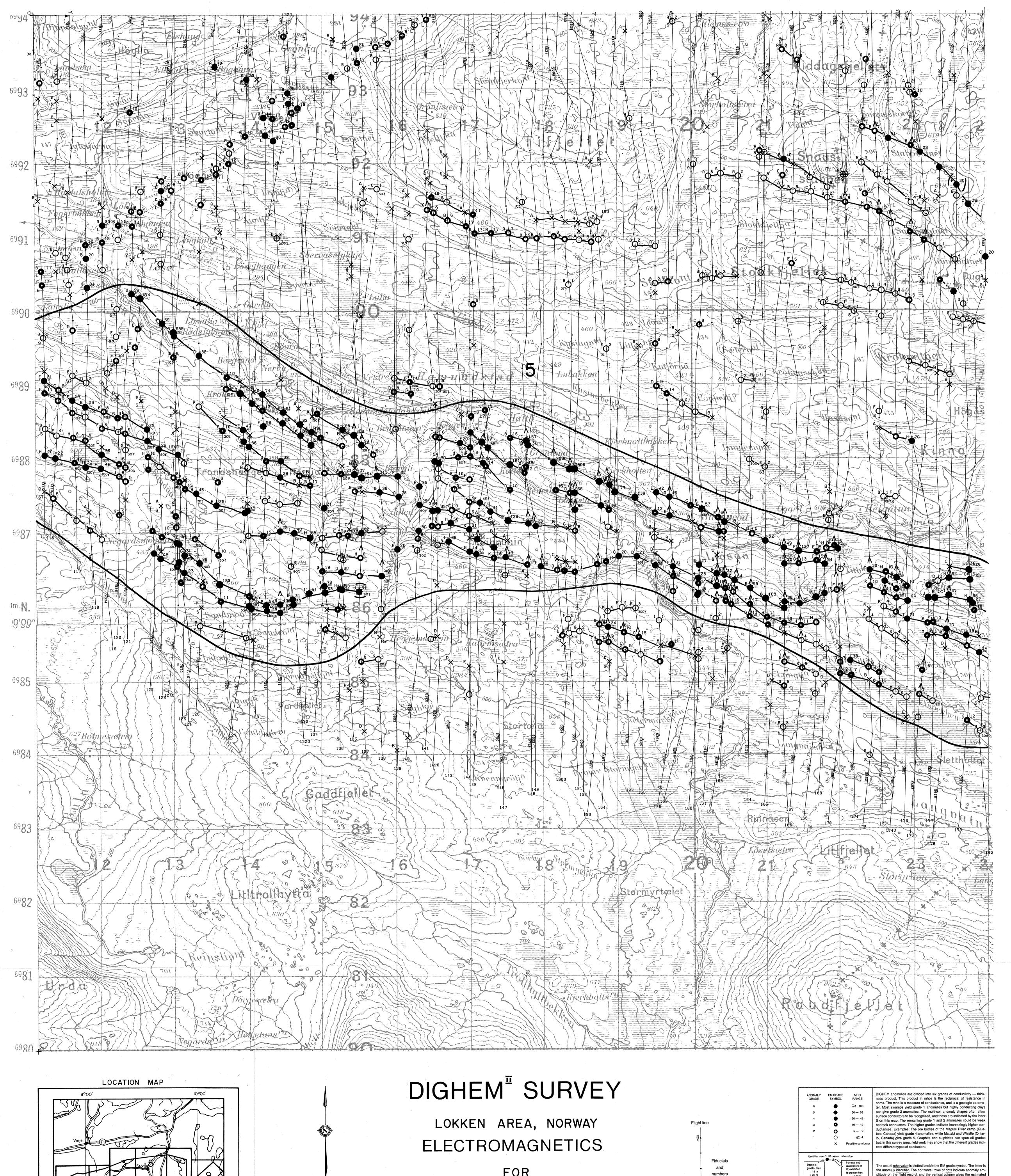


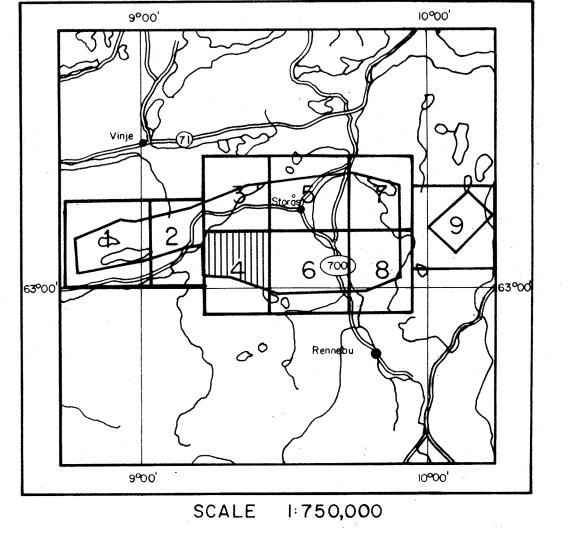


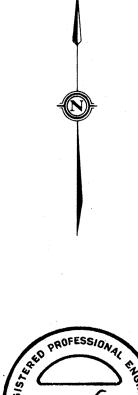




				. 1			Section 1	
	ANOMALY EM GRADE SYMBO		ness pro ohms. T ter. Mos can give surface of S on this bedrock ductance bec, Can io, Cana but, in th	M anomalies are divided it oduct. This product in me he mho is a measure of cit swamps yield grade 1 agrade 2 anomalies. The conductors to be recognized so map. The remaining grade 2 anomalies. The ore broadaly yield grade 4 anomadaly give grade 5. Graphis survey area, field workerent types of conductors.	thos is the conductary anomalies multi-color and the codes incorporate of alies, while and set to code and set	he reciproca nce, and is a se but highly il anomaly s hese are ind id 2 anomali dicate increa the Magusi ile Mattabi a sulphides ca	al of resistance a geologic para or conducting constances often a licated by the le- ies could be wassingly higher of River camp (Ond Whistle (Or an span all gran	e in ime- lays illow etter veak con- Que- ntar-
	report for the	Cuadrature of Coaxial Coil is greater than . 5 ppm 10 ppm 15 ppm 20 ppm of anomalies in survey e actual ppm values for all ronductor depths.	the anor plitude of depth. T ductor n	ual mho value is plotted be maly identifier. The horizo on the flight record, and t his depth may be unreliab nay be deeper or to one dip or conductive overbure	ntal rows he vertic le becau side of t	s of <u>dots</u> ind al column g se the strong he flight line	icate anomaly ives the estimate ger part of the control of the con	am- ated
-	broad expanse of unweathered roc culture which gat from conductive  S? Possible surface L Culture (usually: a fence, power o but also includes L? Possible culture ? Questionable an C Apparent thickne Dip direction	purden, but itive response from if weathered and ks, and from thers current ground). response a line such as r telephone line, buildings, etc.).	quality by stand all mho value ppm and tract from this information terms of comparate	If maps are designed to proper your means of the conductations with geology when places are plotted for those will depth are indicated by in the conductor patterns, remation. The map provide length, strike direction, could be to an interpretation e spacing.	ance grad anning a tho wish o conspicu while be s an inte	de symbols. followup prequantitative of cous dots wheing helpful terpretation of ce and depti	The symbols ogram. The ac data. The anon ich should not to those who we fall conductors. The accuracy	can tual naly dis- vish s in
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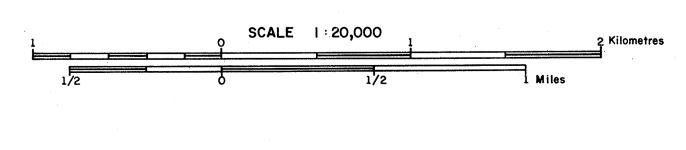




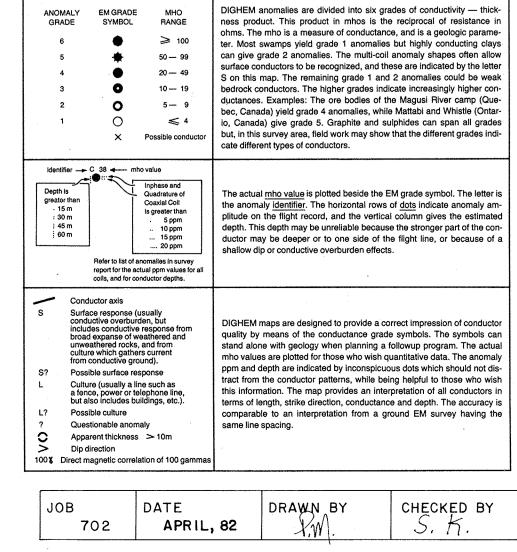


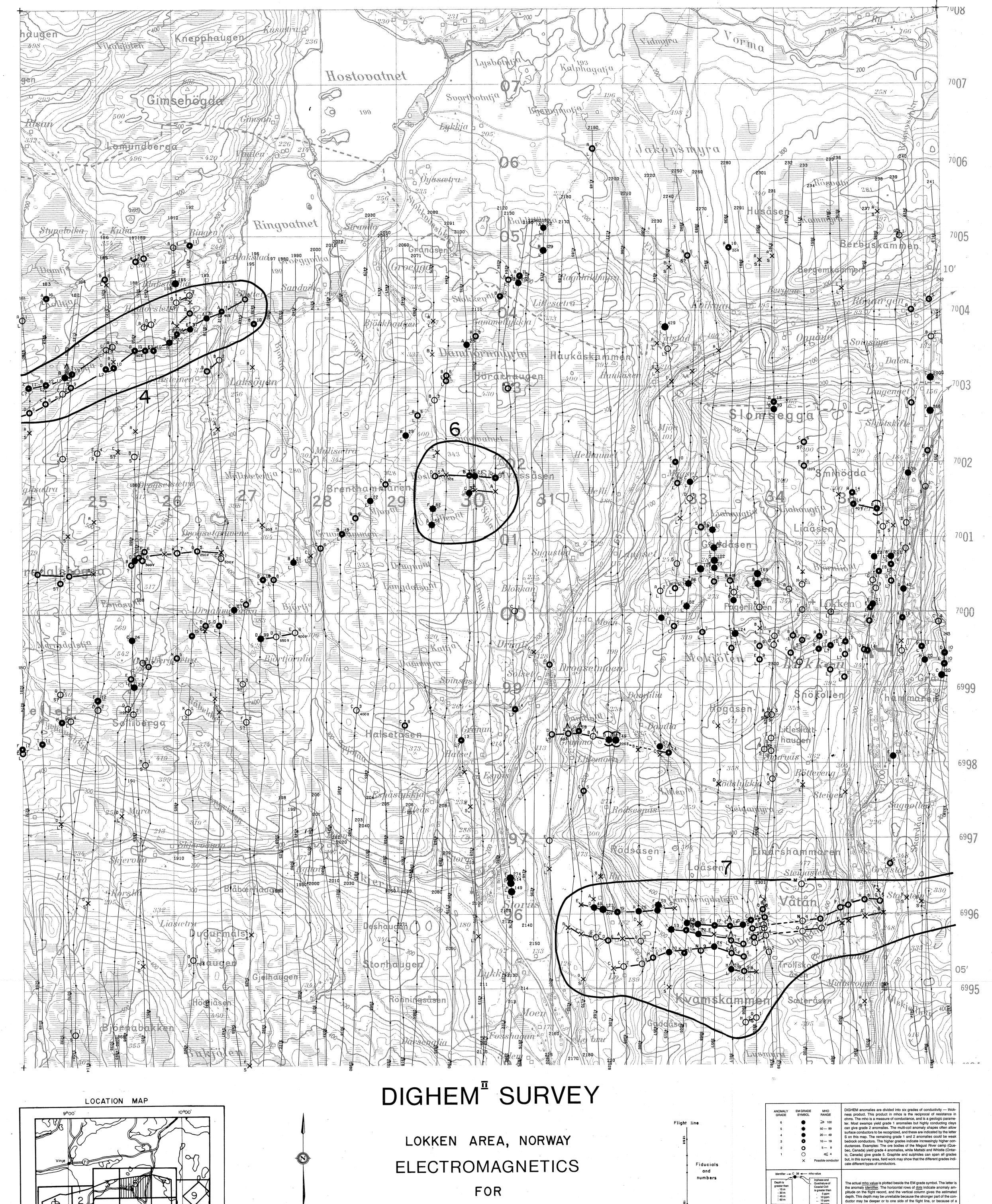
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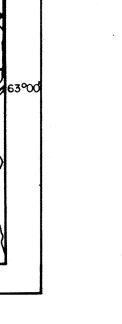
INDUSTRIER A.s. ORKLA





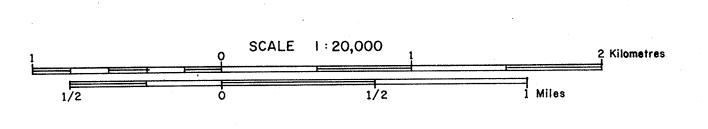




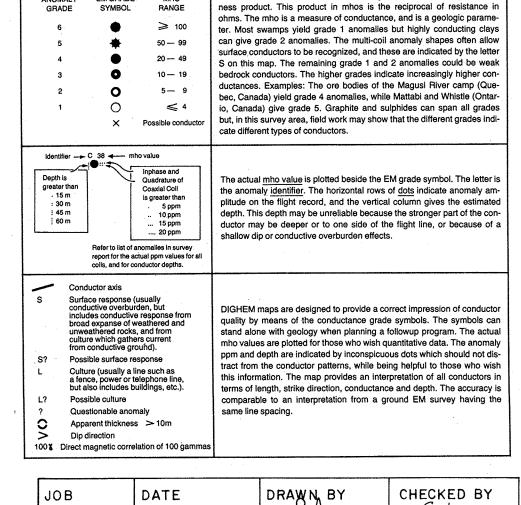


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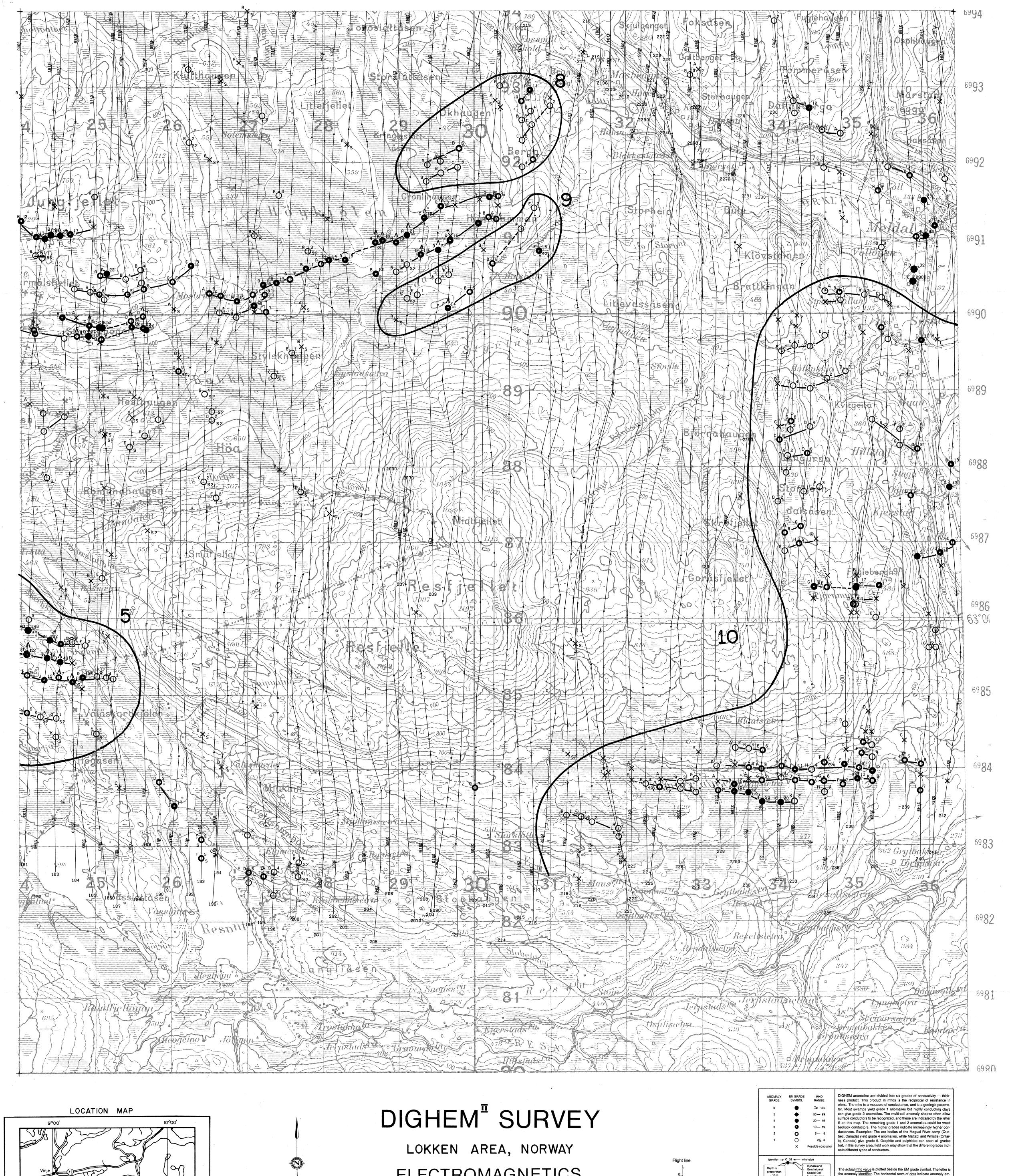
INDUSTRIER A.s. ORKLA

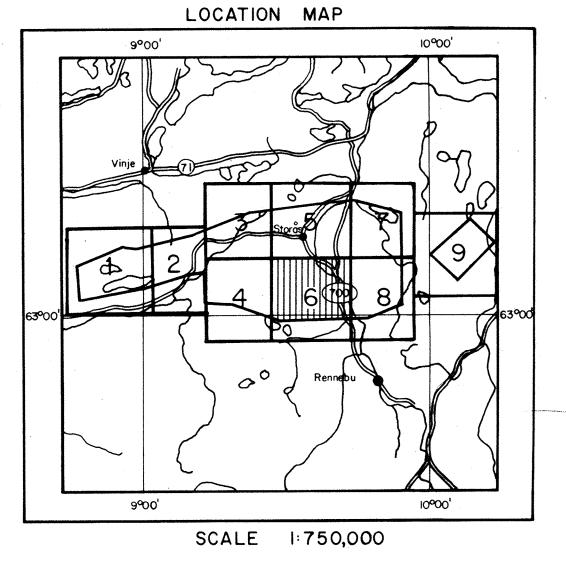


SHEET 5



CHECKED BY APRIL, 82



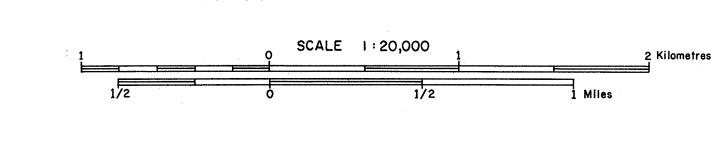


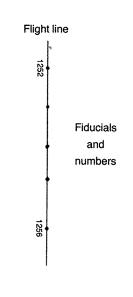


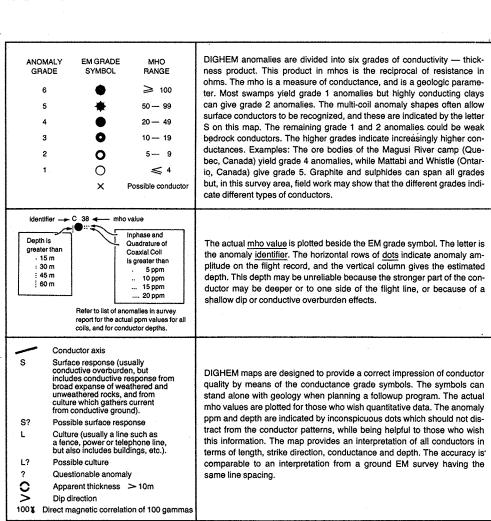
ELECTROMAGNETICS

FOR

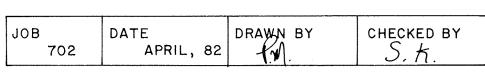
ORKLA INDUSTRIER A.s.

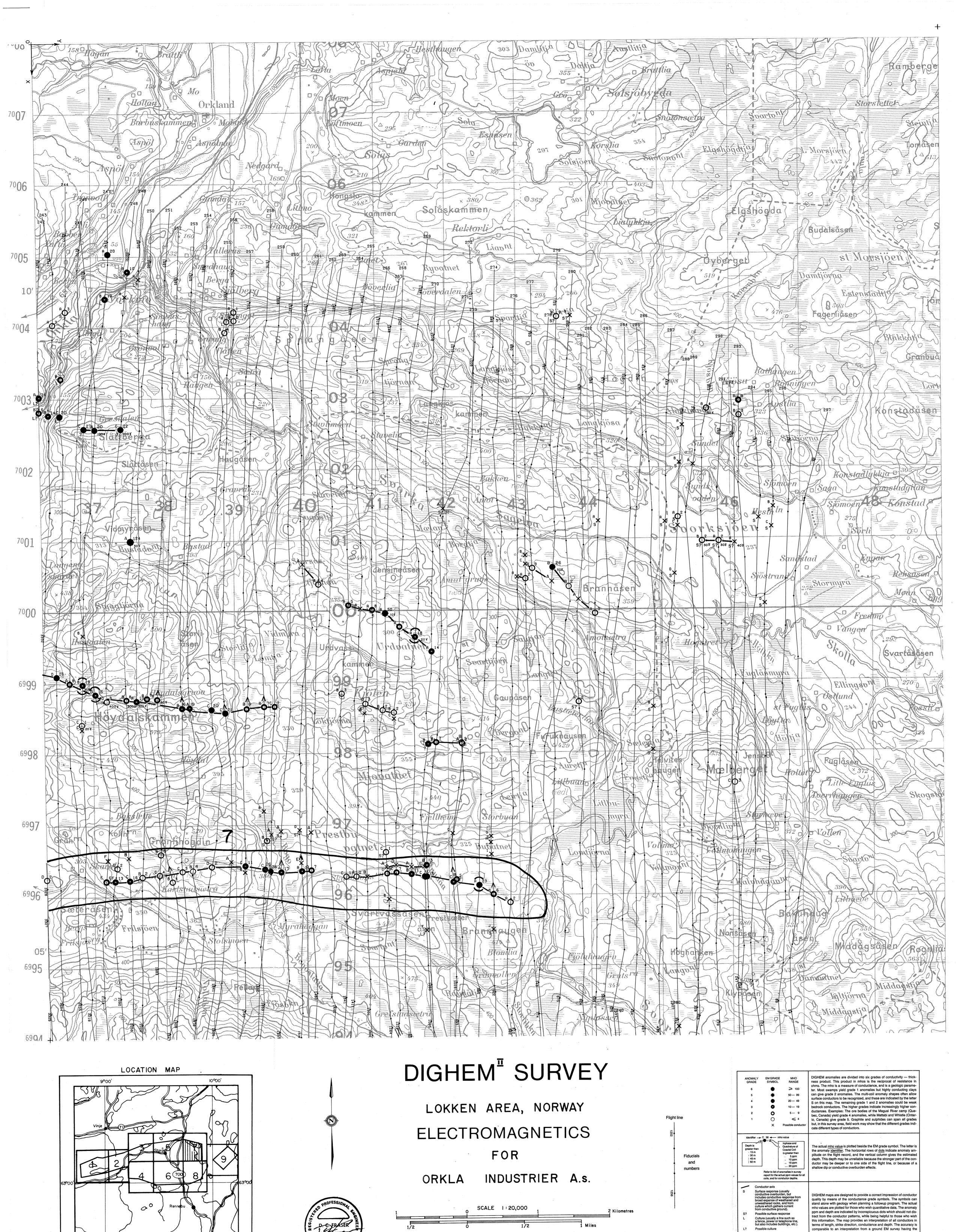






SHEET 6





SHEET 7

10000

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Questionable anomaly

> Dip direction

100 Direct magnetic correlation of 100 ga

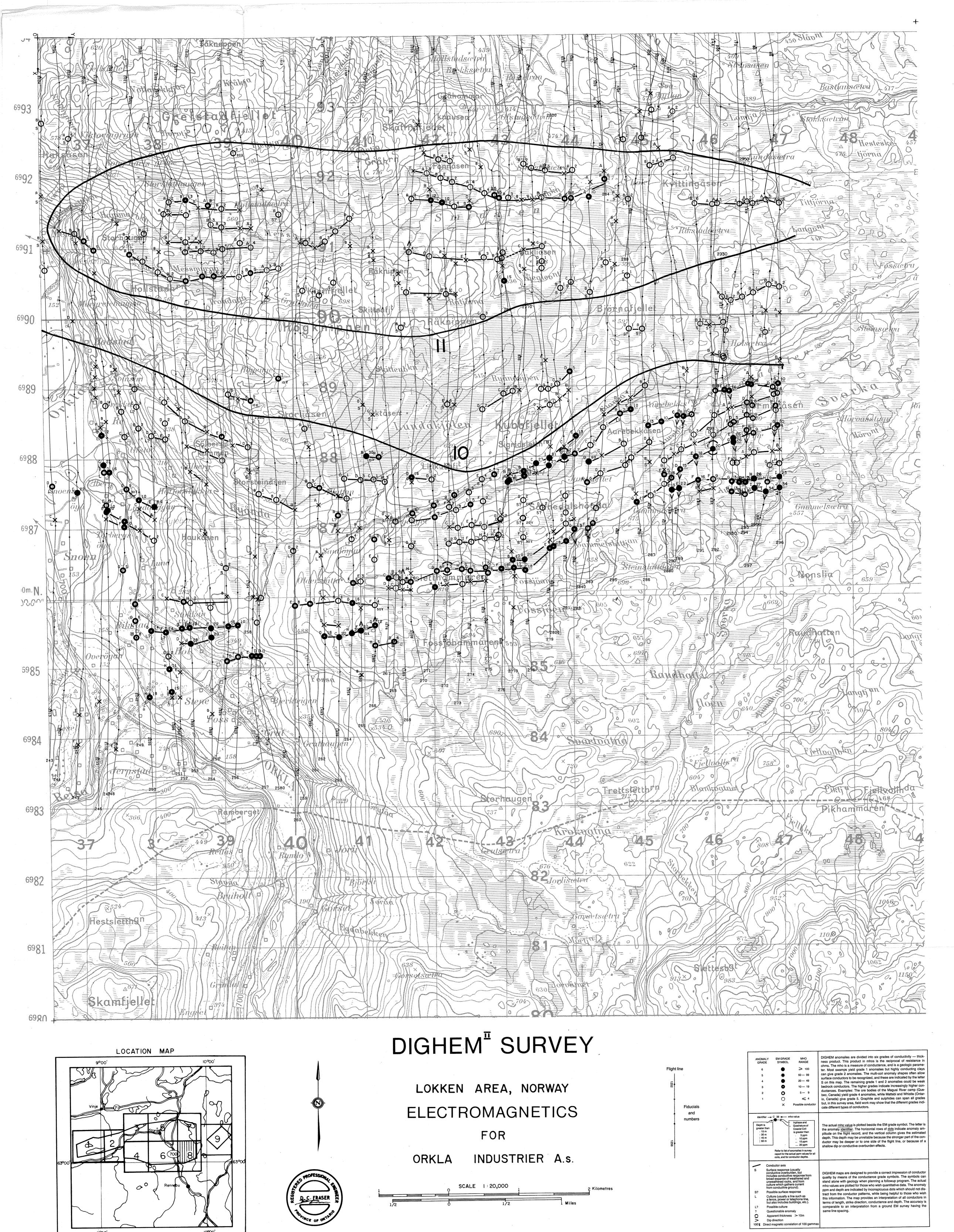
Apparent thickness > 10m

same line spacing.

APRIL, 82

DRAWN BY

S.K.



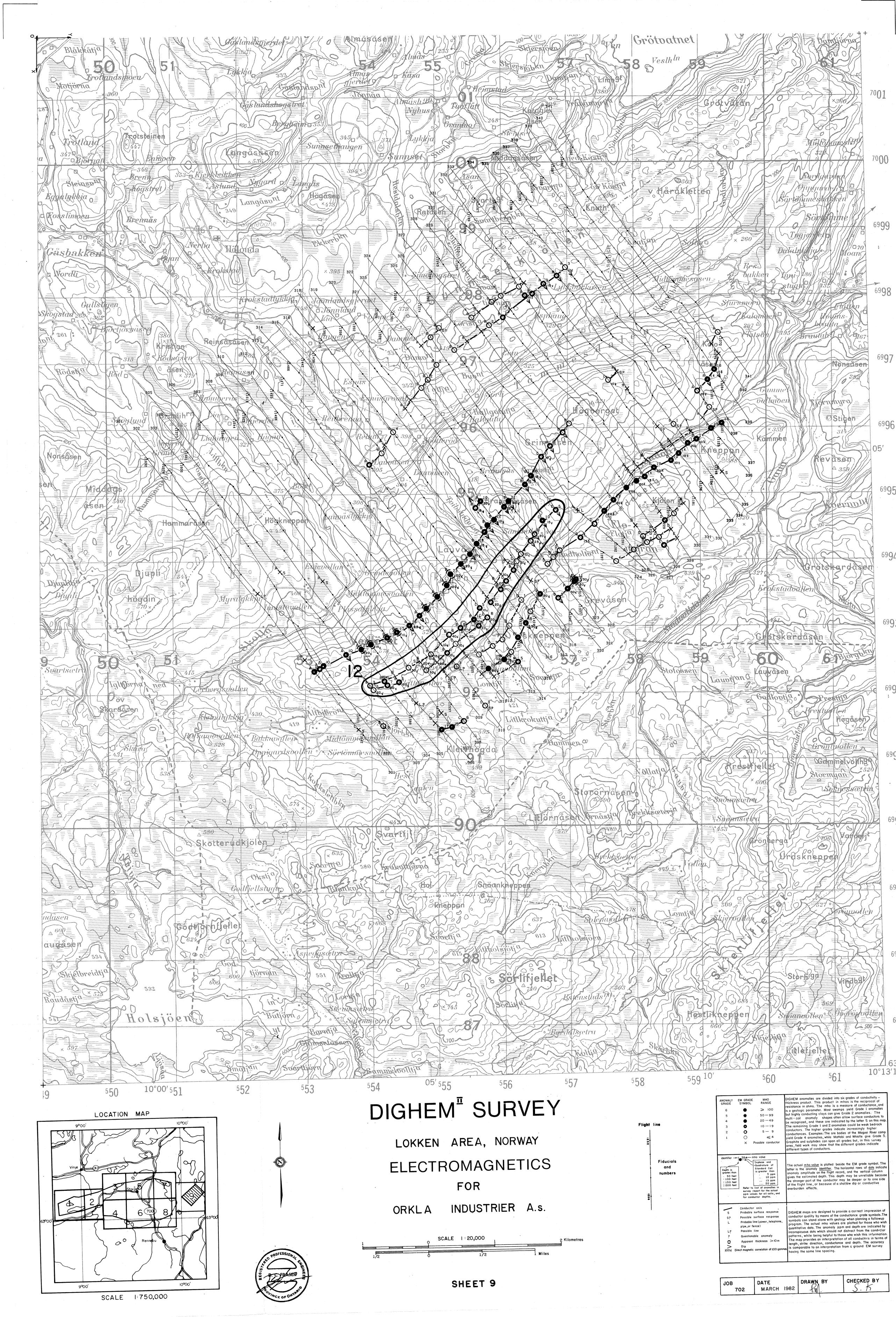
SHEET 8

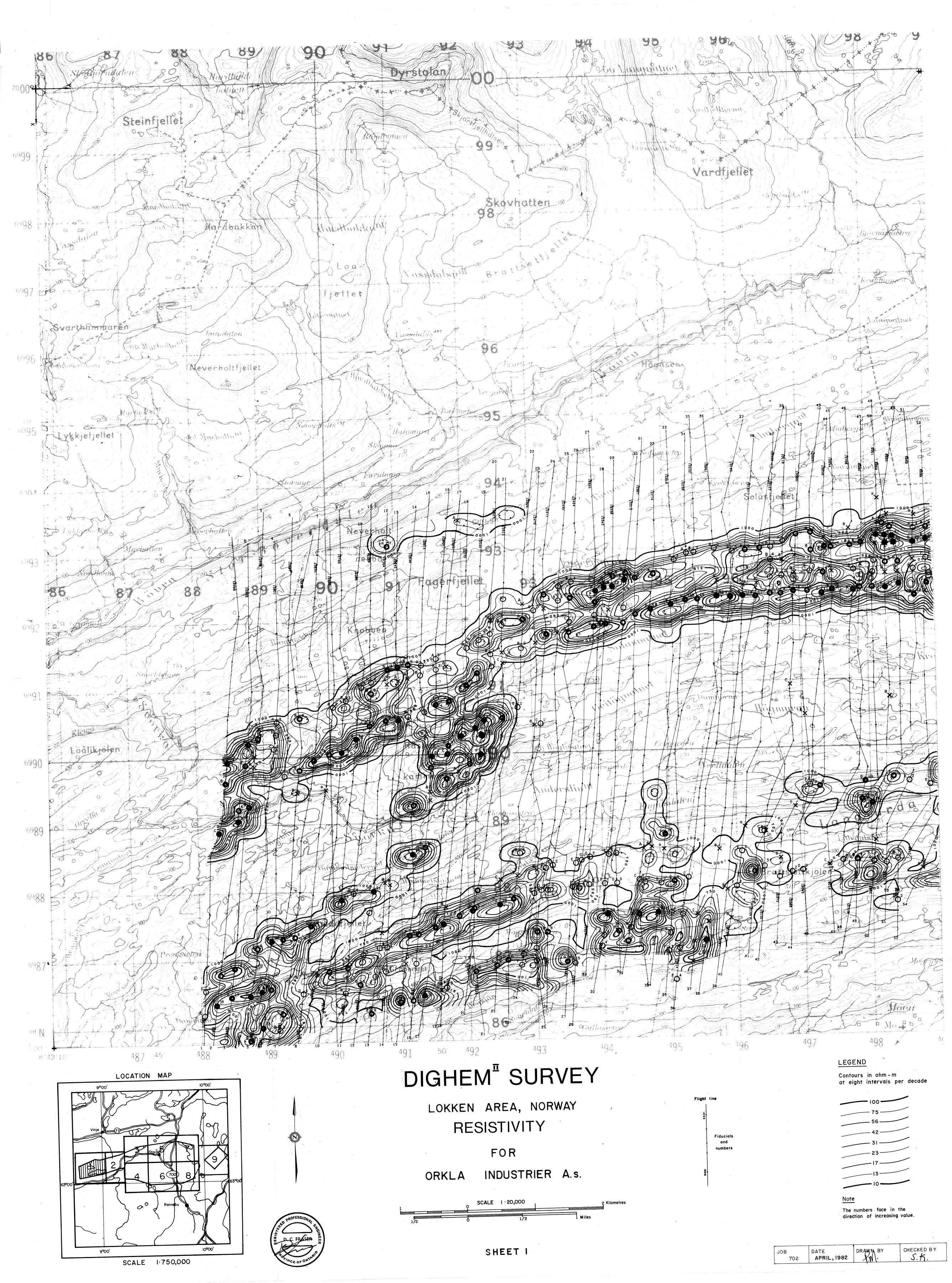
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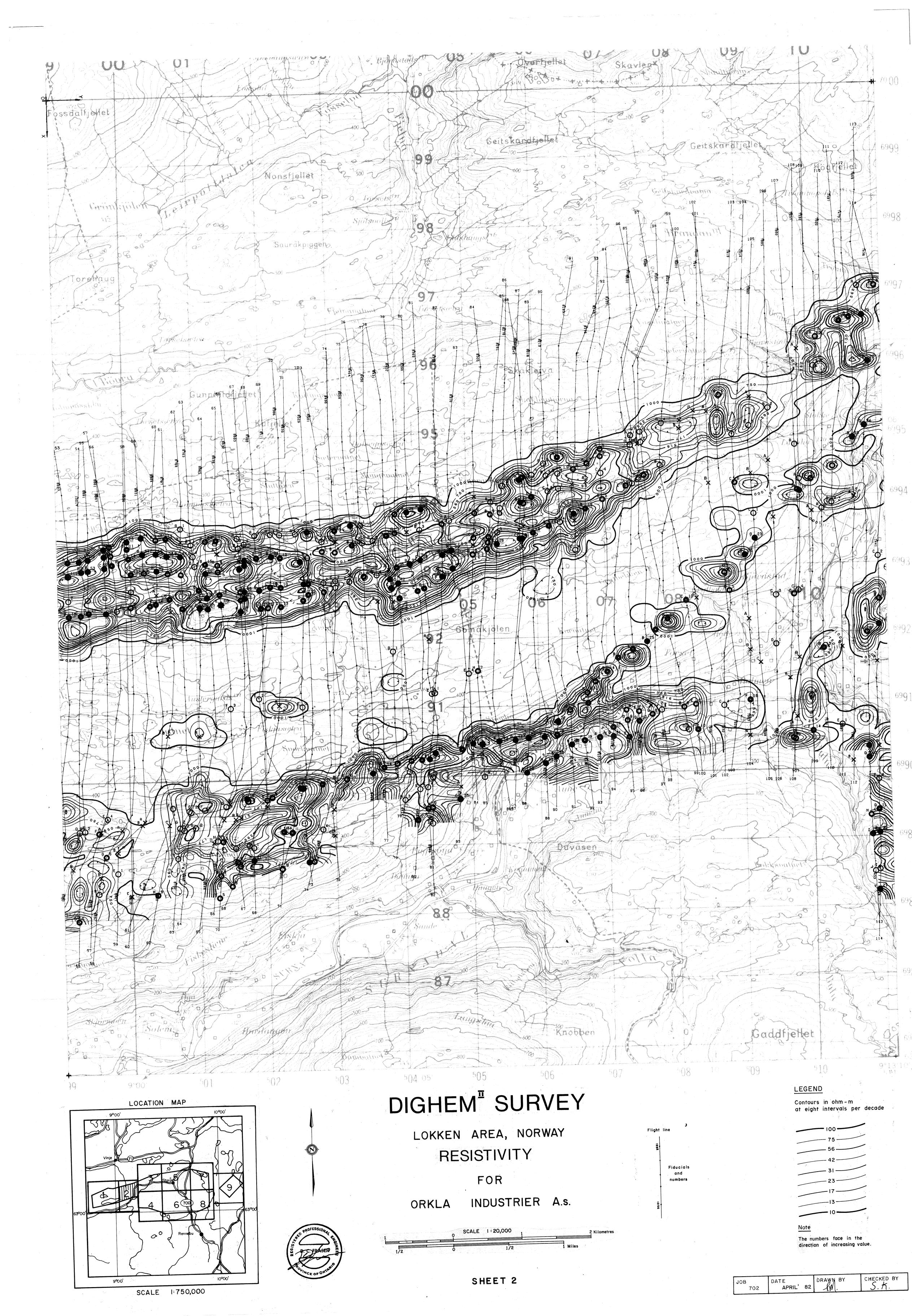
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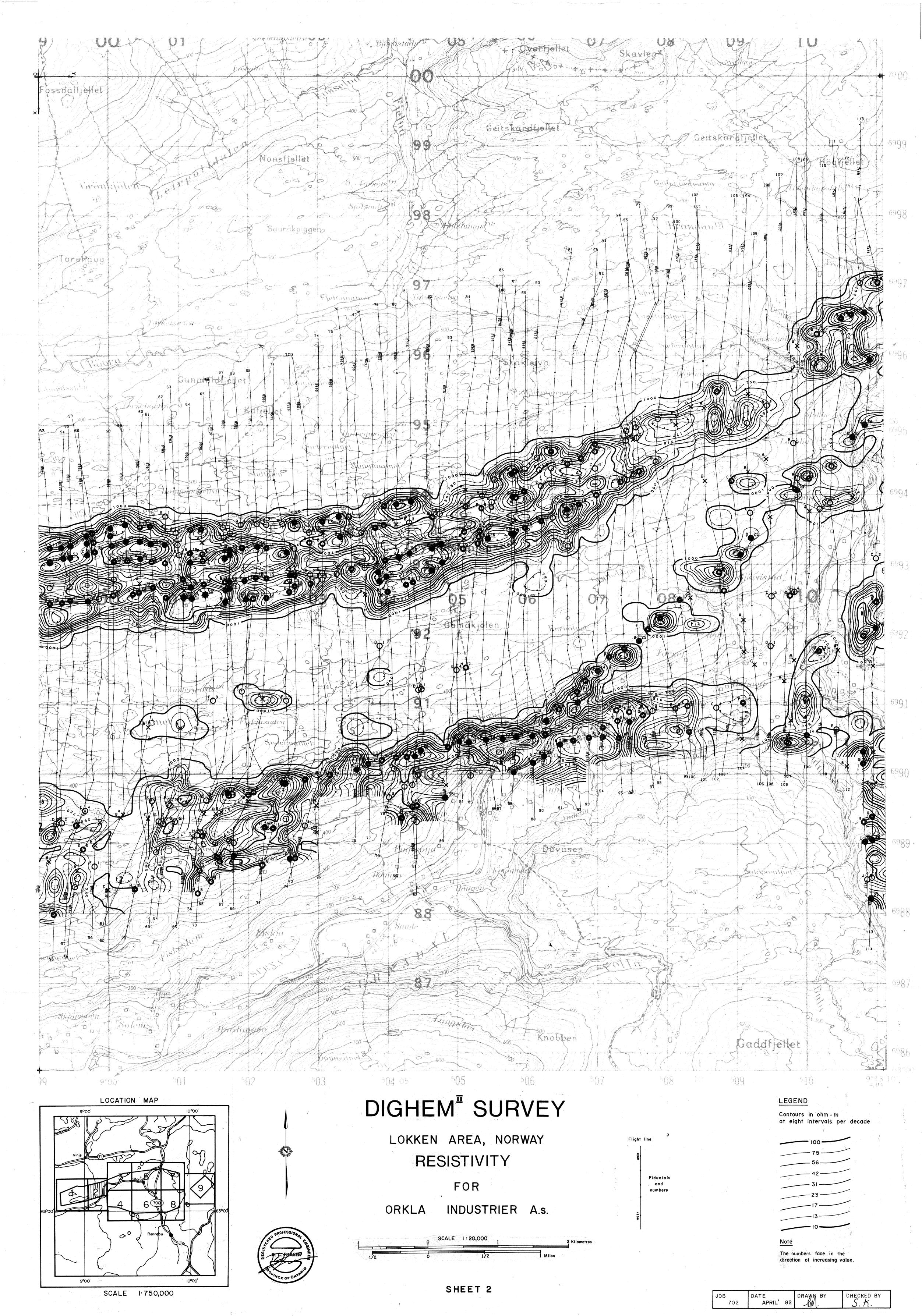
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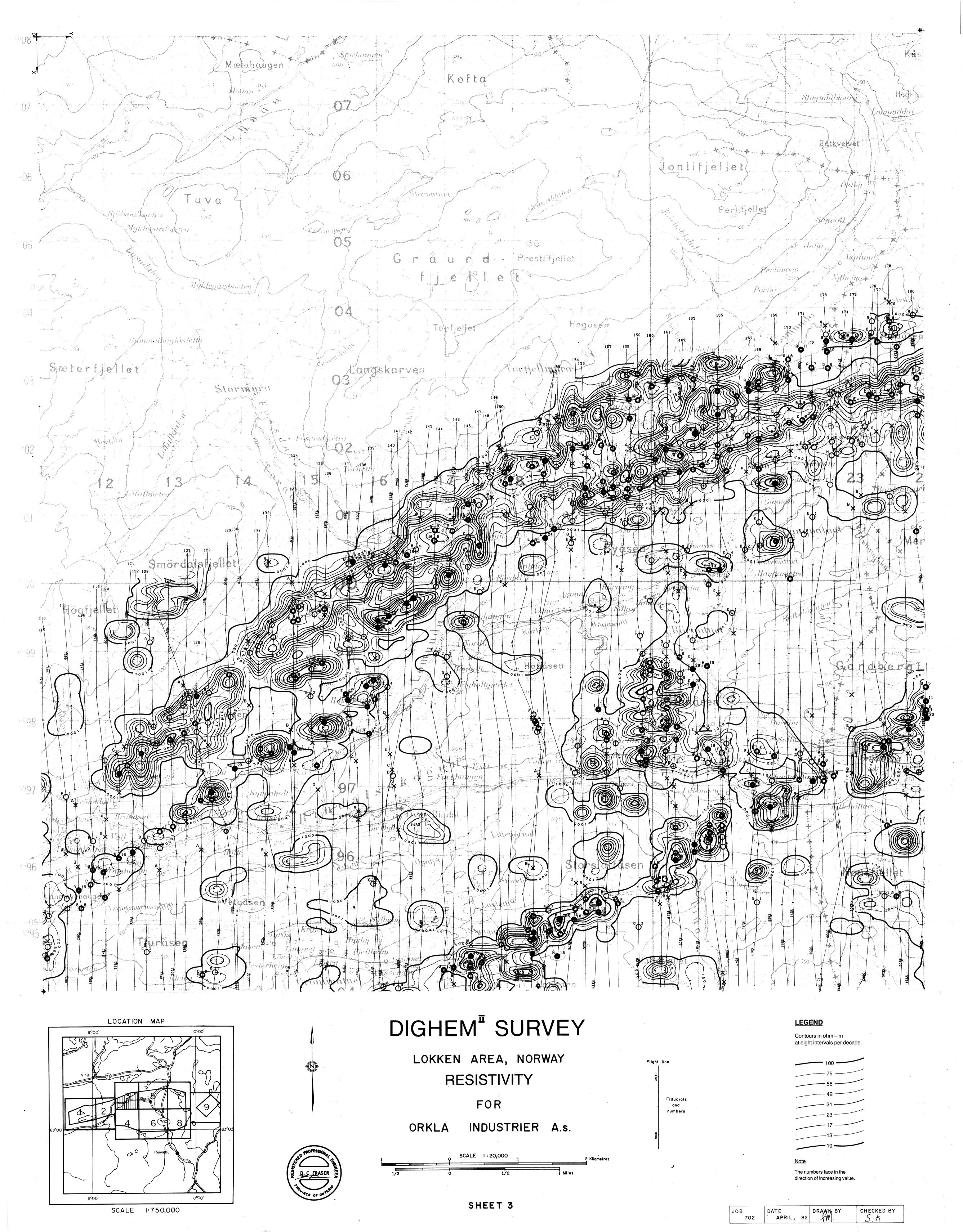
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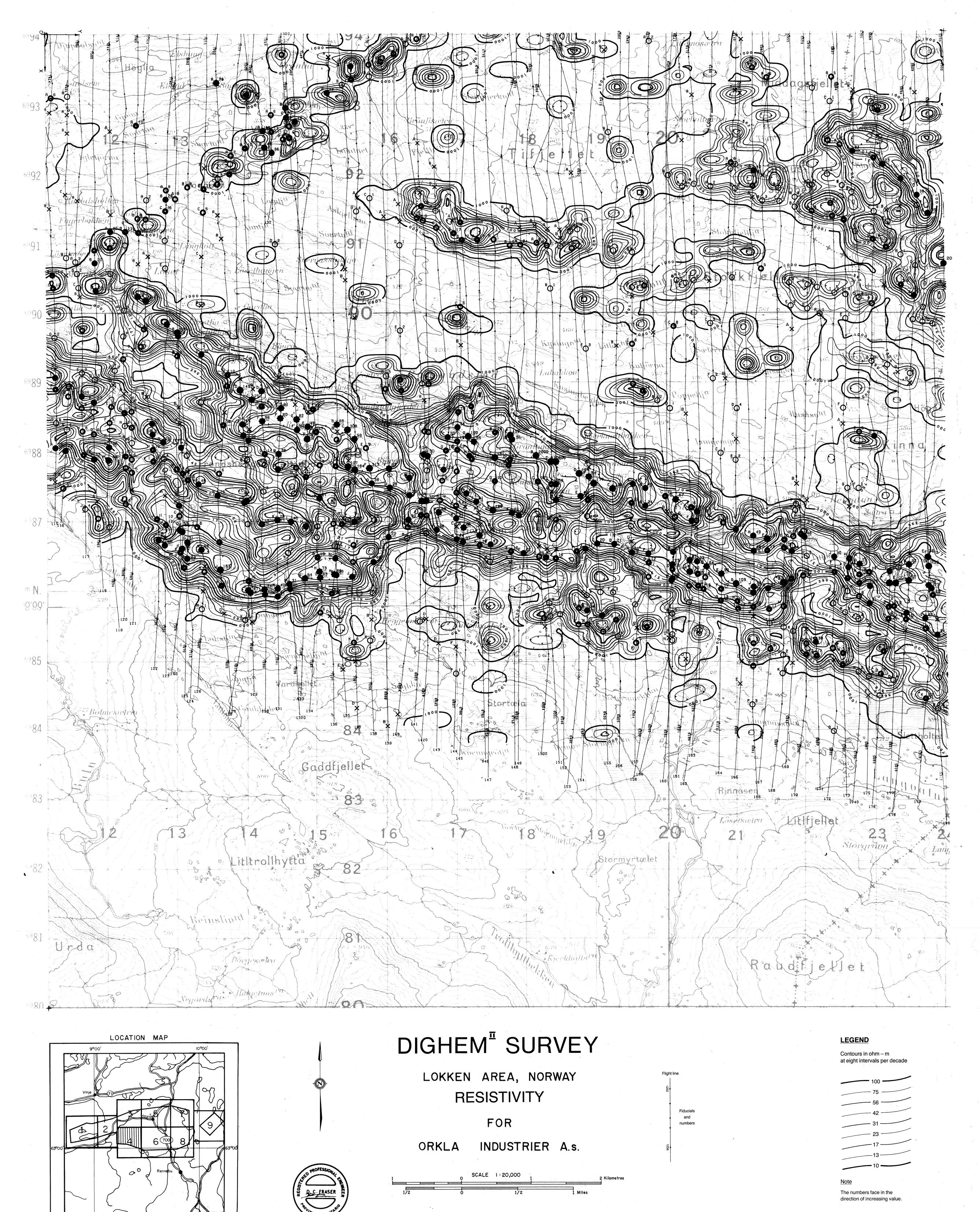








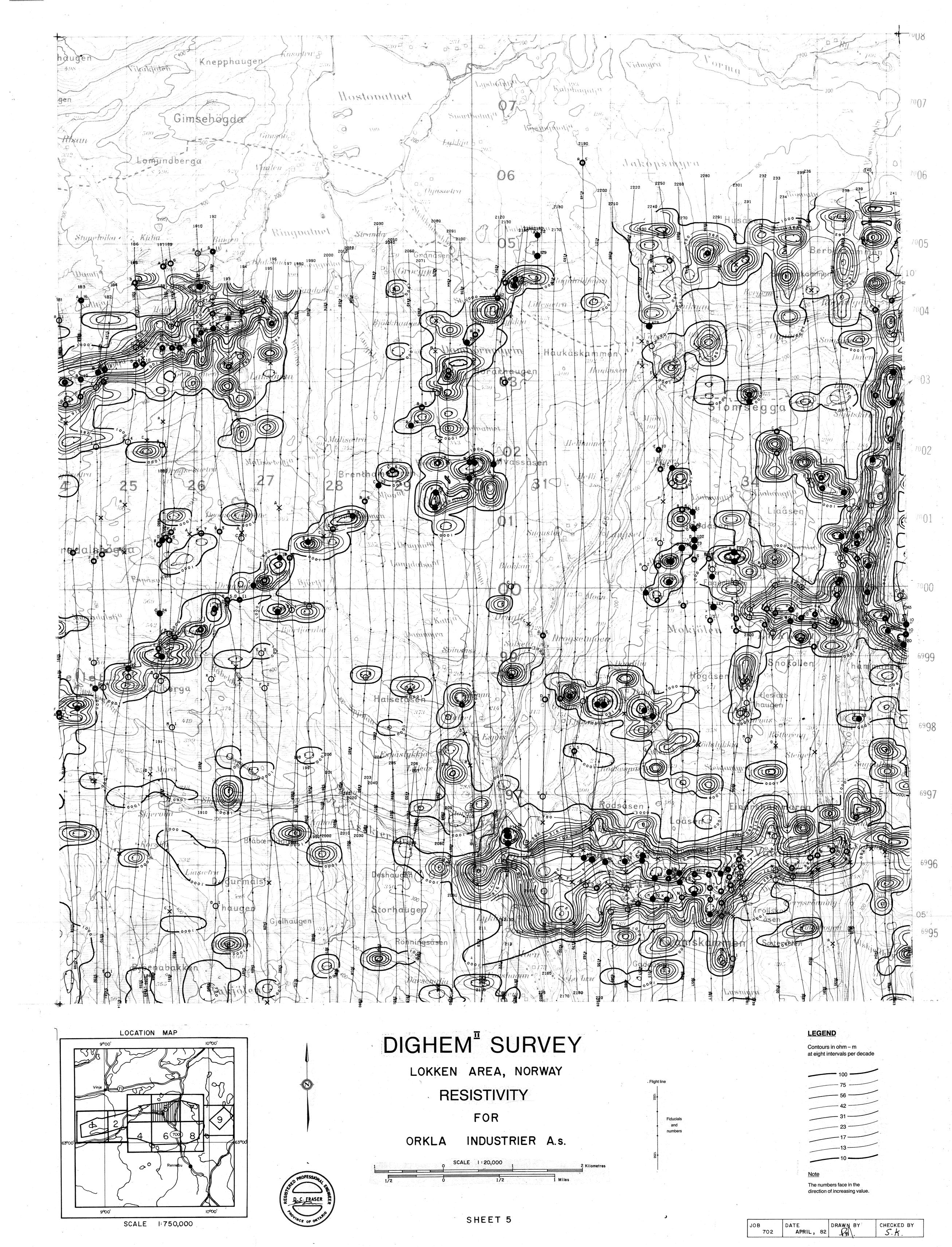


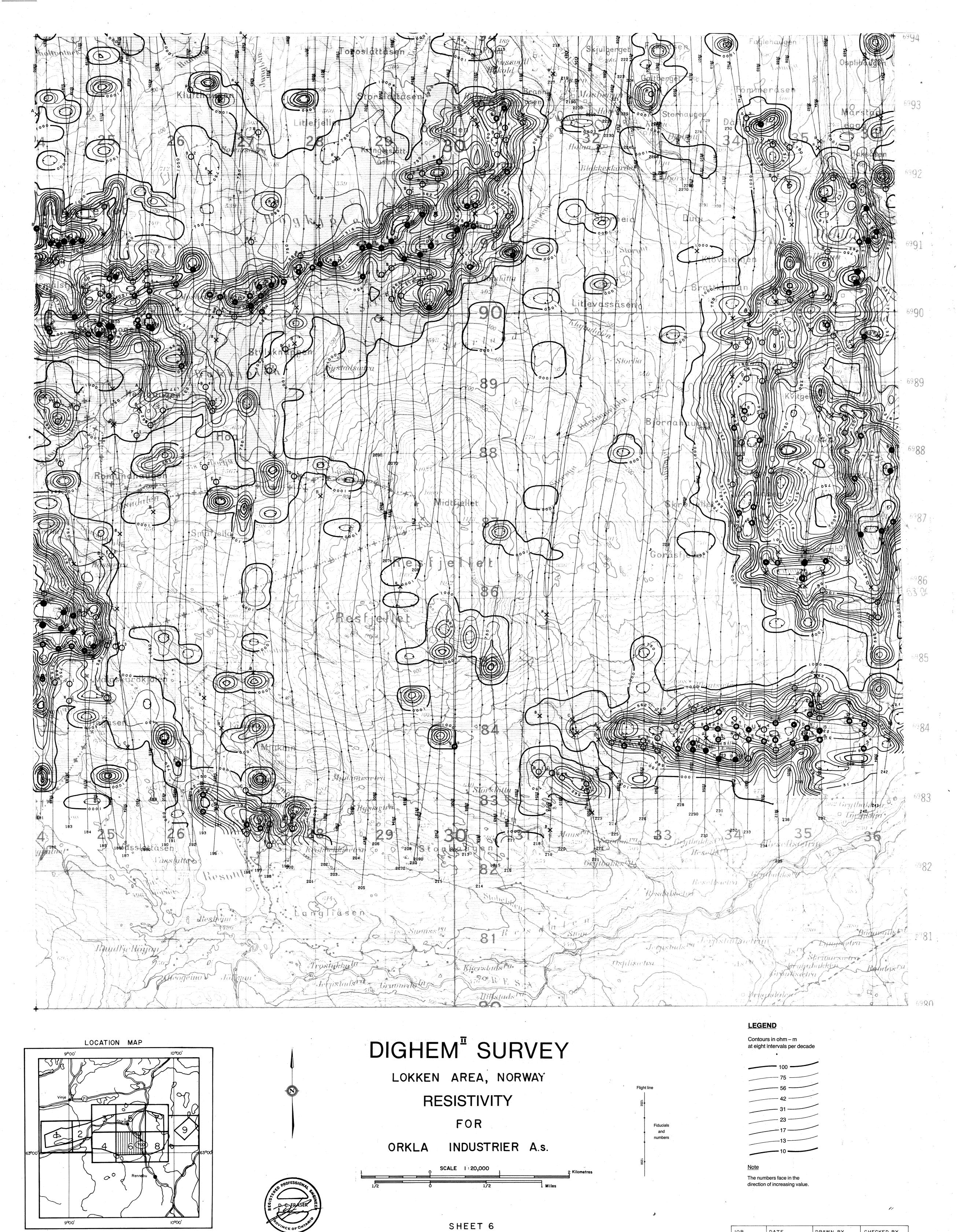


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SHEET 4

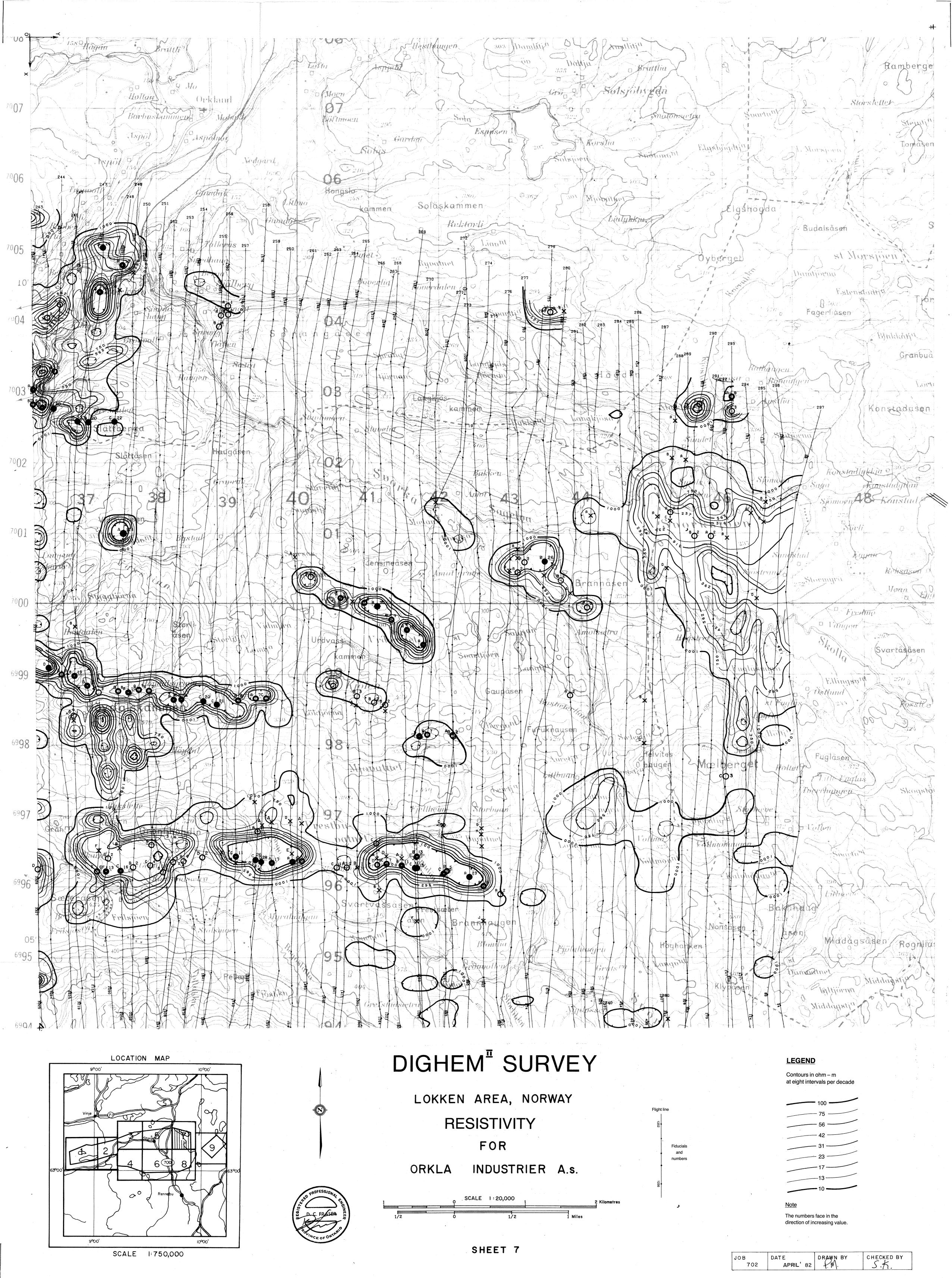
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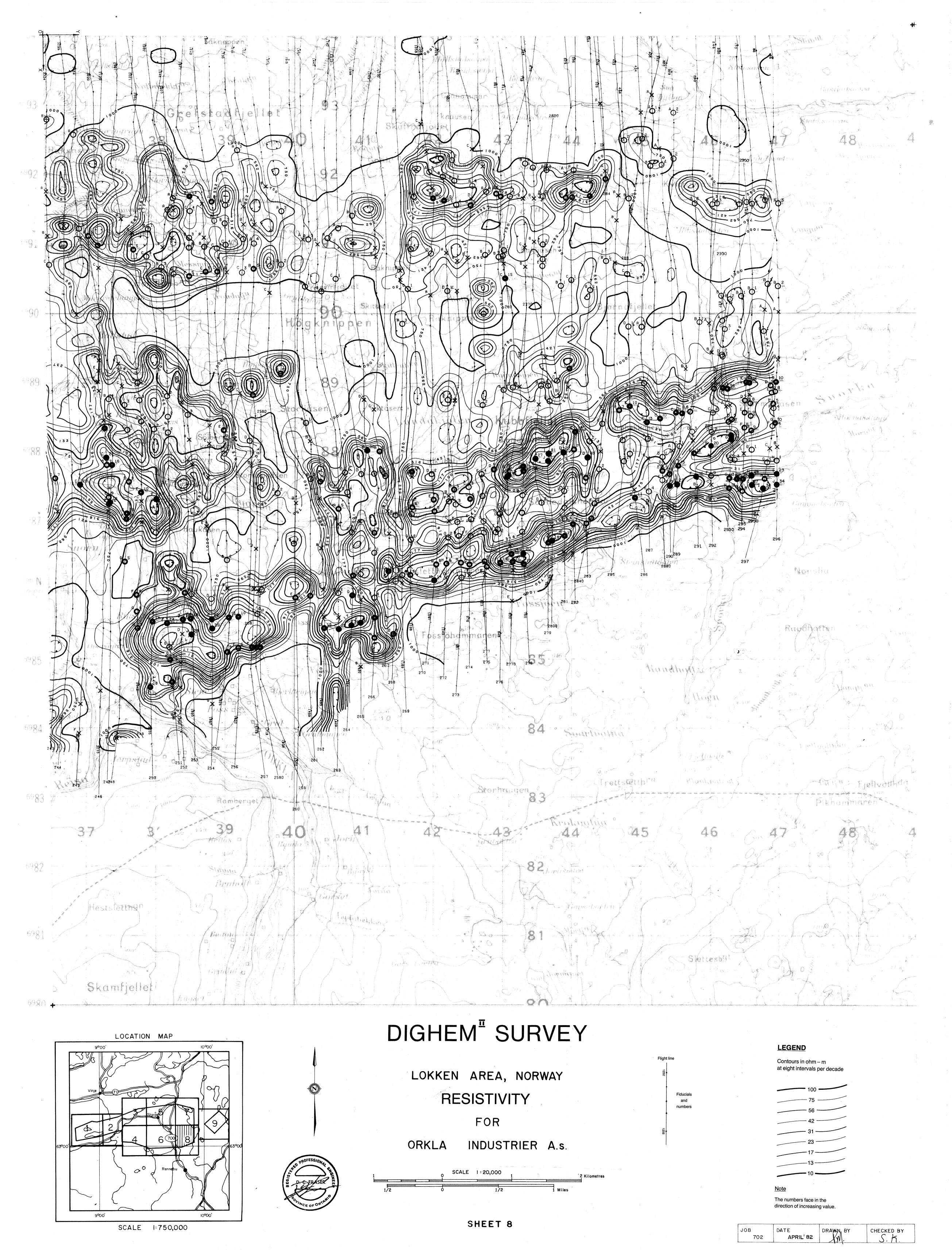


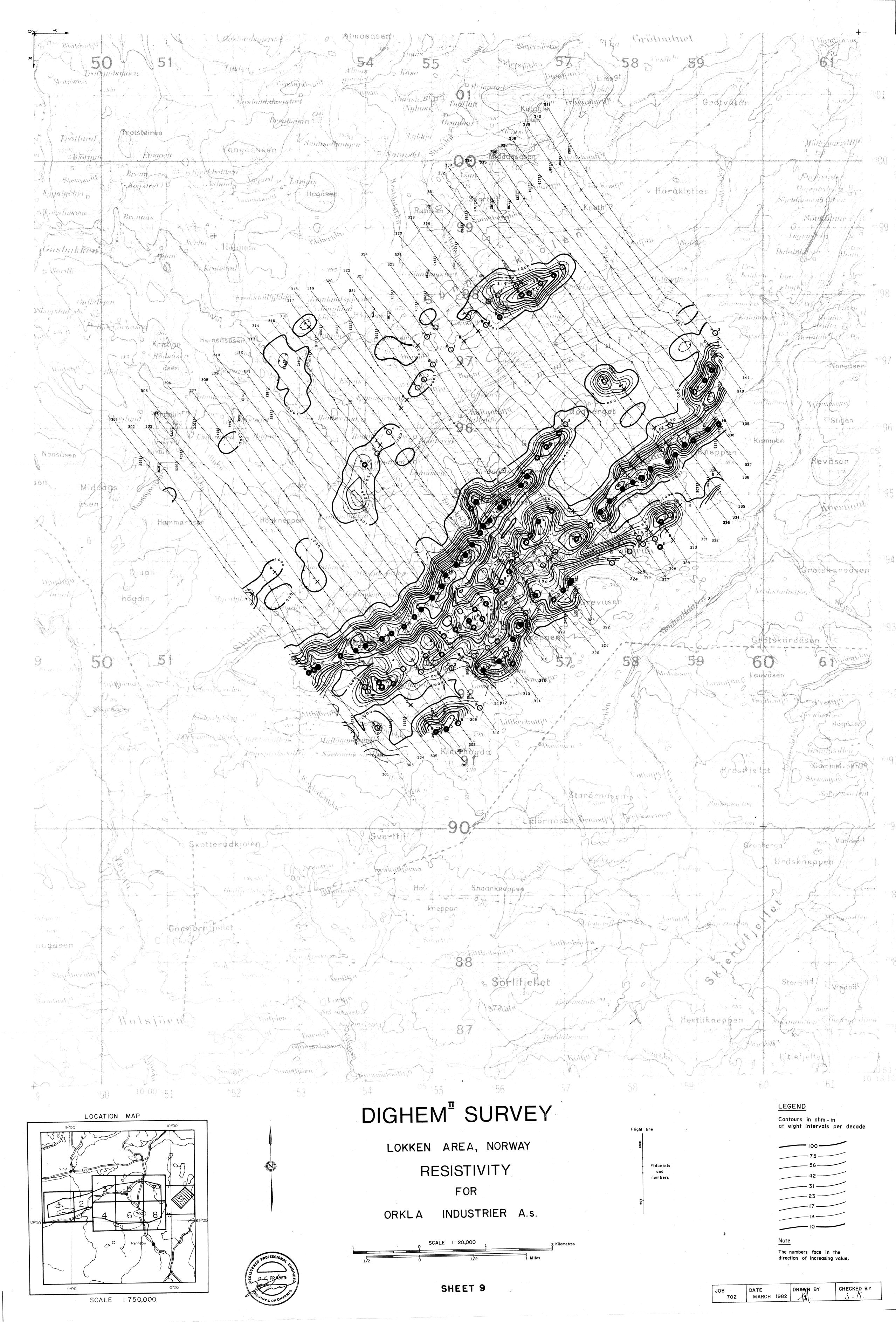


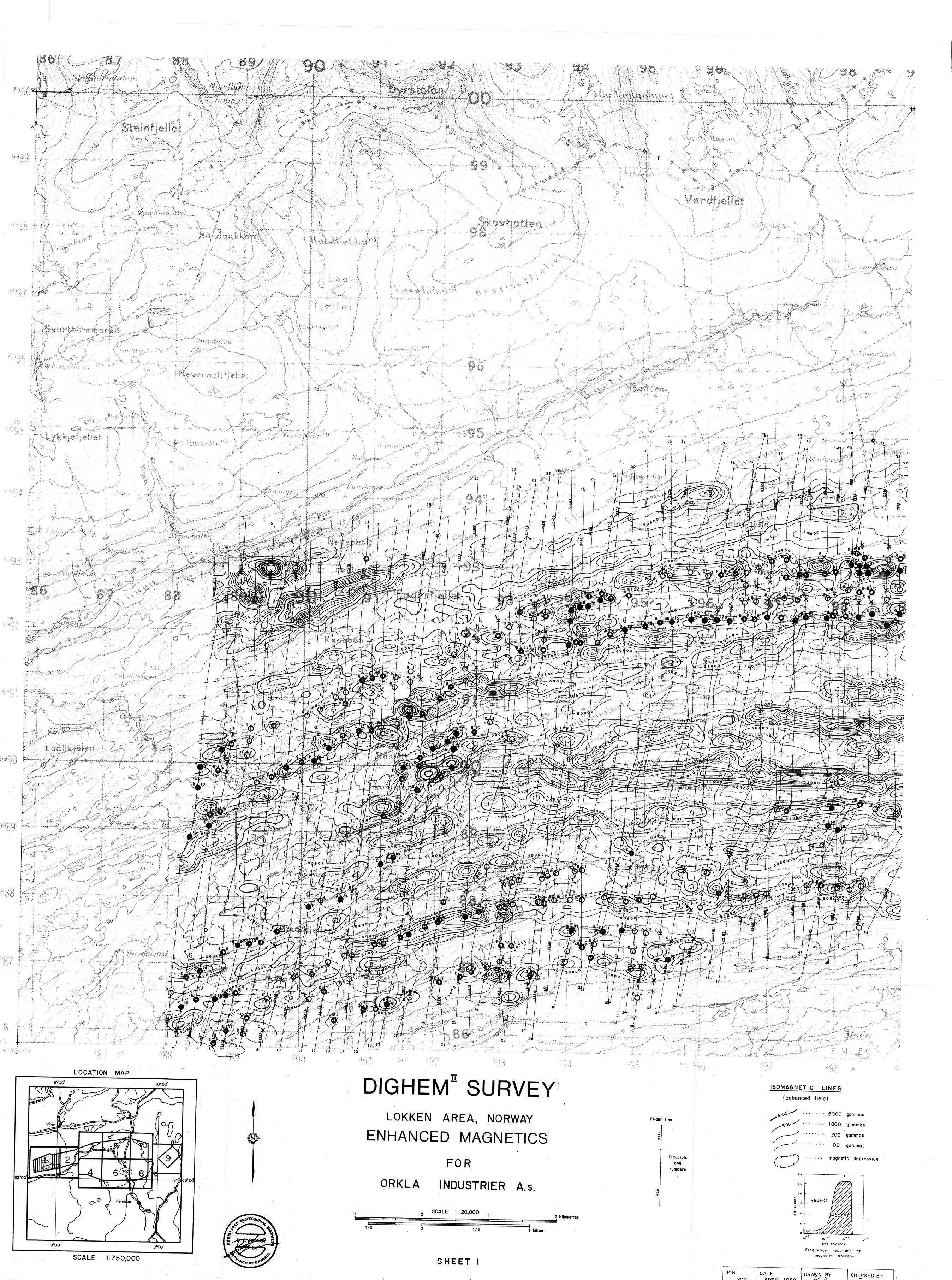
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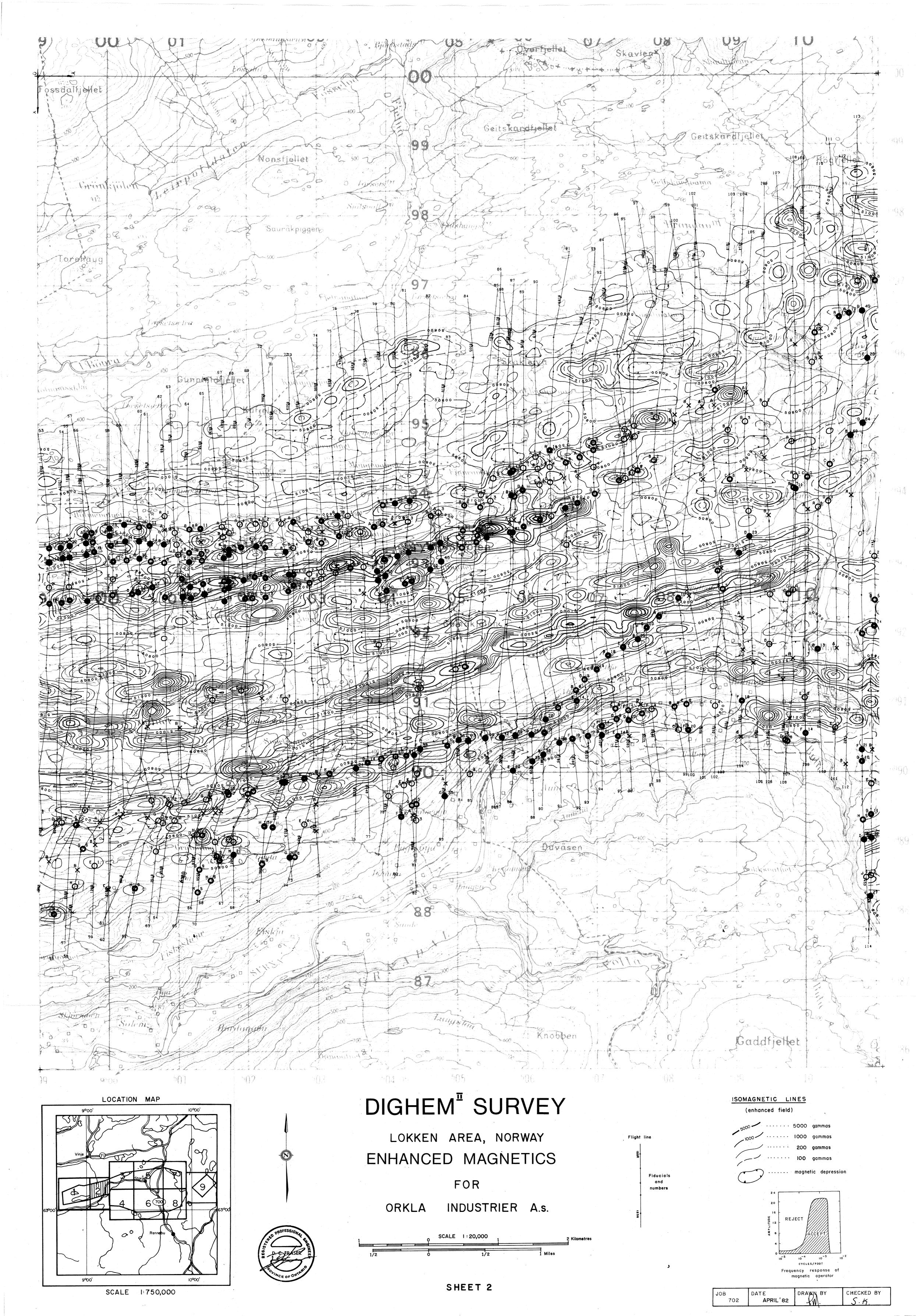
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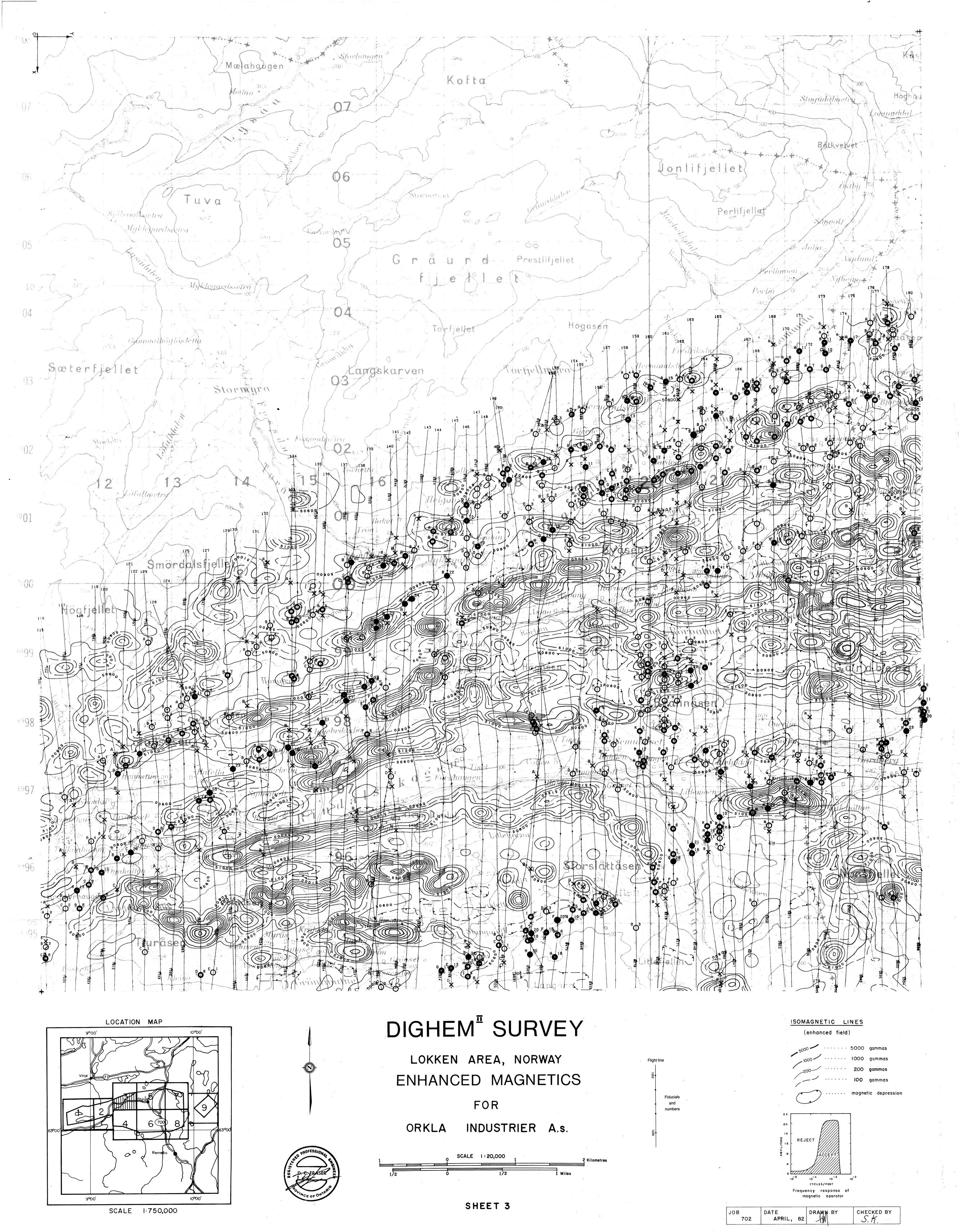


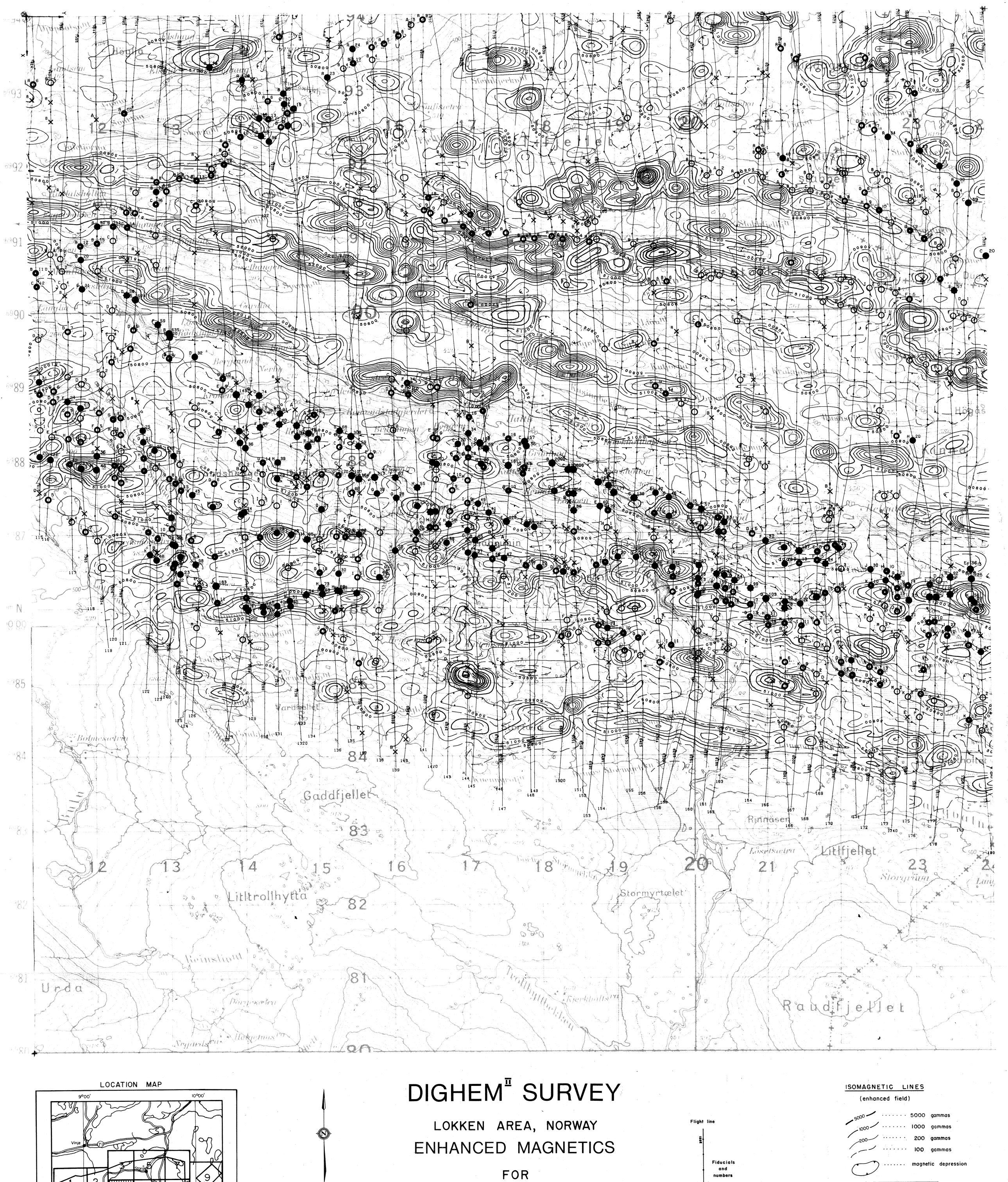


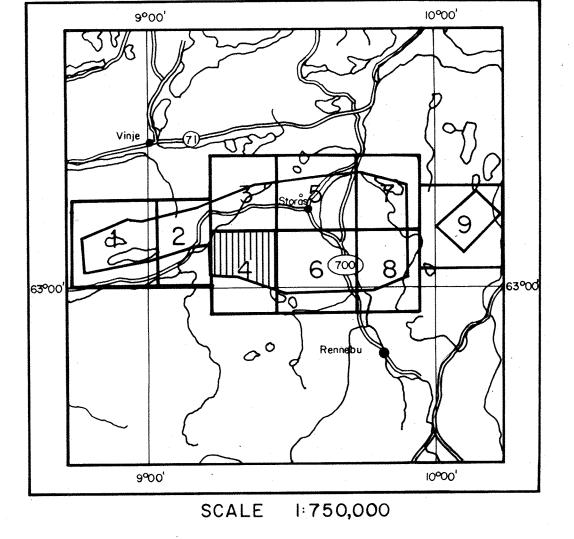






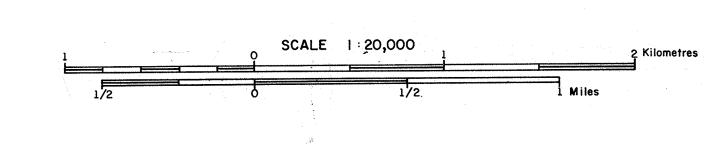




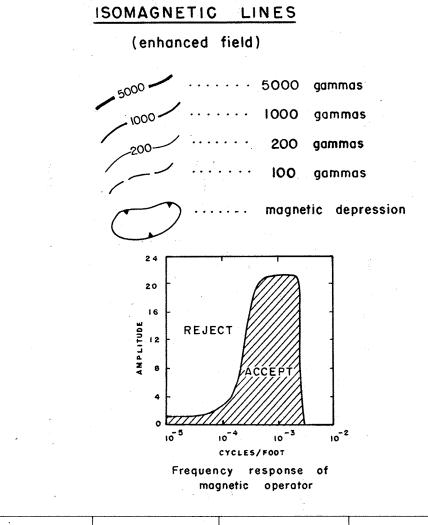


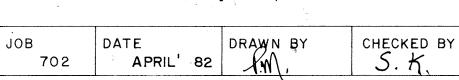


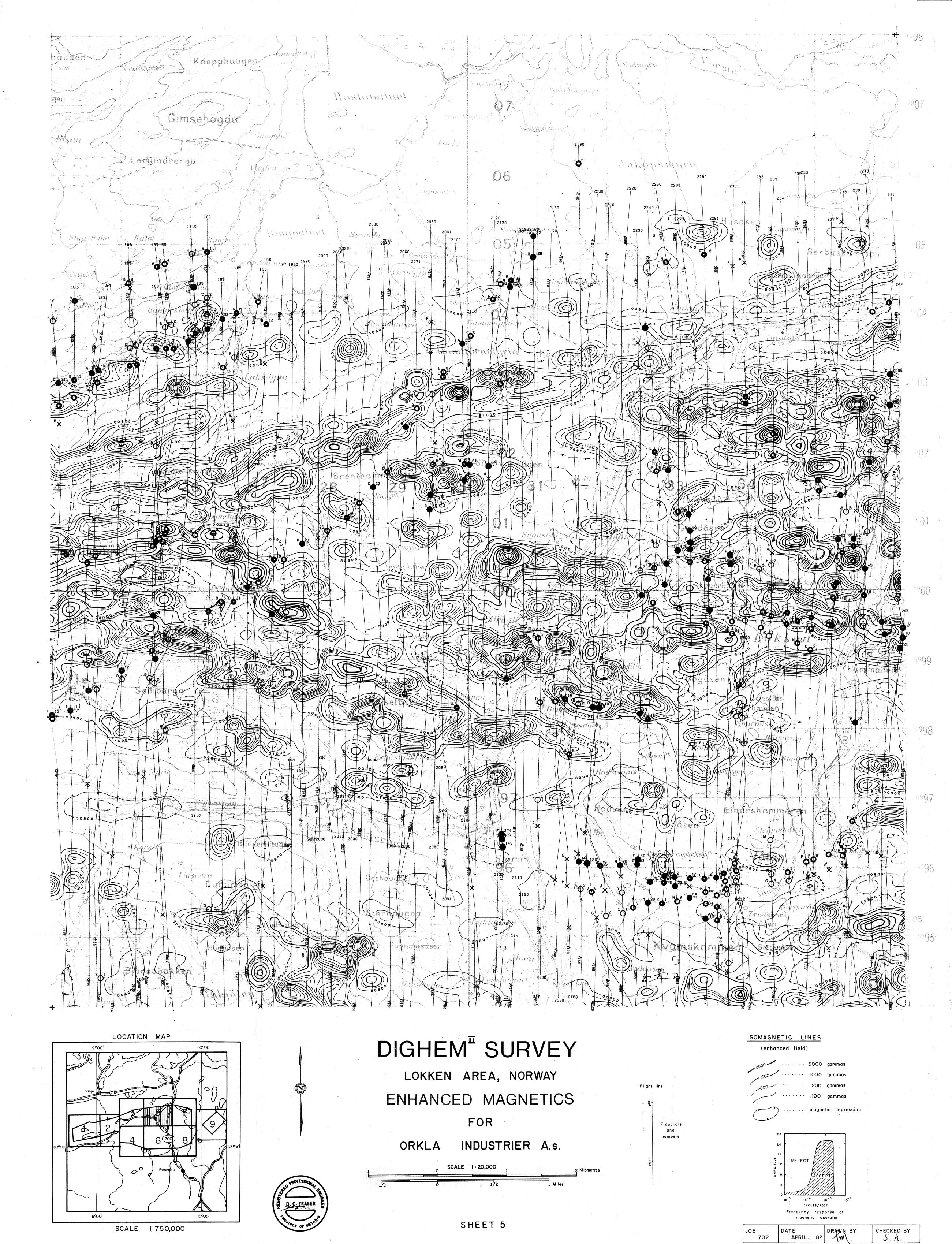
INDUSTRIER A.s. ORKLA

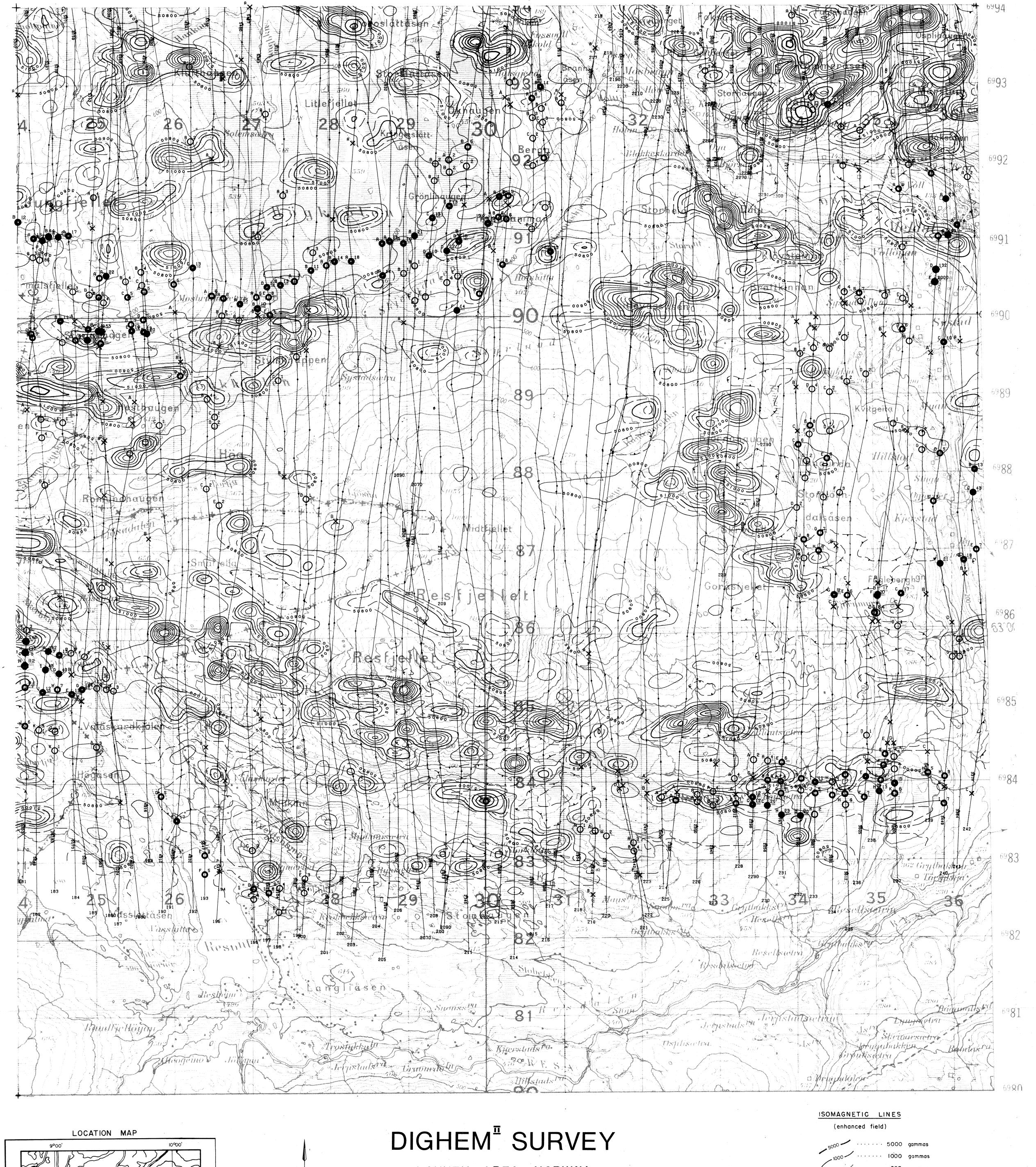


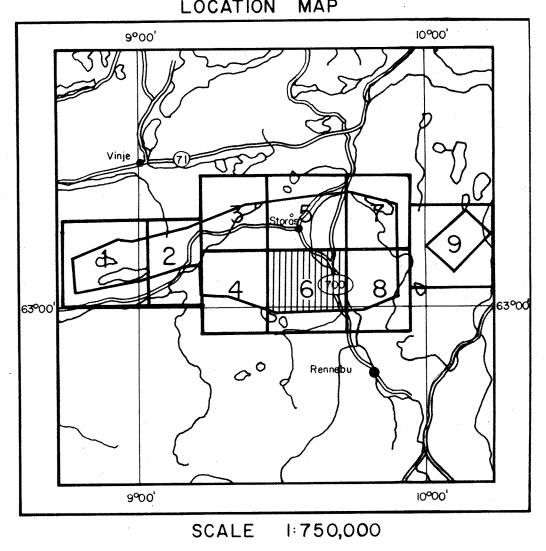








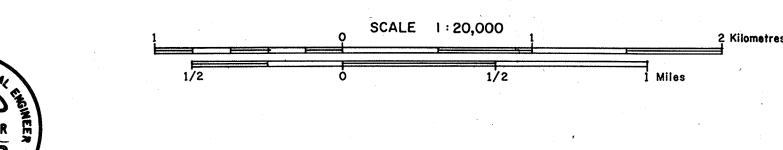


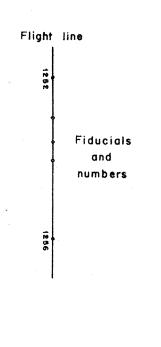


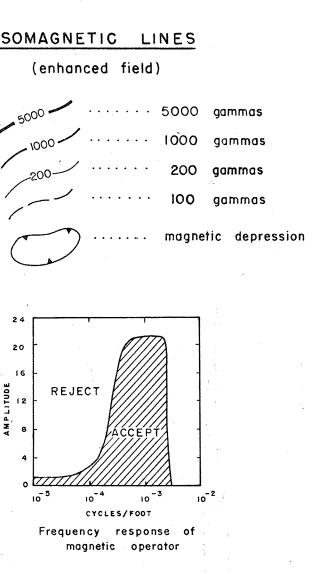


LOKKEN AREA, NORWAY
ENHANCED MAGNETICS
FOR

ORKLA INDUSTRIER A.s.

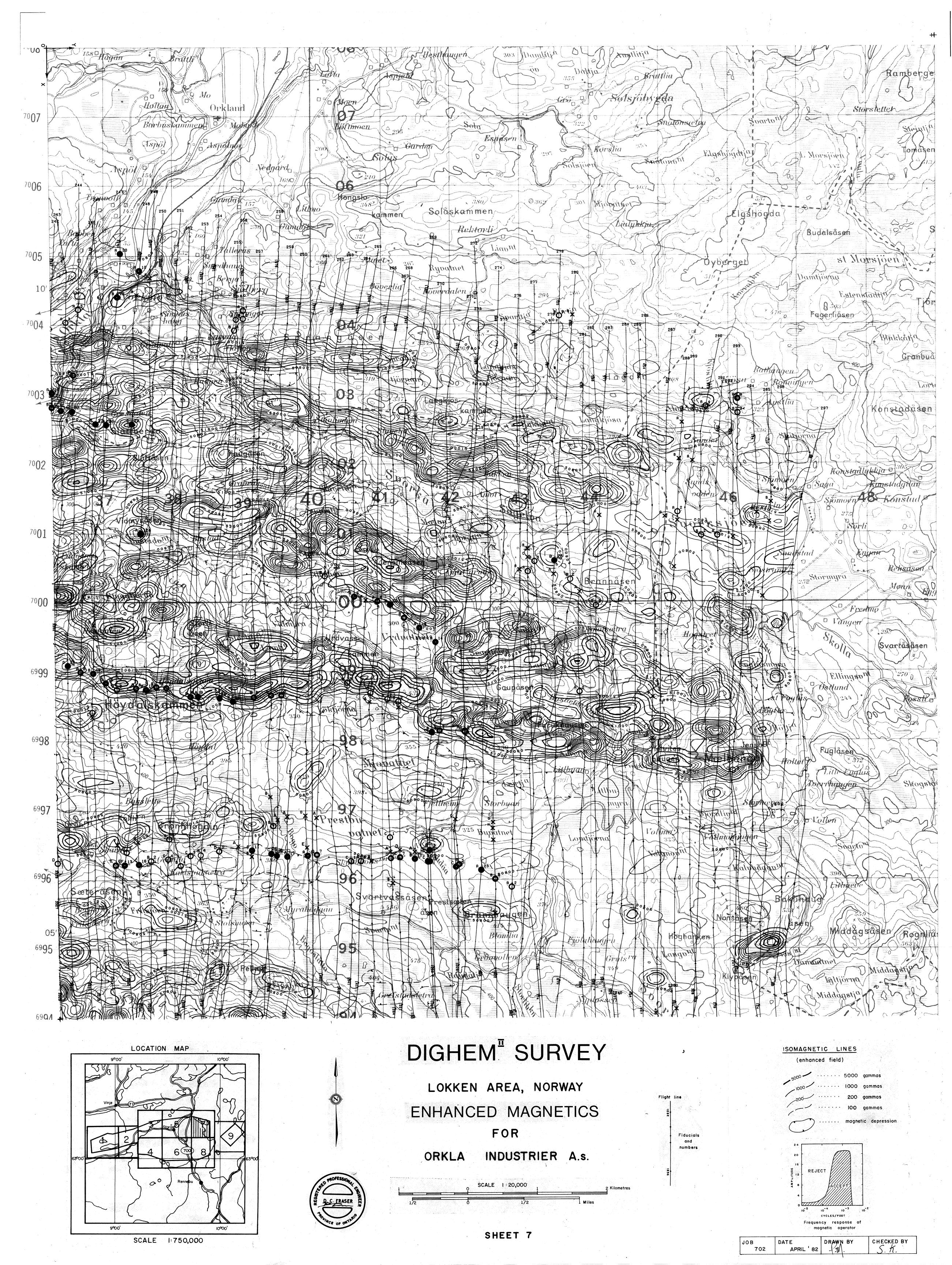


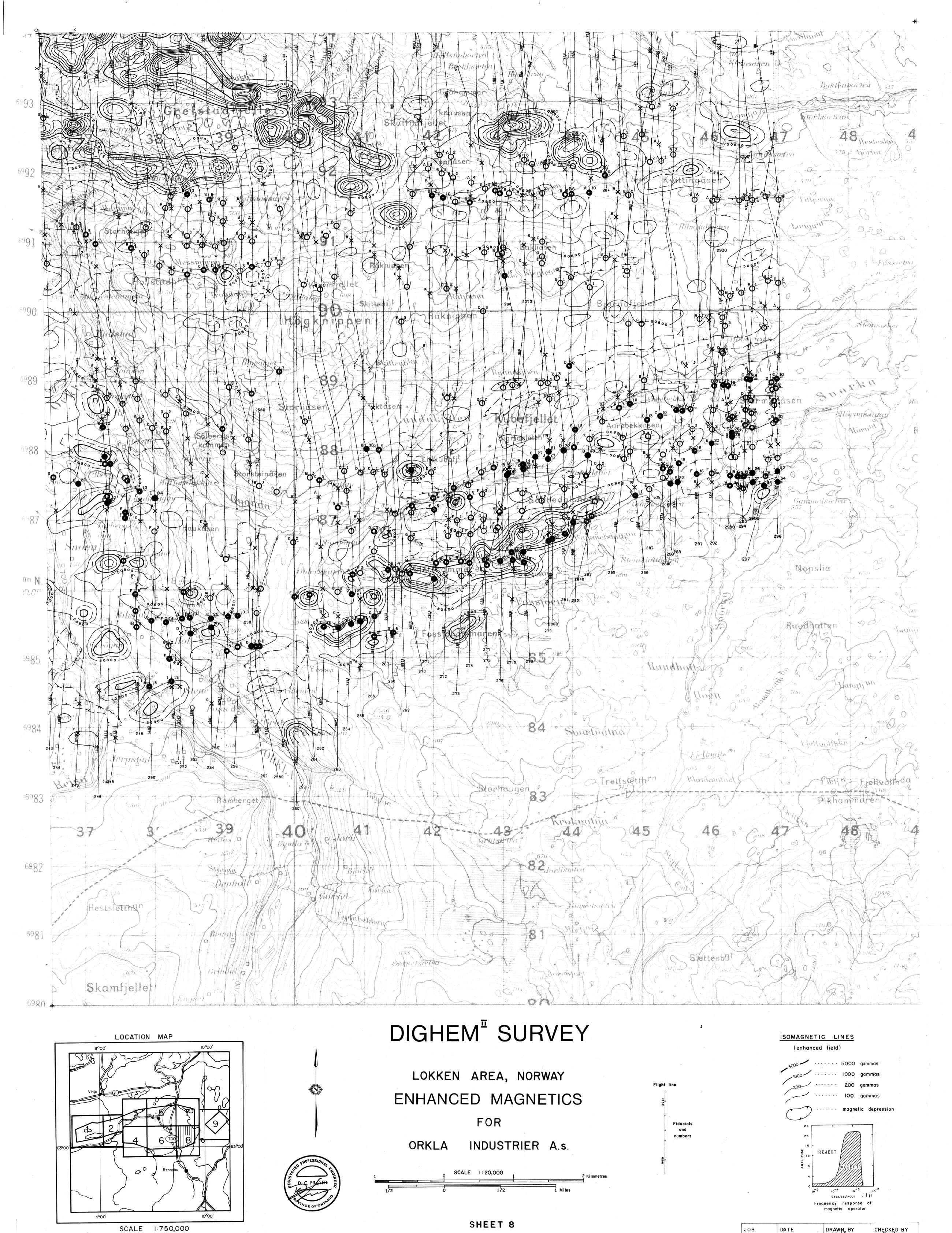




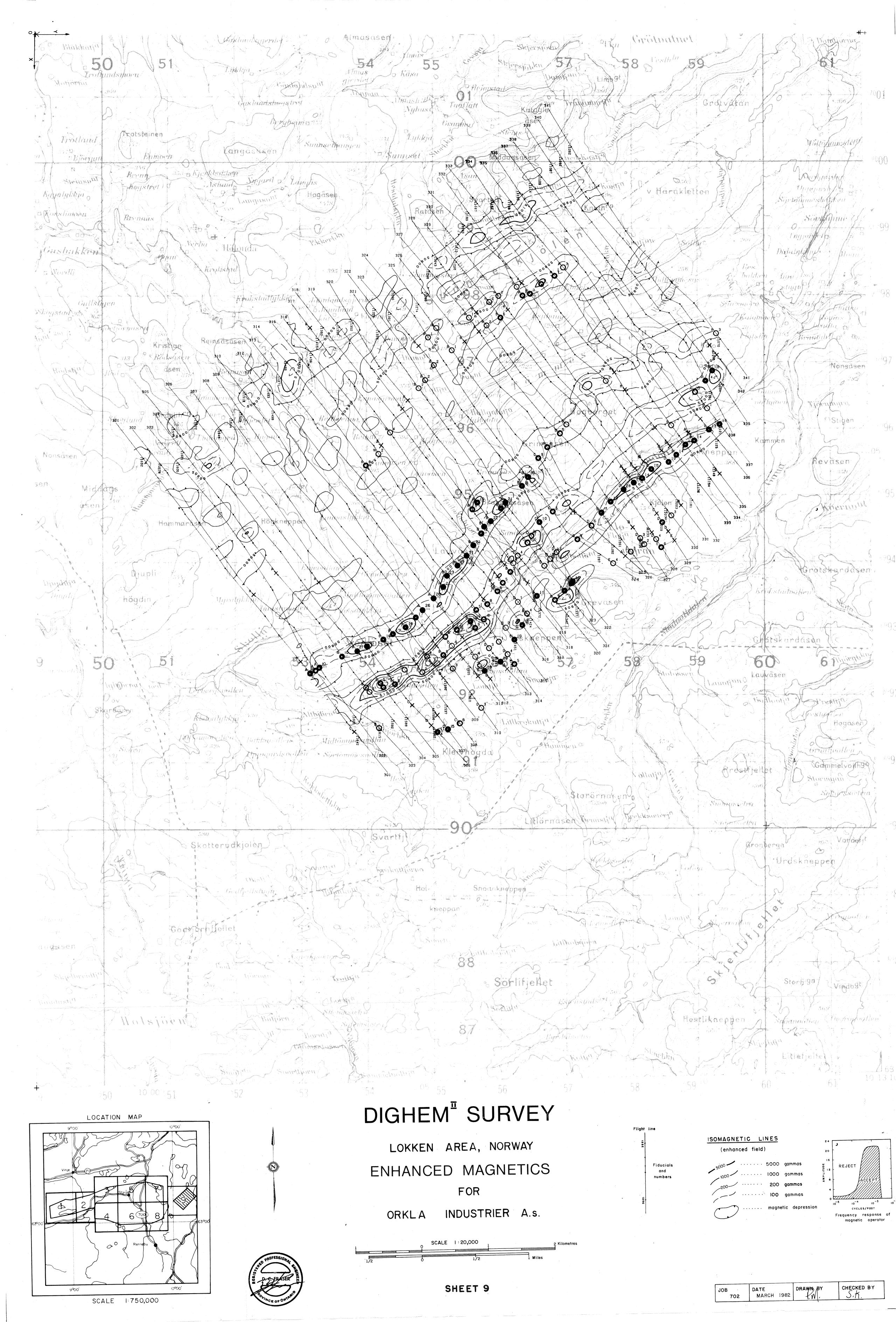
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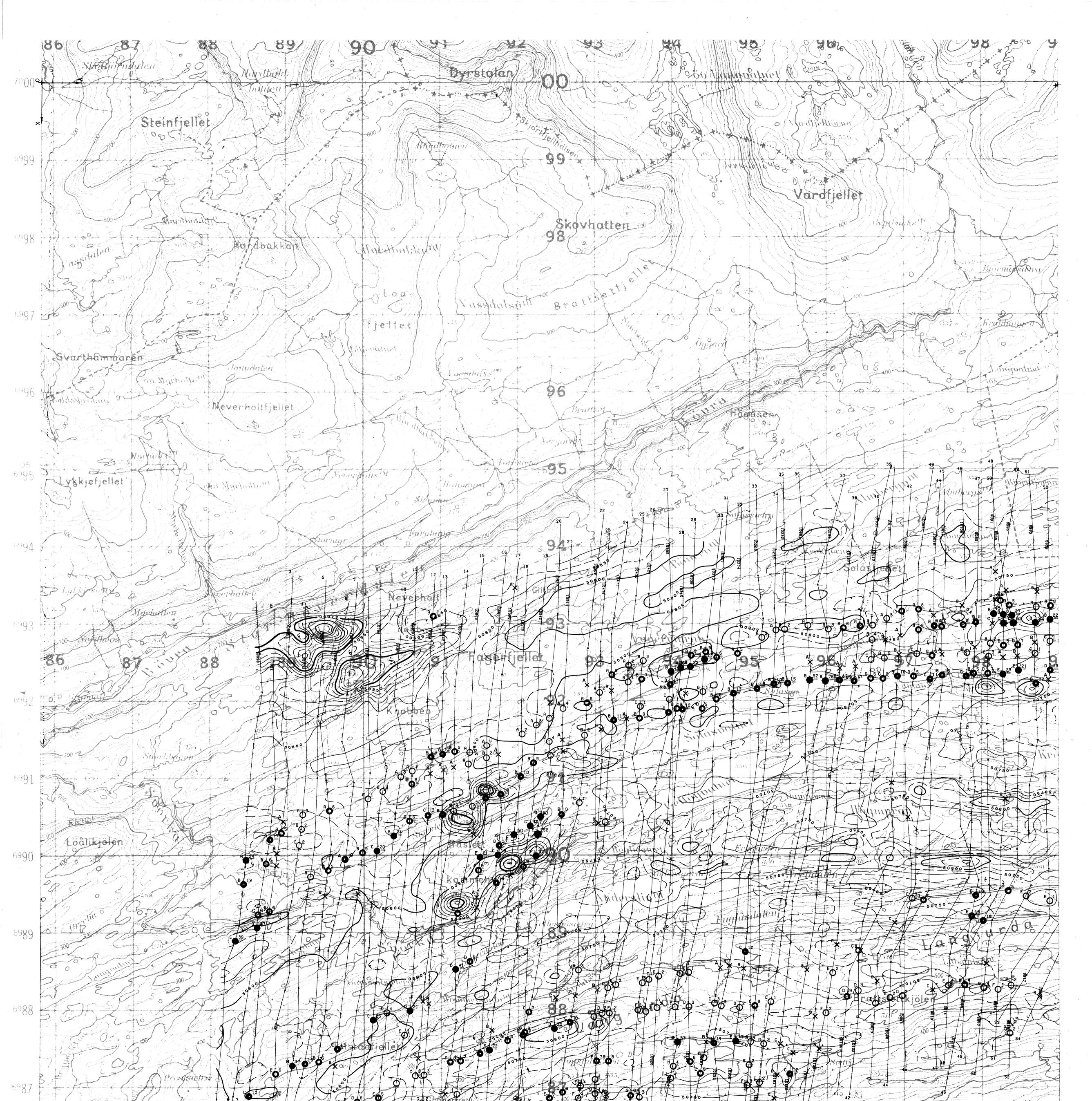


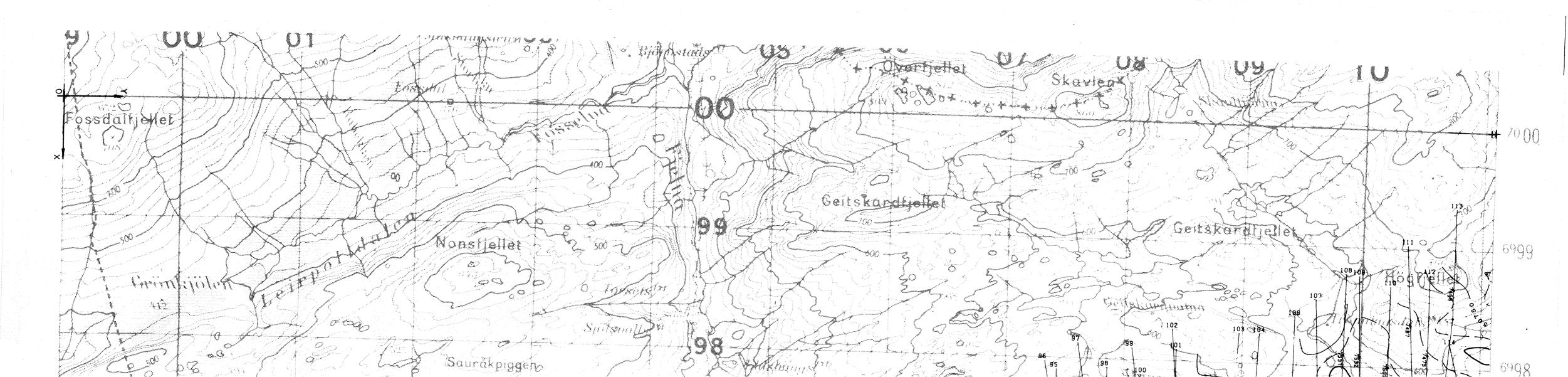


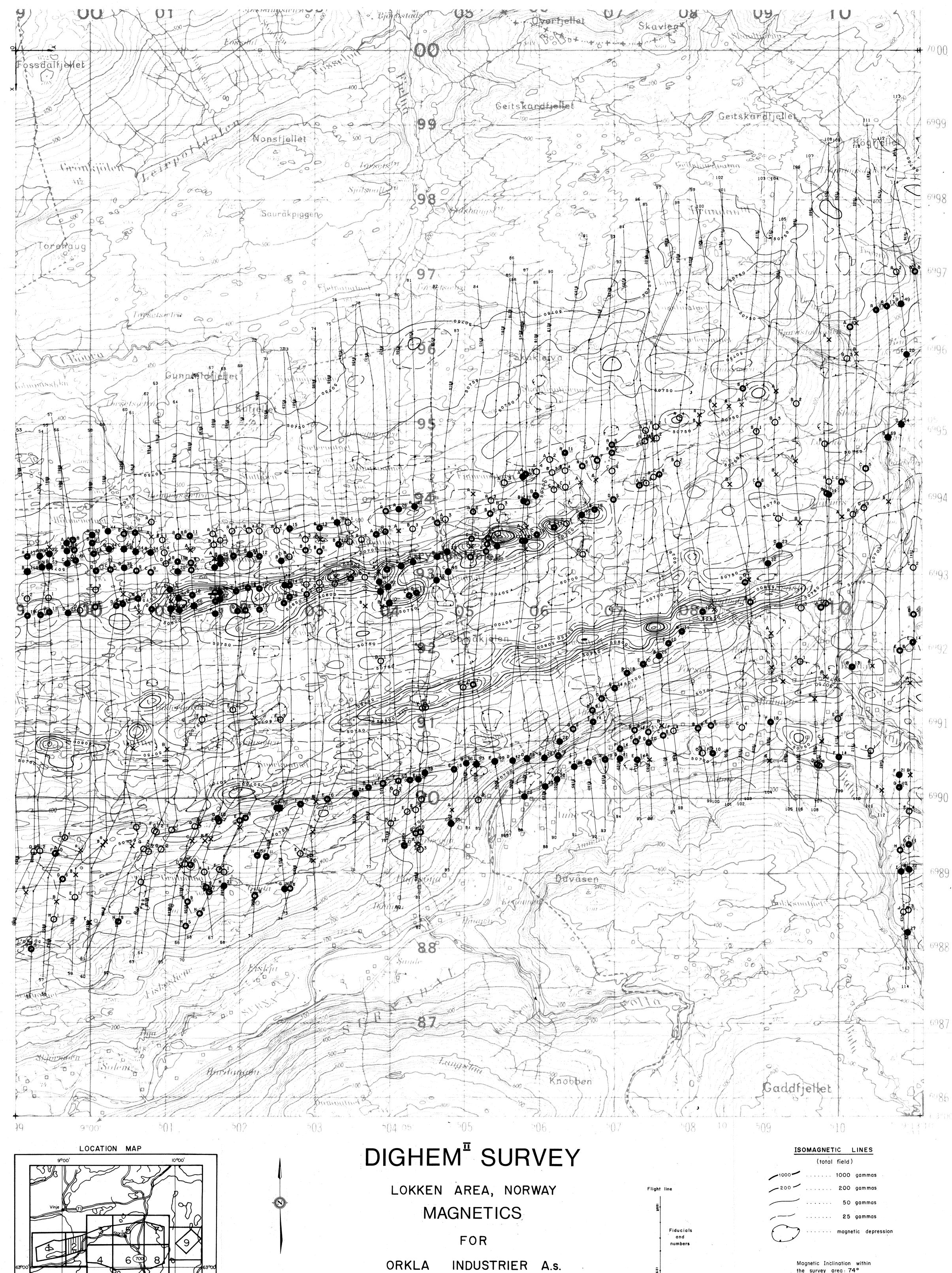


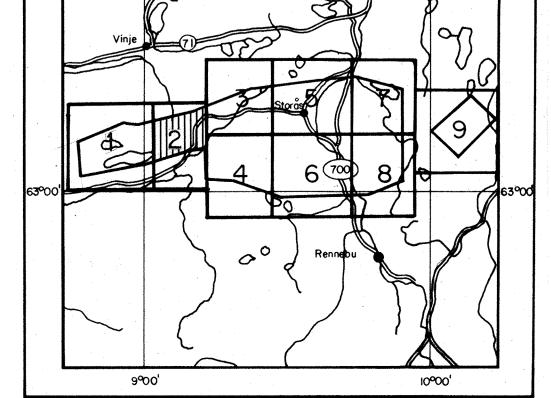
JOB DATE DRAWN BY CHECKED BY
702 APRIL' 82 F.W. S.K.





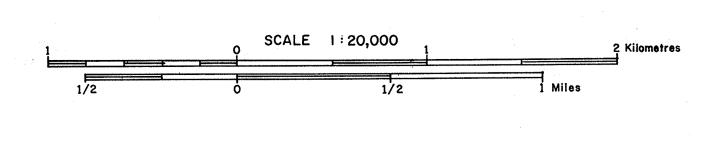






SCALE 1:750,000

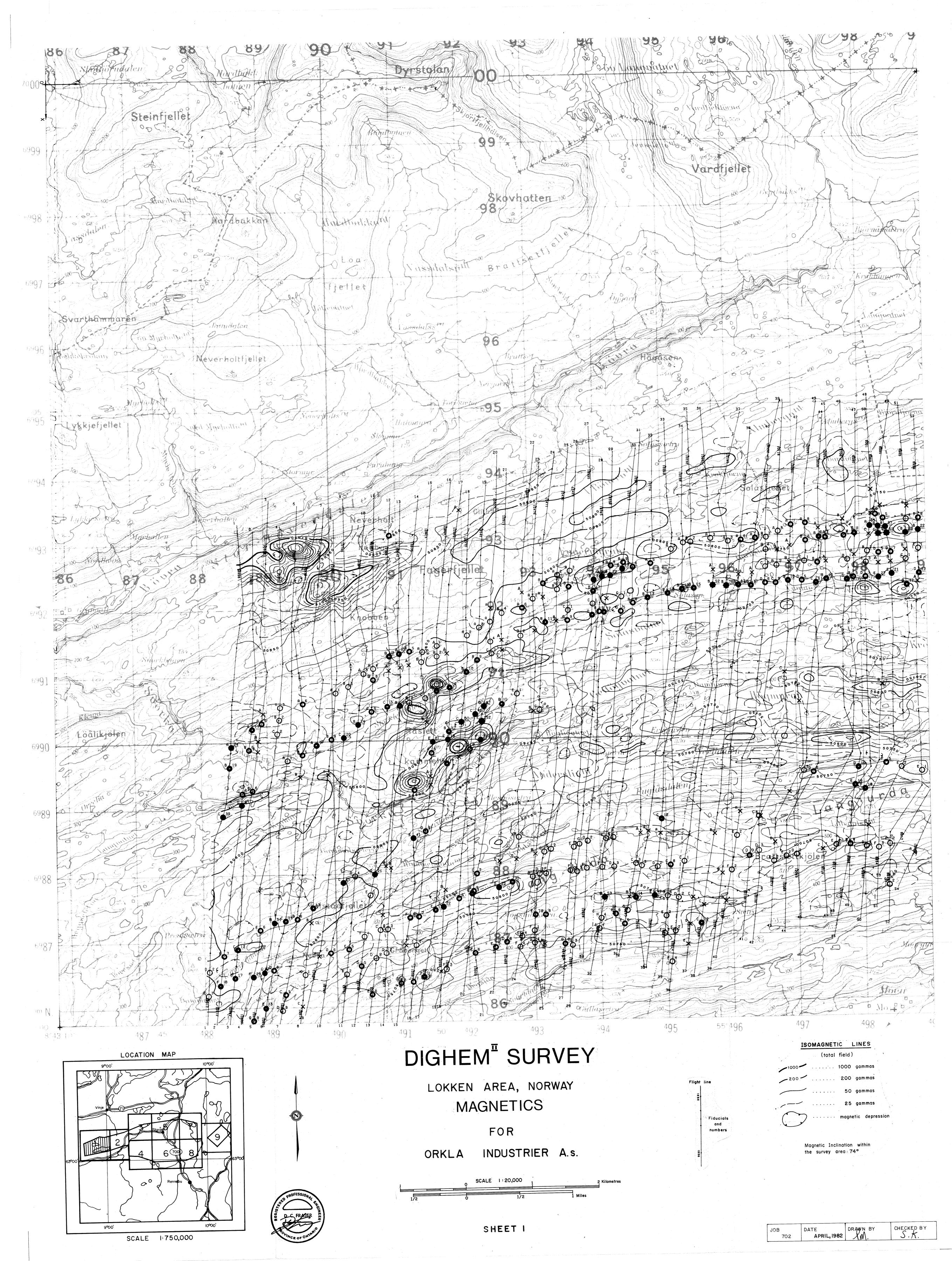


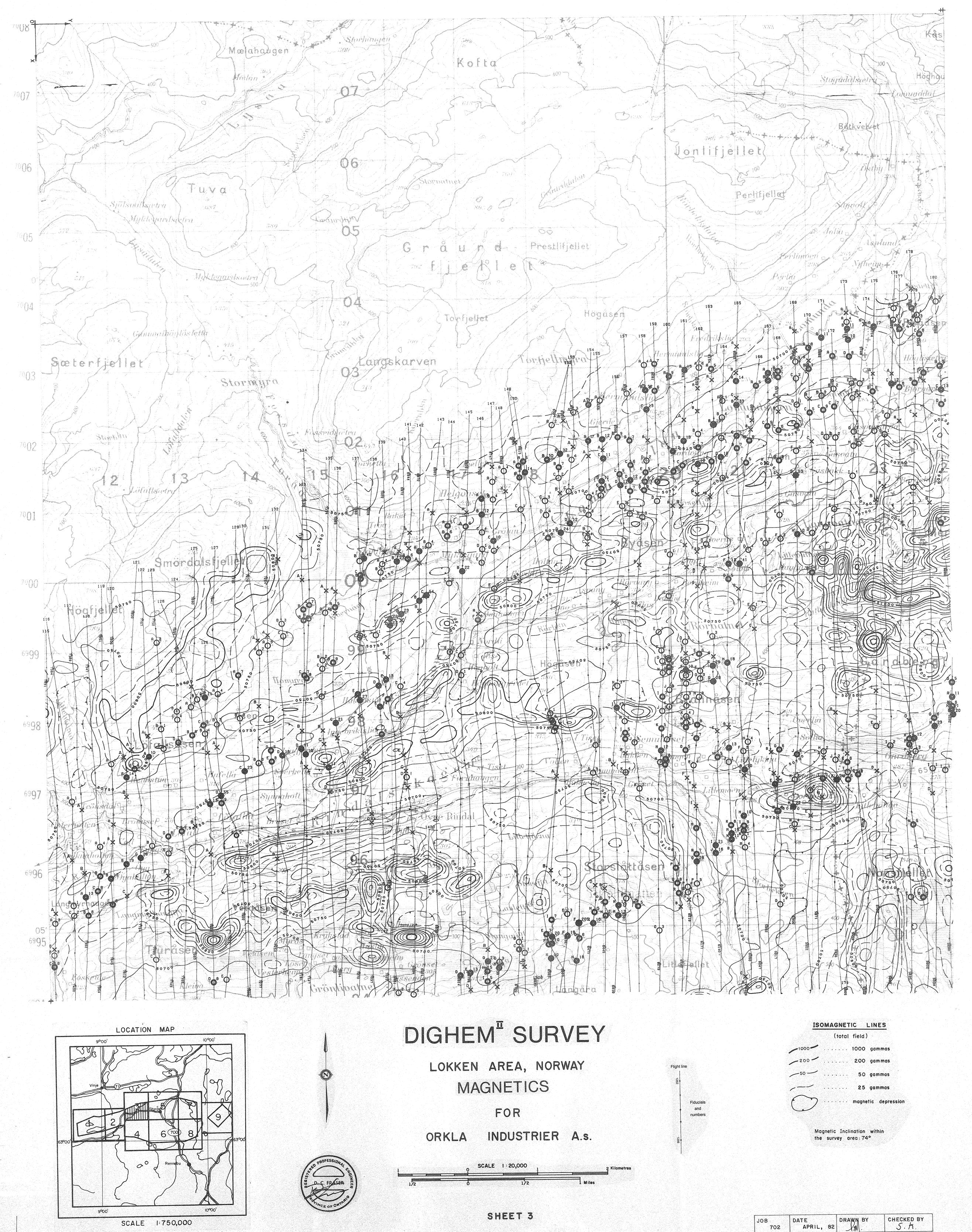


S	H	E	E	T	2

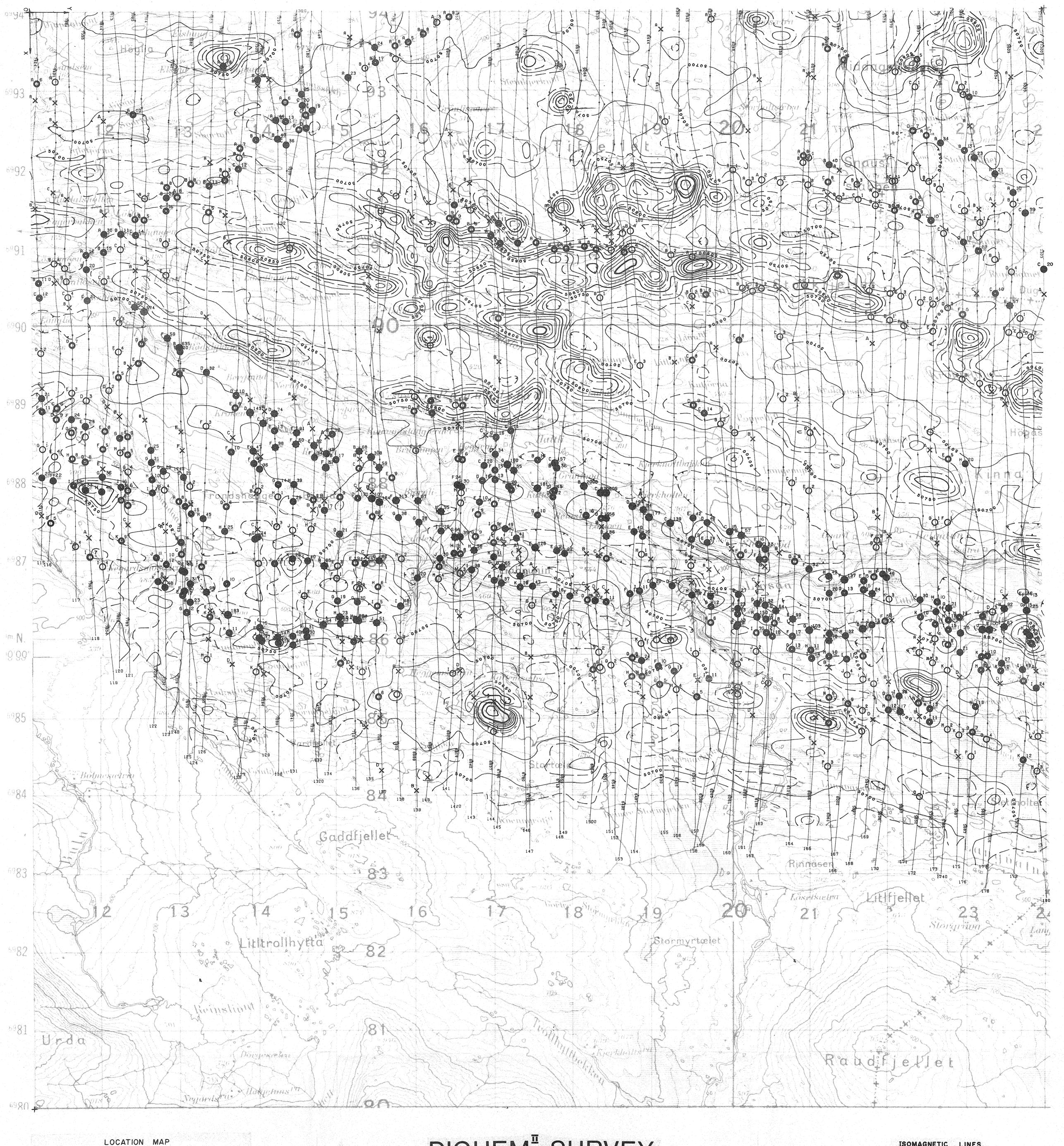
	1000 1000 gammas	
	50 gammas	
<u> </u>	25 gammas	
ducials and ambers	magnetic depression	on
	Magnetic Inclination within the survey area: 74°	
	·	

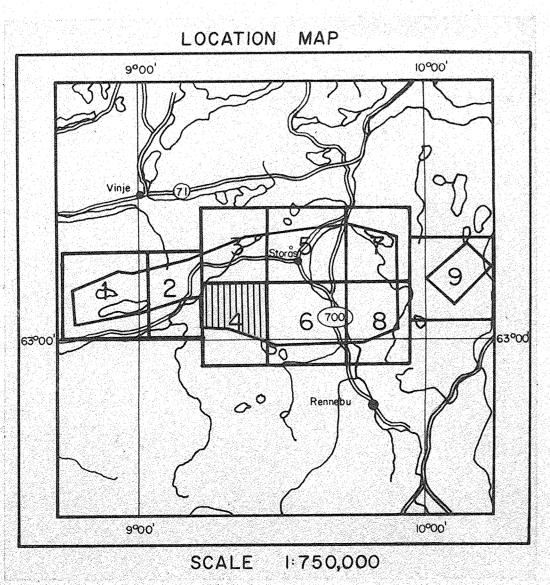
CHECKED BY S.K.

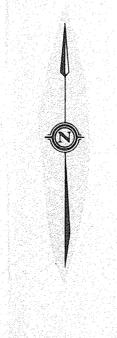




MAG SHEFT 3







## DIGHEM SURVEY

LOKKEN AREA, NORWAY MAGNETICS

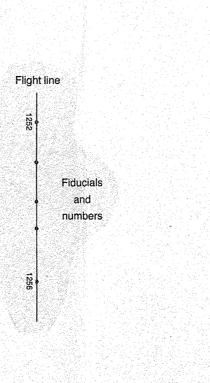
FOR

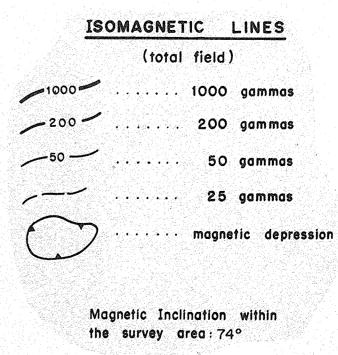
ORKLA INDUSTRIER A.s.



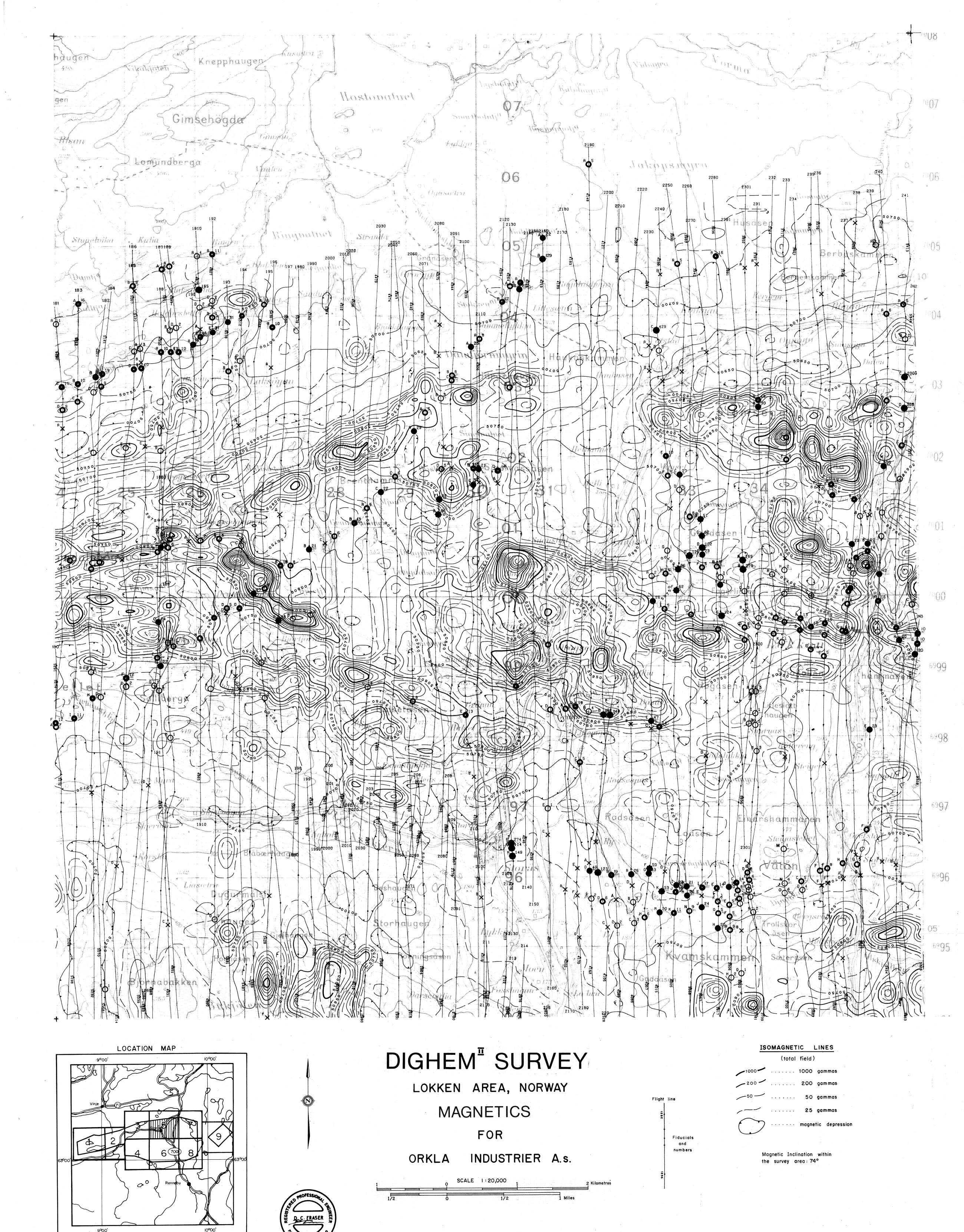
	SCALE 1:20,000	2 Kilometre
1/2	) 0 1/2	Miles

SHEET 4





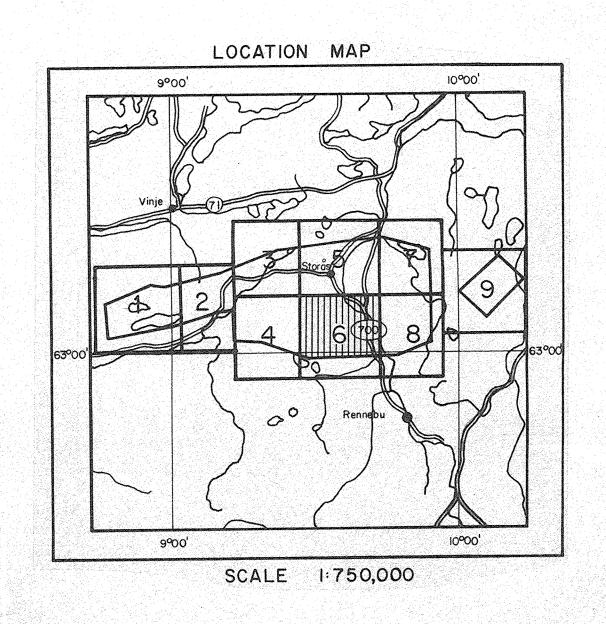
DATE APRIL'82

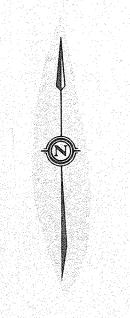


SHEET 5

SCALE 1:750,000

JOB DATE DRAWN BY CHECKED BY 5. K.

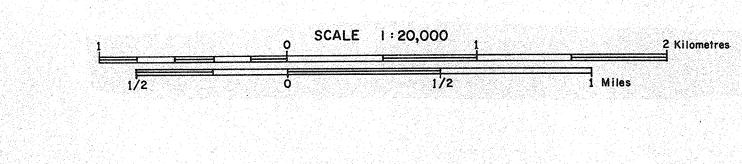




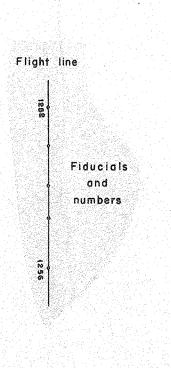
## DIGHEM" SURVEY

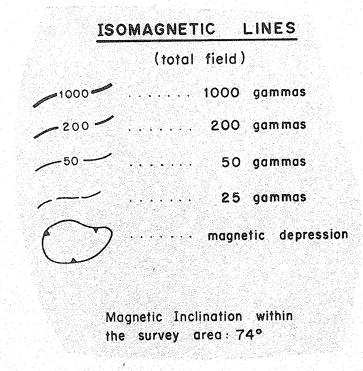
LOKKEN AREA, NORWAY MAGNETICS FOR

INDUSTRIER A.s. ORKLA

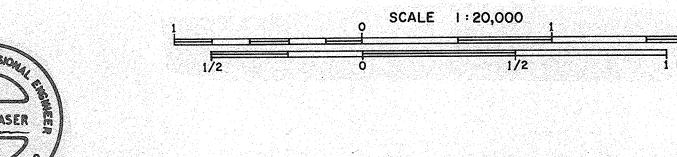


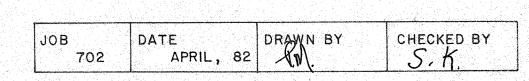
SHEET 6

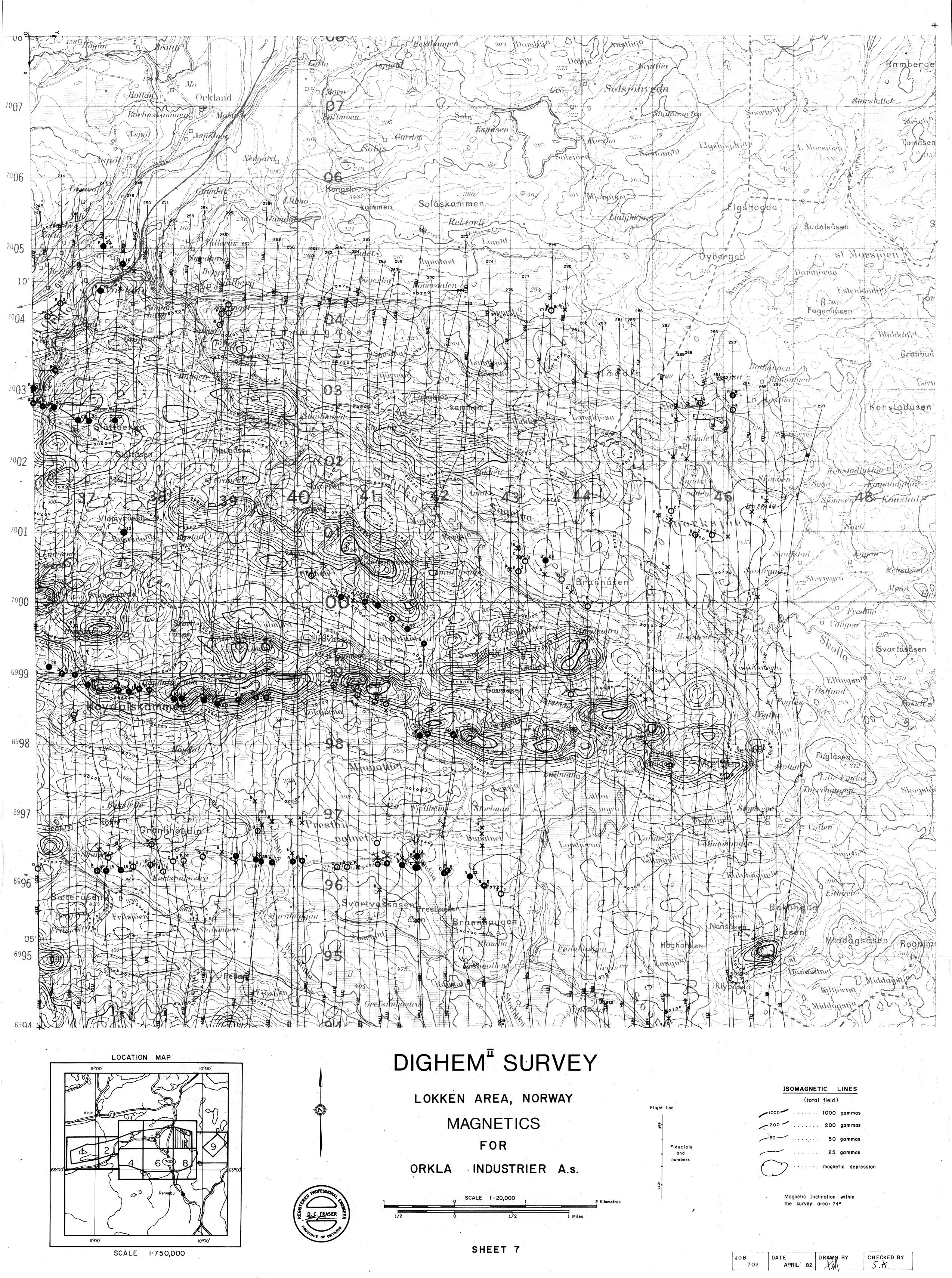


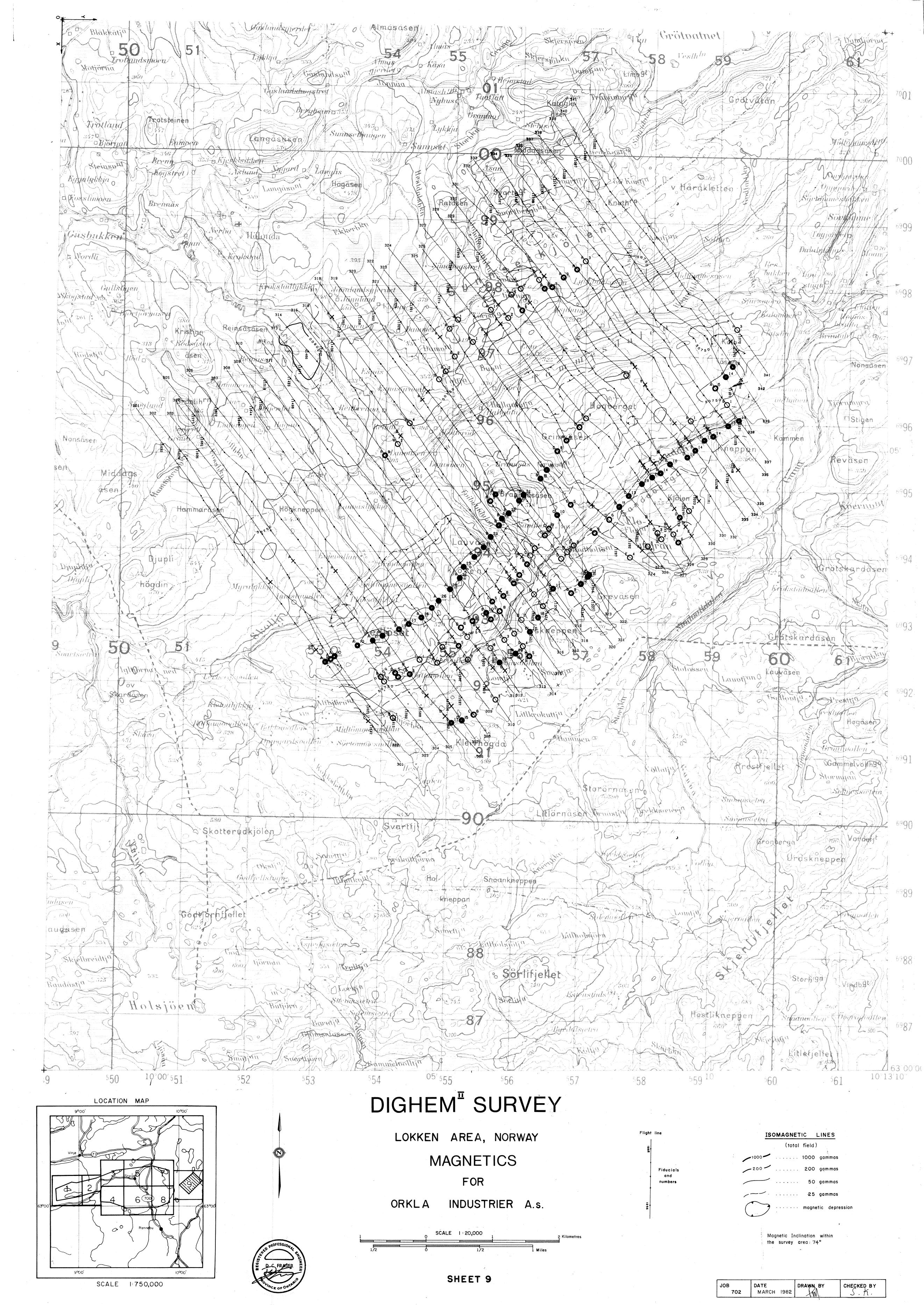


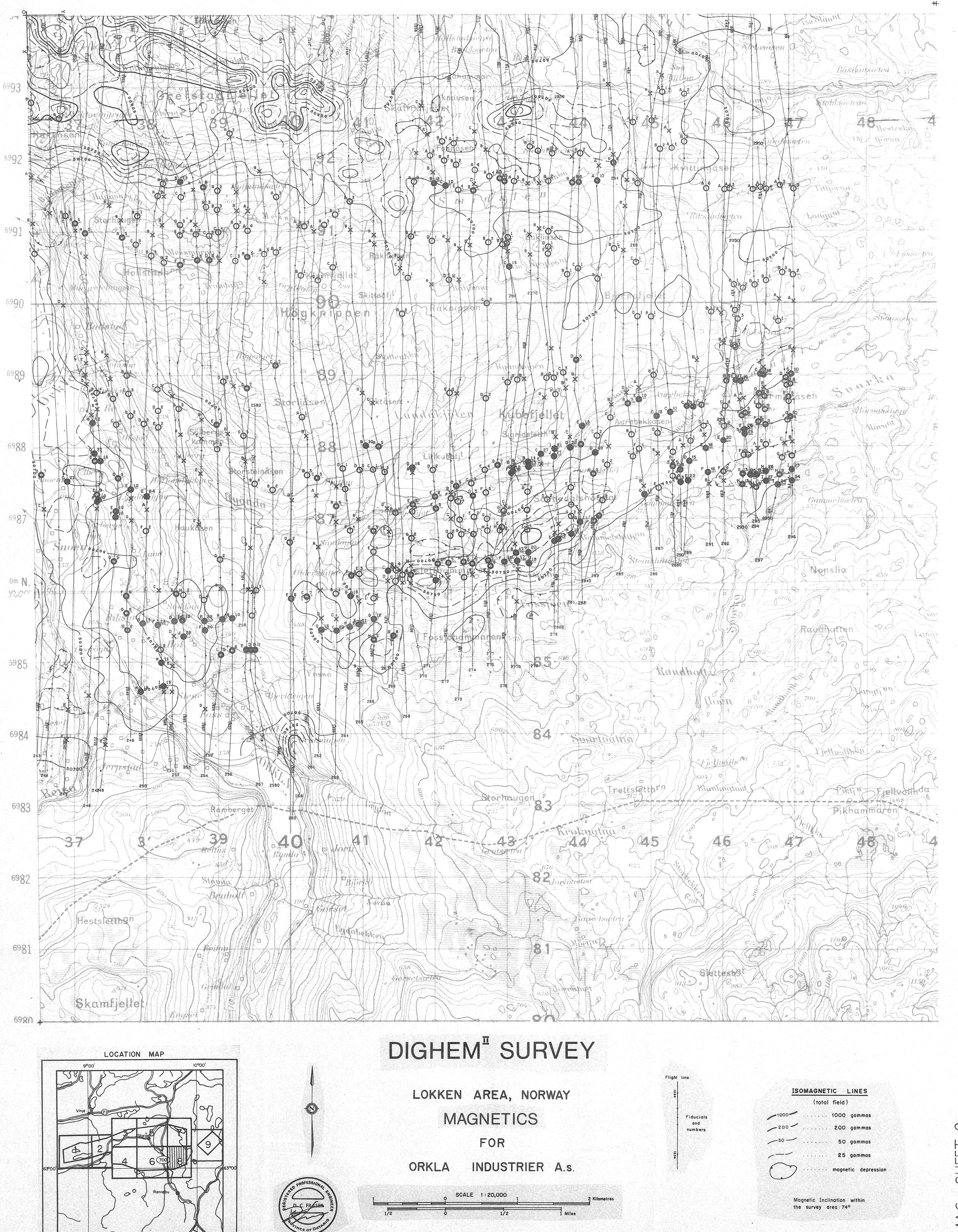
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SHEET 8

SCALE 1:750,000

MAG SHEET 8

CHECKED BY

DATE DRAWN BY